MACHINERY

JUNE 7, 1961 ONE SHILLING & THREEPENCE

ESSA

AUTOMATIC PRESSES

Models BHA 30, 60, 120, 180t.

✳ Give several times more blanks per regrind

plus ONLY HALF GRIND-OFF ALLOWANCE FROM DIE SURFACE

equals MANY TIMES LONGER TOOL LIFE

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ASSOCIATES LIMITED

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Midland Office and Demonstration Room

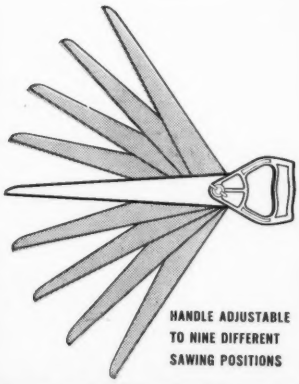
WILFORD CRESCENT NOTTINGHAM

Telephone: NOTTINGHAM 88008

Photograph by courtesy of Woods of Colchester Ltd, shows the blanking of rotor and stator laminations

For any job—
WOOD, METAL, PLASTIC ETC.
it cuts through the lot

Here's a saw which will cut both wood AND metal — *one* saw for all the odd jobs about the house, the farm, the garden, the building site and so on. If the "odd job" is the cutting of hard wood, soft wood, wood in which nails or bolts are embedded, hard rubber, plastics, fibreboard, the every-day range of pipes and bars made from mild steel, copper, brass, aluminium, lead and the like, here's the saw that will cut through the lot! The blade can be adjusted for sawing in almost any position.



HANDLE ADJUSTABLE TO NINE DIFFERENT SAWING POSITIONS

* Price
15/6

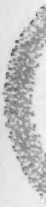
Eclipse

general purpose saw

Made by James Neill & Co. (Sheffield) Ltd., and obtainable from hardware and tool dealers

S.SA. 12

VOLUNTEER



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ELECTU

"These Wild-Barfield furnaces do a really good job"

Where heat-treatment is concerned—are you doing the job as economically as possible? It's surprising the number of people who invest in expensive machine tools for production—and then spoil a good job in outdated furnaces. And the result? Rejects—time, money and probably customer goodwill lost. More and more people are relying on Wild-Barfield equipment. Write for full details and see how you can save by changing to modern electric furnaces.

Self-contained Electrode Salt Bath ESB 346.
Standard Model delivery ex stocks

WILD BARFIELD

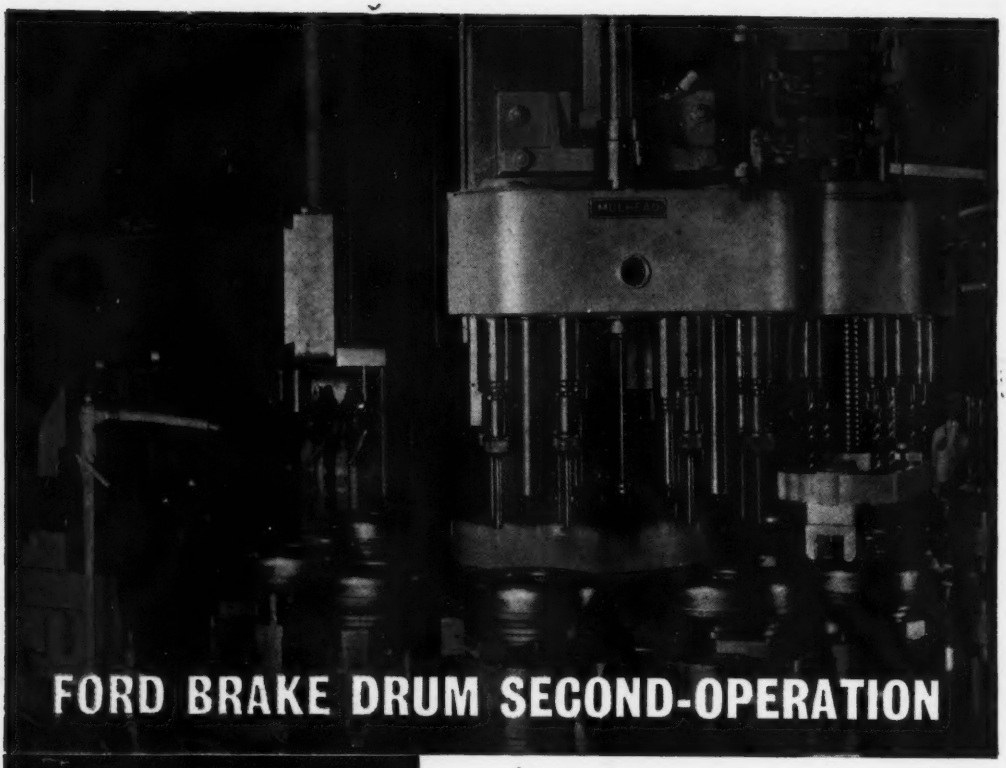
ELECTRIC FURNACES
FOR ALL HEAT TREATMENT PURPOSES
Backed by 40 years specialist experience

WILD-BARFIELD ELECTRIC FURNACES LIMITED

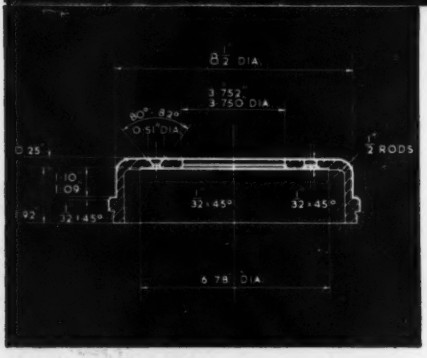
ELECFURN WORKS, OTTERSPOOL WAY, WATFORD BY-PASS, WATFORD, HERTS. Tel: Watford 26091 (8 lines) Grams: Elecfurn, Watford WB71

When answering advertisements kindly mention MACHINERY.

A



FORD BRAKE DRUM SECOND-OPERATION



MACHINED IN 40 SECONDS

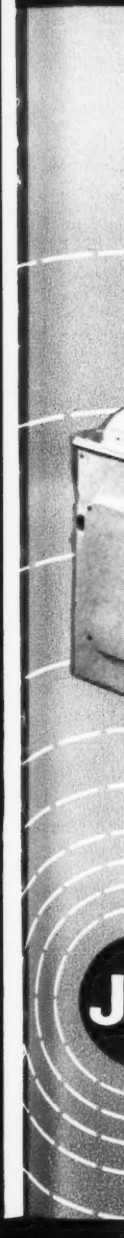
The use of special Mulhead multi-drill heads on the Ryder Verticalauto enables drilling, reaming, countersinking and back-chamfering operations to be performed in addition to standard boring and facing work.

The second operation on this Ford Brake Drum is completed at very high output rates on this 12-spindle No. 10 Ryder Verticalauto.

Ryder ***VERTICALAUTO***

Thos. Ryder & Son, Limited, Turner Bridge Works, Bolton, England.
Makers also of single spindle Rydermatics and Piston Ring Lathes.

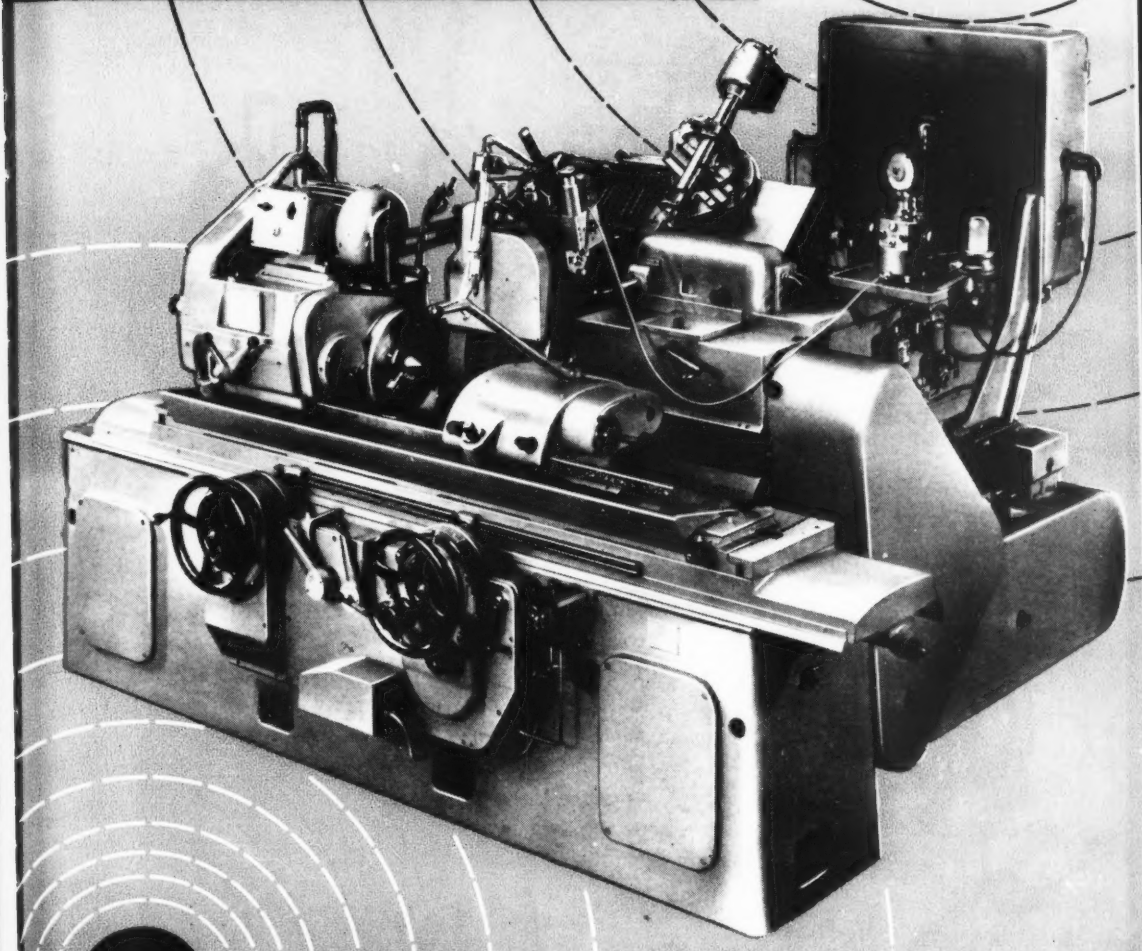
LA



LA PRODUCTION CYLINDRICAL GRINDERS

STANDARD AND FULLY AUTOMATIC MACHINES IN THE SIZE RANGE 12″ x 24″ TO 16″ x 120″

NEWALL
ESTABLISHED IN 190



JIC BUILT THROUGHOUT TO J.I.C. STANDARDS

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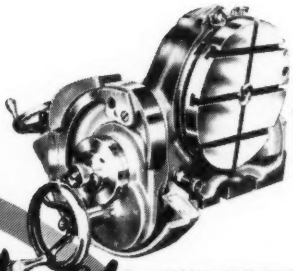
HAND OPERATED
PLAIN TYPES



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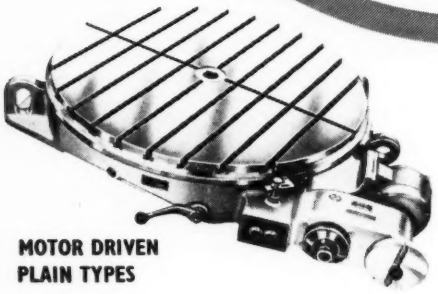
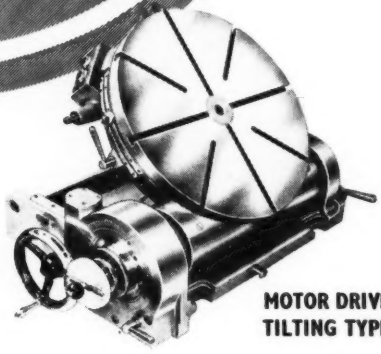
PRECISION ROTARY TABLES

FIRST CHOICE FOR PRECISE
CIRCULAR SPACING AND
ANGULAR POSITIONING



MOTOR DRIVEN
PLAIN TYPES



MOTOR DRIVEN
TILTING TYPES

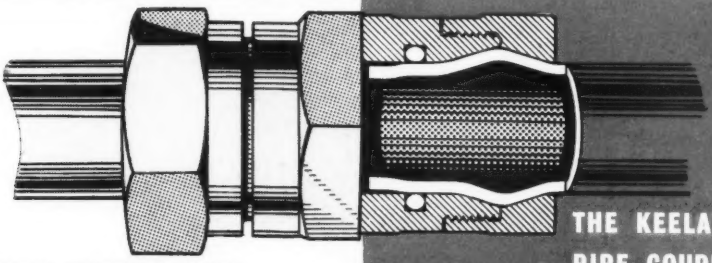
BUCK & HICKMAN LTD – OTTERSPOOL WAY – WATFORD BY-PASS – HERTS

HEAD OFFICE
P.O. BOX 74 WHITECHAPEL ROAD
LONDON, E.1.

BRANCHES
ALPERTON — BIRMINGHAM — BRISTOL
GLASGOW — LEEDS — MANCHESTER

KEELAVITE
Hydraulics

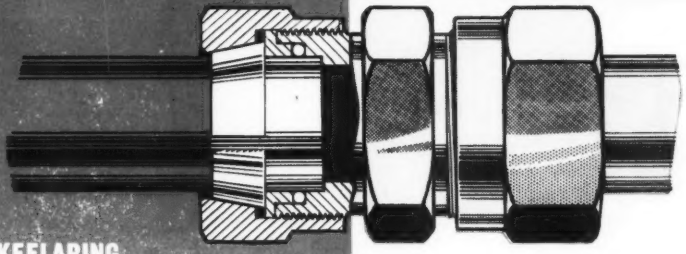
HIGH-PRESSURE PIPE COUPLINGS



Keelavite, the recognised authority on hydraulic power transmission, needed high-pressure pipe couplings to meet the high standards required for their successful hydraulic installations, result The KeelaTite and the Keelaring Couplings.

THE KEELATITE PIPE COUPLING

The KeelaTite coupling provides a simple safe and sure way for speedy hydraulic pipework. Absolute reliability under steady and fluctuating pressures. Tube-end is formed hydraulically by a quick and effortless operation.



THE KEELARING PIPE COUPLING

The new Keelaring coupling is a collet-type joint consisting of five separate pieces which when assembled force the sealing ring into a tapered recess and thus provide a leak proof seal. Standard tools give adequate tightening with no damage to tube ends. 100% reusable.

Each coupling has its special characteristics and uses, but both are equally successful. Designed to provide perfect sealing and to withstand vibration.

THE RECOGNISED AUTHORITY ON HYDRAULIC POWER TRANSMISSION

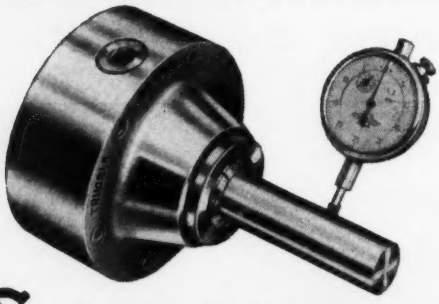
KEELAVITE
Hydraulics

For full details of these couplings write to

KEELAVITE HYDRAULICS LTD, ALLESLEY, COVENTRY

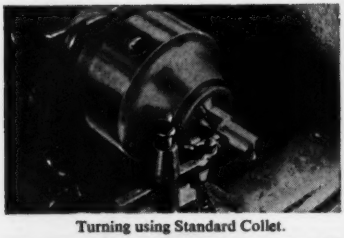
Telephone: Meriden 441

9 Applications to the Crawford "TRUGRIP" COLLET CHUCK



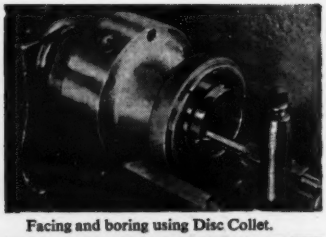
Sizes: 5in. dia., 1in. capacity;
7in. dia., 2in. capacity

With the Crawford "Trugrip" Collet Chuck, work is held true, instantly, by the turn of a key. Absence of drawtube or sleeve means that full bore of spindle can be used. Powerful, positive action, with no distortion, and no marking of previously machined surfaces, makes it ideal for second operation work. Wide range of collets greatly increases capacity of machine, nine typical examples shown below.

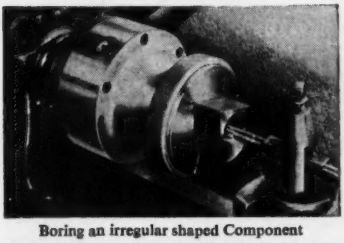


Turning using Standard Collet.

Facing and turning using Ring Collet.

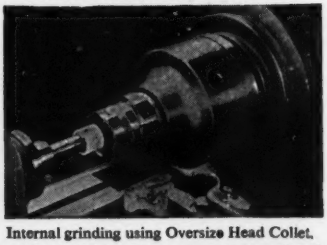


Facing and boring using Disc Collet.

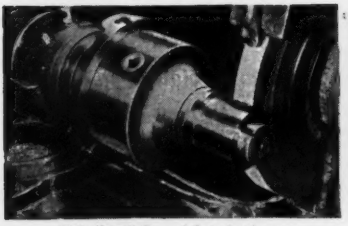


Boring an irregular shaped Component

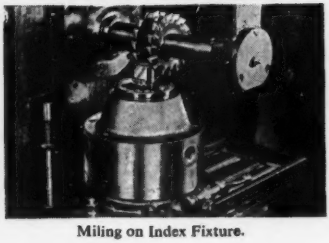
Grinding using Standard Collet.



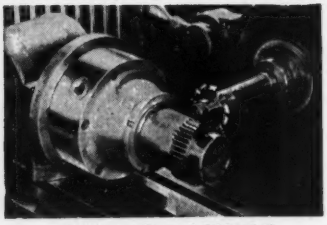
Internal grinding using Oversize Head Collet.



Grinding O.D. and face dead true with bore using Expanded Mandrel.



Miling on Index Fixture.



Milling on Expanded Mandrel.

CRAWFORD COLLETS LIMITED

WITNEY · OXON · TELEPHONE WITNEY 334

London Stockists: Acbars Limited, 16-18, Macleod Street, Walworth Road, S.E.17. Tel: RODney 7191
Midland & N W England Stockists: Retselp Engineering Ltd., Vulcan Road, Industrial Site, Lode Lane, Solihull, Birmingham. Tel: Solihull 2239
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ABWOOD

HIGH PRECISION
TOOL & DIE SURFACE GRINDER
MODEL SG-4H

HYDRAULICALLY OPERATED

RAPID POWER ELEVATION OF KNEE

HIGH PRODUCTION WITH VERSATILITY

SENSITIVE CONTROLS WITH RUN OUT TO LOADING POSITION

Automatic in-feed for depth of cut in .0002in. steps.

Pressure lubricated completely covered slideways.

Hydraulic reservoir and pump housed in base.

Large capacity mobile coolant tank with removable sludge tray.

Segmental chuck available for maximum stock removal.

Built to Schlesinger limits.

Finishes to 1.5 micro inches on suitable materials.

Manual table traverse for use with Cutter Grinding Attachment.

ABWOOD MACHINE TOOLS LTD., PRINCES ROAD, DARTFORD, KENT

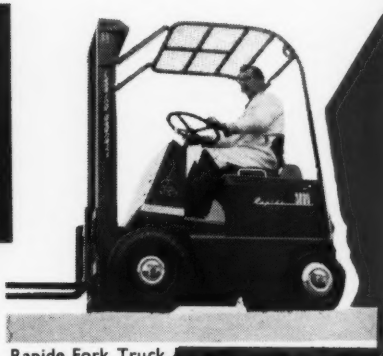
Telephone: Dartford 25271 (5 lines)

Telegrams: ABWOOD DARTFORD

PEAK KEEPS

Precision-made components by Peak Engineering have contributed to the efficiency of modern transport.

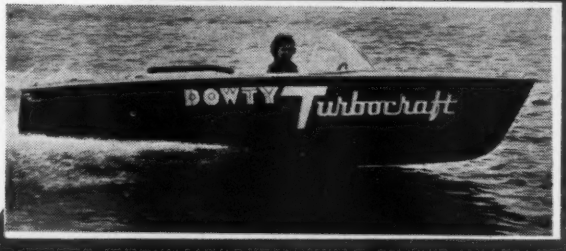
De Havilland Comet by permission of 'Flight'



Rapide Fork Truck
Bagnall Ltd.

Land-Rover by permission of The Rover Co. Ltd.

Centurion Tank



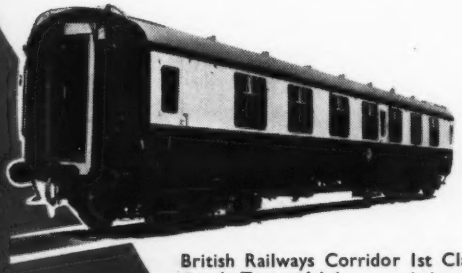
Standard model Turbocraft by permission of Dowty Marine Ltd.

Your safety and comfort may depend on us.

PEAK ENGINEERING CO. LTD.

THEM MOVING

These illustrations represent some of the projects in which Peak precision engineering has been incorporated.



British Railways Corridor Ist Class Coach Type 'A' by permission of Metropolitan-Cammell Carriage & Wagon Co. Ltd.

Sailing Craft fitted with twin Perkins 35 h.p. Outboard Motor.
Inset-six 354 vehicle diesel engine, by permission of Perkins Group of Companies.

ger Coach by
A.E.C. Ltd.

rdson Tractor, by permission of Ford Motor Co. Ltd.

Precision made parts by us are used in a vast variety of engineering applications in the air, on the land, on the sea and even in your kitchen. Your washing machine probably has one. If you are lucky enough to own a dishwasher, there is probably one in that too.

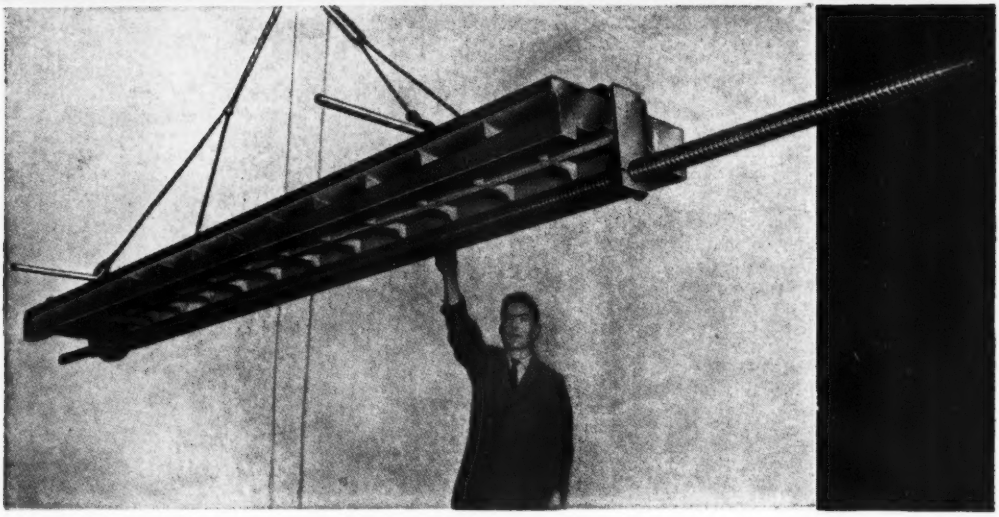
PRECISION AND PRODUCTION ENGINEERS

MASONS ROAD, STRATFORD — UPON — AVON, WARWICKSHIRE.

Telephone: Stratford-upon-Avon 3821. Telex 31627

LUBRICATION & WEAR PROBLEMS SOLVED BY ROTAX

WITH THE MOST ADVANCED RECIRCULATING BALL THREADS USED IN INDUSTRY



Rotax Precision Ballscrew assemblies are available to manufacturers, in all types of industry, for all types of application. Precision Ballscrews improve machine tool efficiency and drastically reduce maintenance costs.
The 25′ hardened precision ballscrew illustrated is being fitted to a high speed plane miller at Brooke Tool Automation Limited.

ROTAX

INDUSTRIAL GROUP ROTAX LIMITED
WILLESDEN JUNCTION, LONDON N.W.10

LUCAS-ROTAX (AUSTRALIA) PTY., LTD., Melbourne and Sydney, Australia
LUCAS-ROTAX LTD., Toronto, Montreal and Vancouver, Canada

WIN half the battle BEFORE you start!

PL

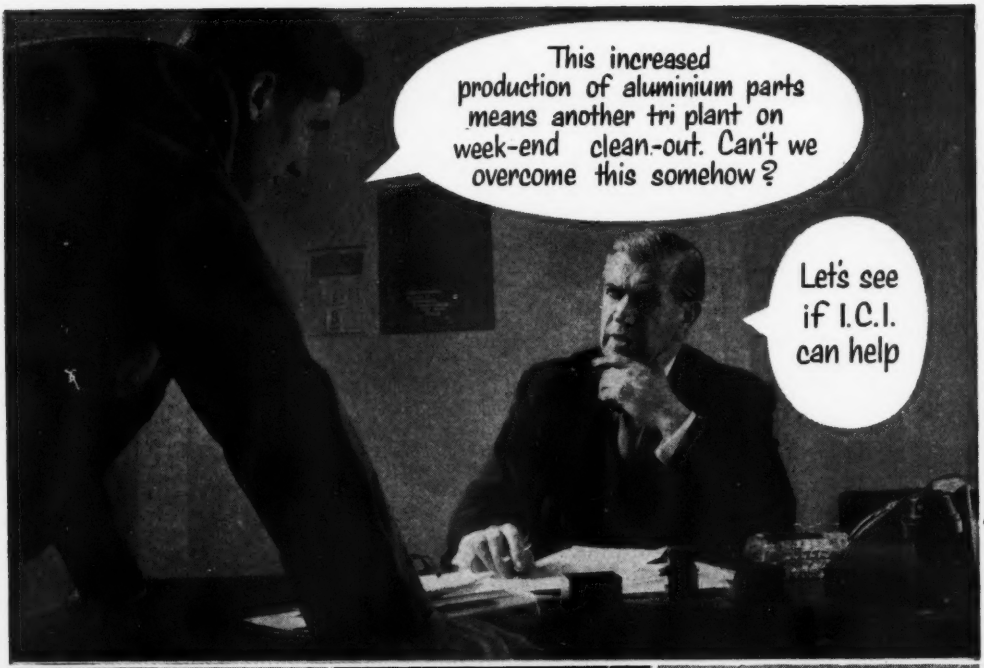
SIZES FROM $\frac{1}{16}$in. TO 1$\frac{3}{4}$in. DIAMETER SUPPLIED TO LIMITS OF ±0·00025in. SIZES ABOVE 1$\frac{3}{4}$in. TO 3in. DIAMETER SUPPLIED TO LIMITS OF ±0·0005in. LENGTHS FROM 6ft. TO 30ft. ALL WITH FLAWLESS SURFACE FINISH.

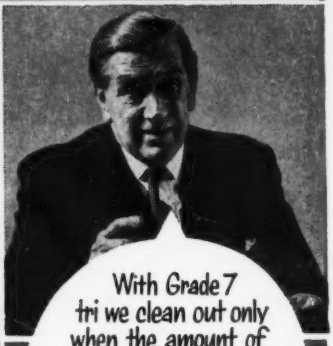
PRATT, LEVICK & CO. LTD.

CHESTER · ENGLAND

TELEPHONE: CHESTER 22265/6

When answering advertisements kindly mention MACHINERY.


This increased production of aluminium parts means another tri plant on week-end clean-out. Can't we overcome this somehow?
Let's see if I.C.I. can help



I.C.I.'s rep. told us about a new I.C.I. solvent—Grade 7 trichloroethylene—that gives excellent protection against aluminium reaction.

We decided to tackle our problem by putting all plants dealing with aluminium on Grade 7 tri-which would mean less frequent clean-outs.

With Grade 7 tri we clean out only when the amount of aluminium swarf makes it necessary – which gives weeks of continuous running. Ask I.C.I. for Grade 7 trichloroethylene if you are worried about degreasing aluminium.

ICI GENERAL CHEMICALS DIVISION

It pays to consult I.C.I. Metal Degreasing Service

IMPERIAL CHEMICAL INDUSTRIES LIMITED LONDON SW1

DP.267

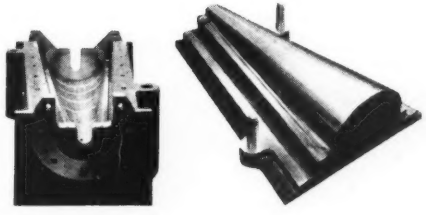
Save on time and cost of cold and hot forming operations by using HARPER 'CAST-TO-FORM' TOOLS

If you are forming metals, plastics, rubber, glass fibre or asbestos compounds you can save time and money. Harper 'cast-to-form' tools need minimum finishing before putting into service and first quality materials ensure long life. We can offer exceptionally good delivery.

Fully descriptive technical leaflet T.3 on request from:

JOHN HARPER & CO. LTD., WILLENHALL, STAFFS.

WILLENHALL 124 (5 lines) · FOUNDED 1790 · LONDON: ABBey 5906/7
MANCHESTER: BLAckfriars 0295 · POOLE FOUNDRY LTD: POOLE 212
Makers of the famous Beatrice Oil Heaters and Harper Housewares



Showing the high finish obtainable on polished tools used for production of six-feet long asbestos components.

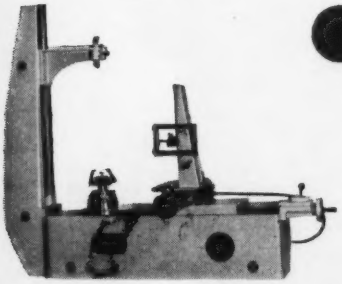
let us "HANDLE" your machines

WM. WHITELEY & SONS, LTD. *incorporating* J. CHARLESWORTH
(MACHINE TOOL DIVISION) PROSPECT IRONWORKS, LOCKWOOD, HUDDERSFIELD, YORK
Telegrams: Drying, Huddersfield Telephone: Huddersfield 4410
makers of Machine Components since 1854

Goulder

GEAR MEASURING EQUIPMENT

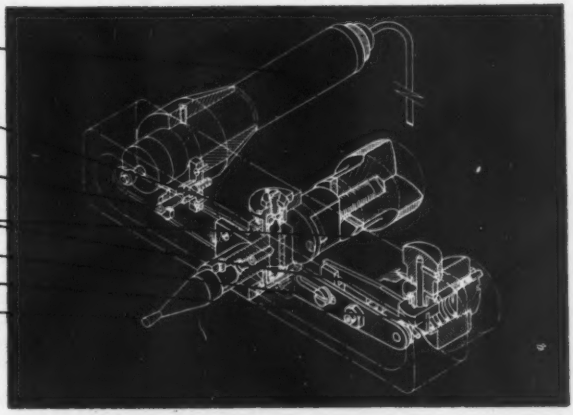
This series of advertisements is intended to show how attention to detail design backed by careful and precise manufacture has made Goulder gear measuring equipment first choice of buyers who appreciate these qualities.



INVOLUTE TESTER INDICATING HEAD

used on Goulder Nos. 1, 2 and 3 Involute Testers to measure deviation of profile from true involute.

- ELECTRONIC RECORDING USING AXIAL GAUGE HEAD WHICH CAN BE USED ON OTHER INSTRUMENTS WHEN REQUIRED
- PIVOT BEARINGS FOR SENSITIVITY AND ACCURACY
- PROTECTION AND EASE OF OPERATION THROUGH TRAVEL LIMITING DEVICE
- BUILT IN BIASSING THROUGH LEAF SPRING
- SIMPLE MEASURING PRESSURE ADJUSTMENT
- ADJUSTABLE BALANCE SPRING
- INTERCHANGEABLE STYLUS
- UNIT CONSTRUCTION FOR EASE OF MAINTENANCE
- ROBUST AND DUSTPROOF ASSEMBLY



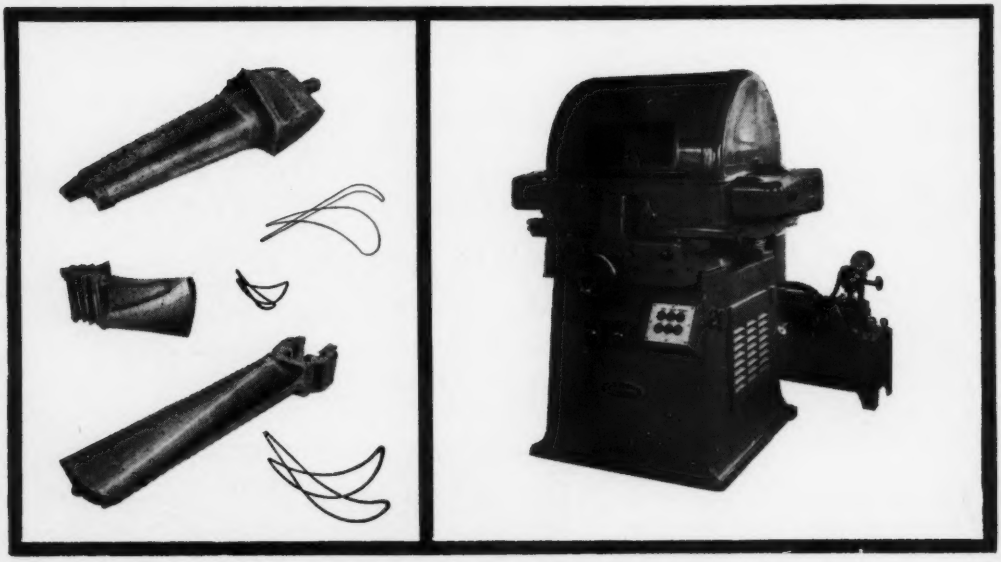
Goulder *THE NAME FOR ALL GEAR TESTING*

J. Goulder & Sons Ltd., KIRKHEATON, HUDDERSFIELD. *Tel: Huddersfield 5252-3*

M.15

Cadamco

The only precision copy belt grinding machine in the world to reproduce any shape of turbine blade



- Automatic machine cycle—one operator can control a bank of machines
- Accurate to ± ·002 in.
- Currently operating throughout the British turbine industry

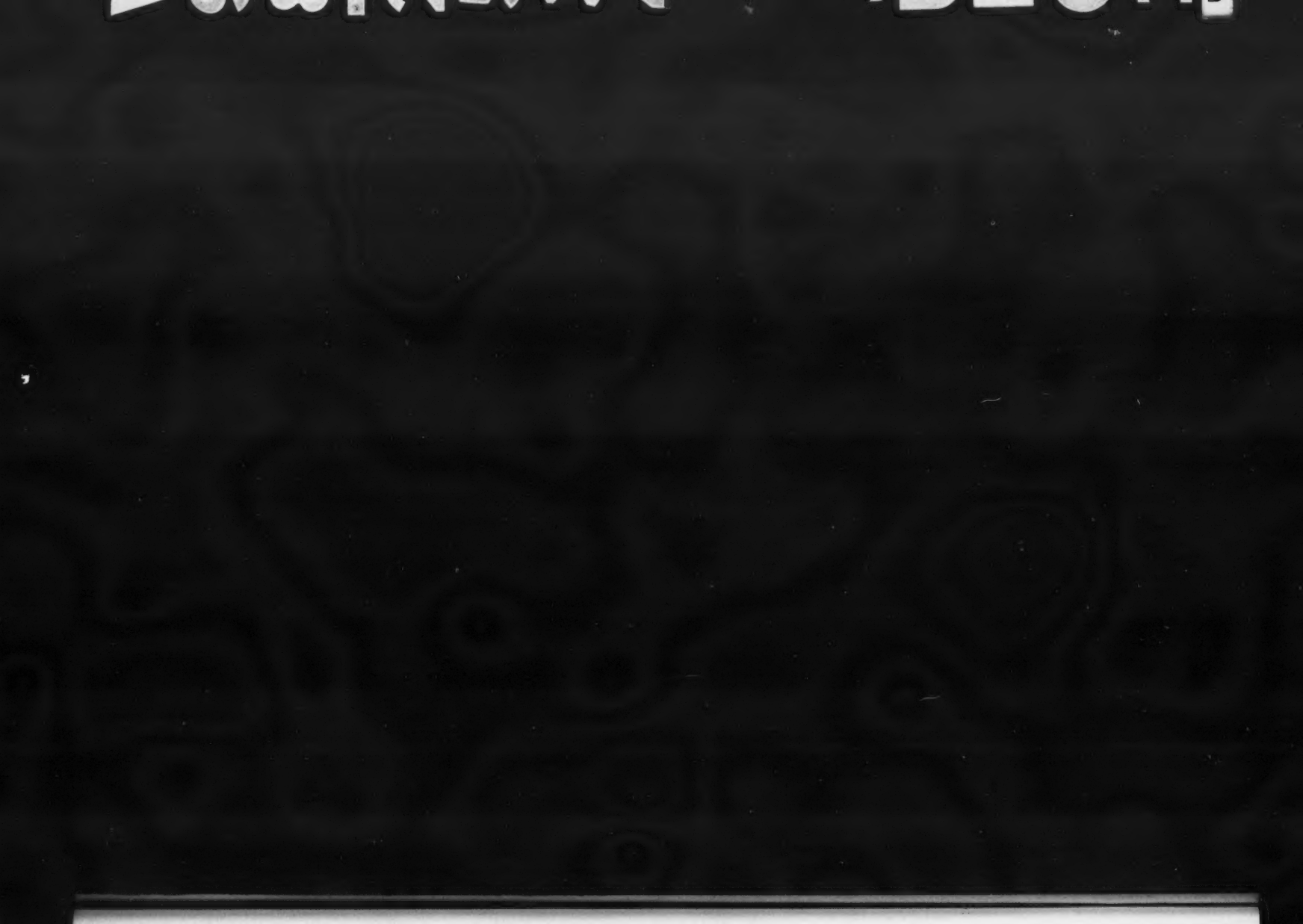
CYRIL ADAMS & CO. LTD.,

155 East Barnet Road, New Barnet, Hertfordshire
Telephone: Barnet 2335/6/7

Designers and Manufacturers of Jigs, Fixtures and Special Purpose Machine Tools

Member of the Staveley Coal & Iron Co. Limited Group of Companies, in association with James Archdale and George Richards

Member of the Machine Tool Trades Association



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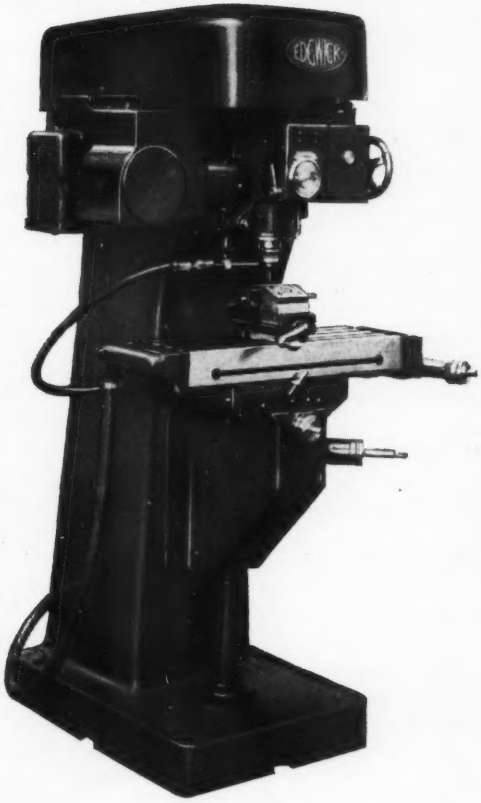
—— for fast, accurate machining of keyways, slots, splines, etc., the ——

EDGWICK KEYSEATER



This machine is designed to machine a keyseat by the well-known principle of a series of light cuts with a reciprocating cutter slide and a sequence down-feed.

On general toolroom work the machine can be used to advantage as a light hand-feed vertical milling machine.

Max. keyway cut, auto crank drive and table adjustment, $\frac{1}{2}$" x 20". (at one setting of the table $\frac{3}{4}$" x 5").

Max. depth of keyway cut, automatic, $2\frac{1}{4}$".

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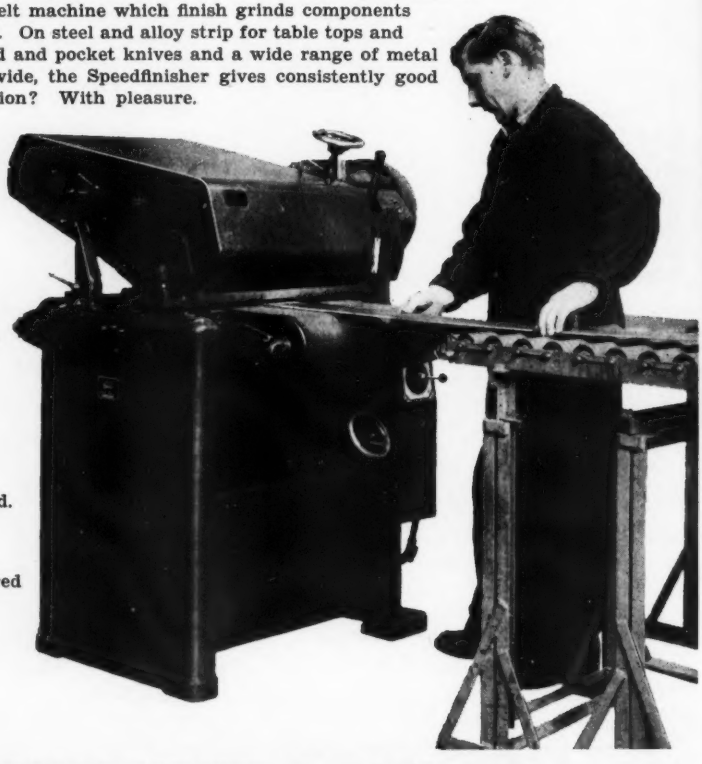

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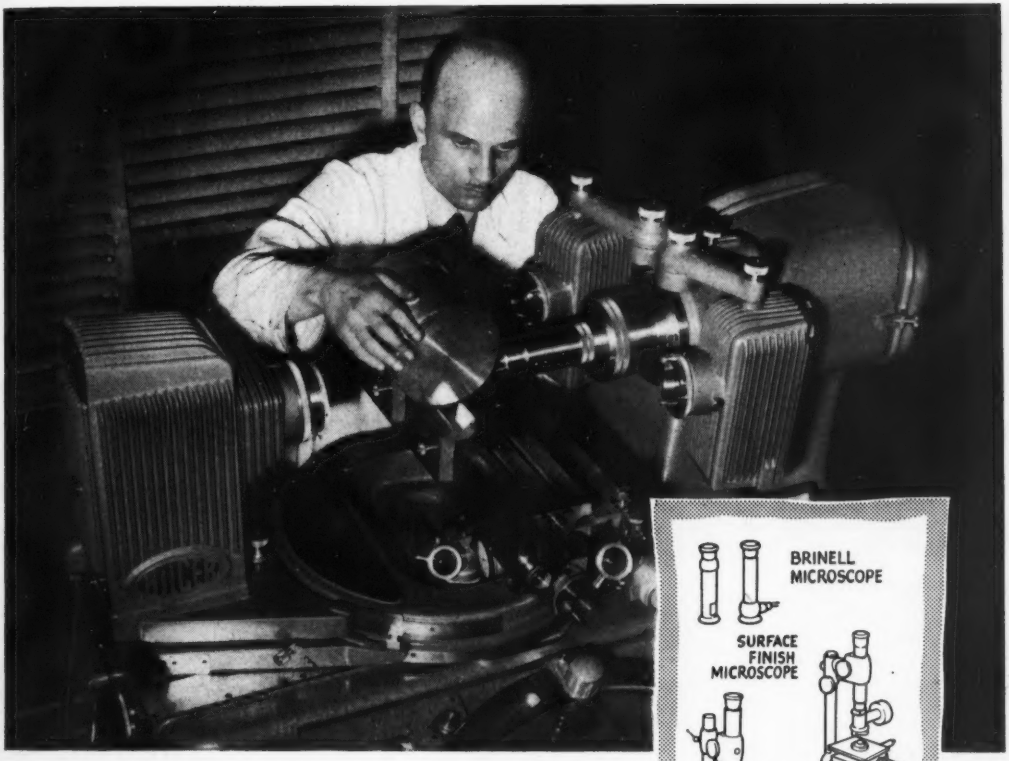

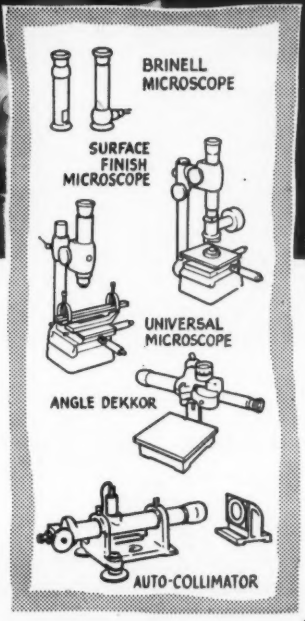

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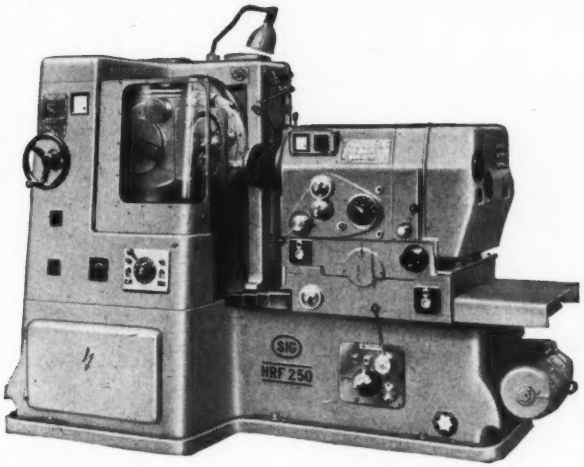

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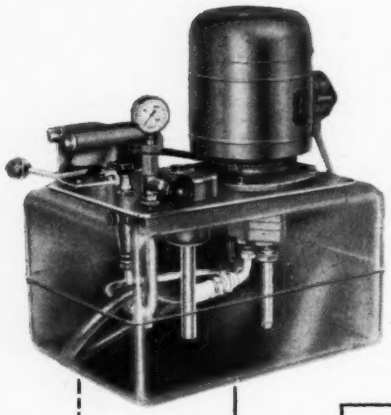

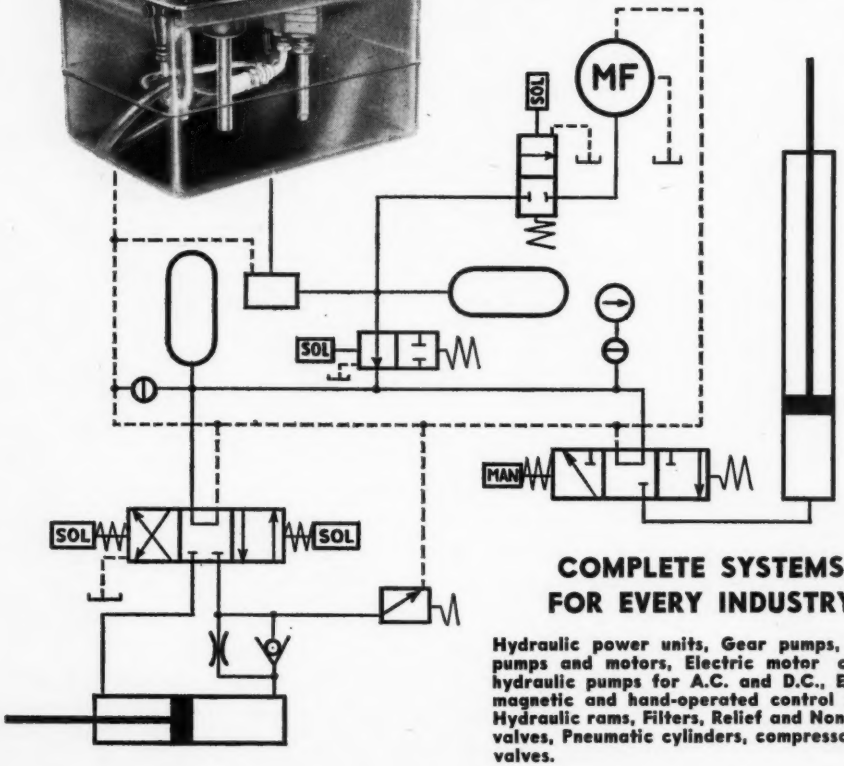

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Single lever operation.
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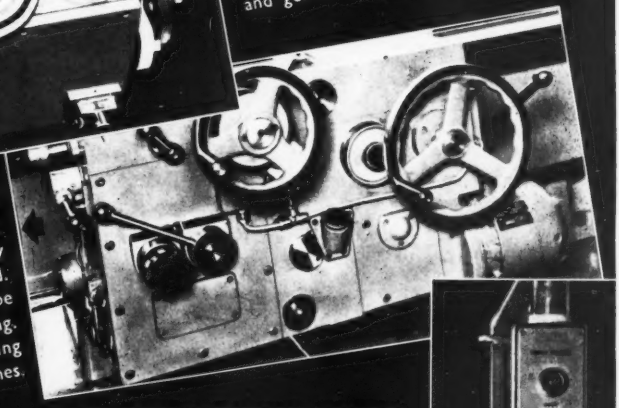

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Totally enclosed with all gears and bearings pump lubricated.
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Feed change allows feeds to be halved or doubled while cutting.
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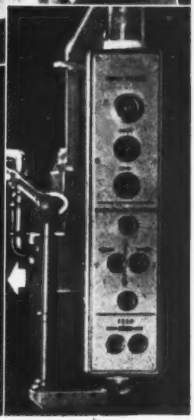

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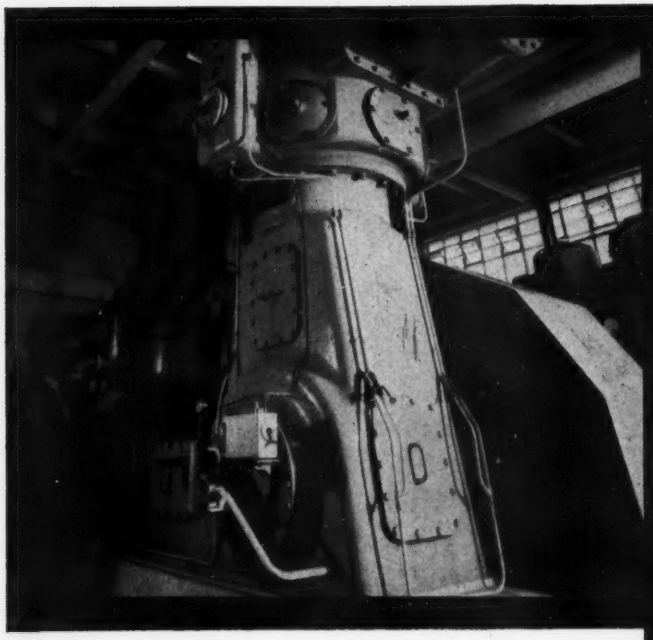

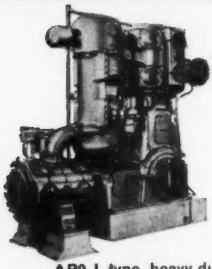

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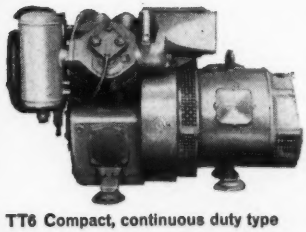
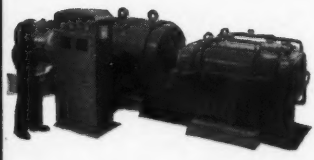


TT6 Compact, continuous duty type



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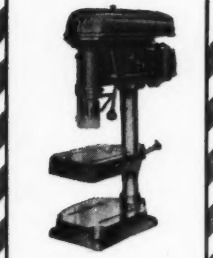

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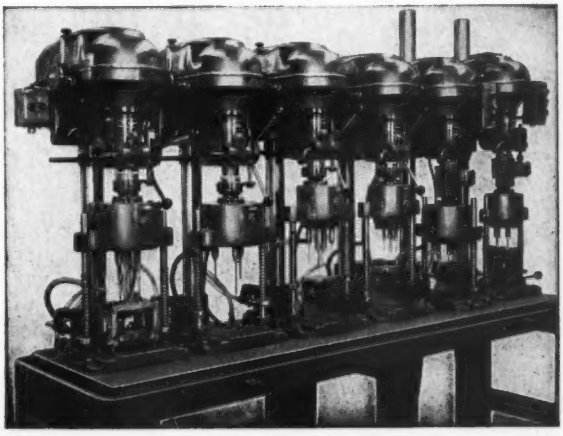

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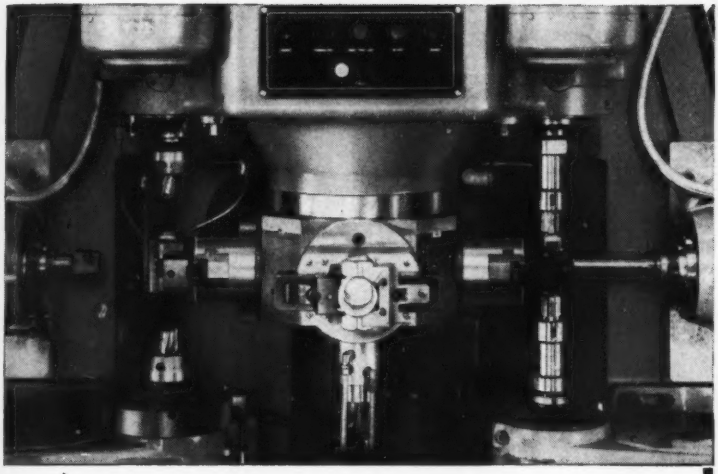

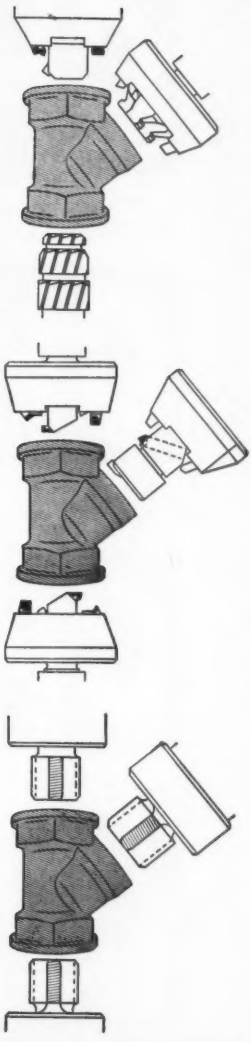

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for the production of pipe fittings, valve and cock bodies

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Production times for lateral valve housing illustrated:
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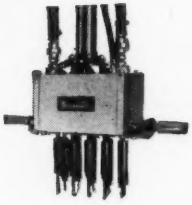

A Desoutter multi-studrunner plants 9 studs into an Austin cylinder block.

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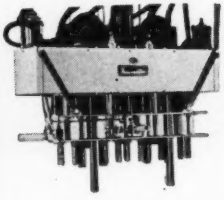

A Desoutter multi-nutrunner fixes 25 nuts on a Ford diesel cylinder head.

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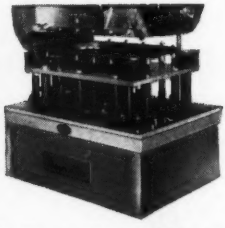
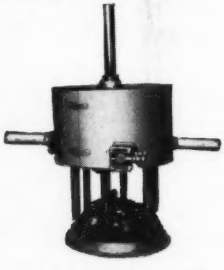


A Triumph Herald sump is put on by a Desoutter 16-spindle multi-nutrunner.

CHOUF!



A Desoutter multi-nutrunner assembles a Vauxhall clutch plate, or tightens the wheel nuts on a Rootes Group car. And so it goes on: the Desoutter CHOUF speeds mass-production, makes sweet music in industrialists' ears. And no wonder—everyone has a taste for that sort of music—and nearly everyone has something to play it on! CHOUF! (on a carburettor)...CHOUF! (or a light fitting)... CHOUF! (or a washing machine)... CHOUF! (or anything else that needs assembling).

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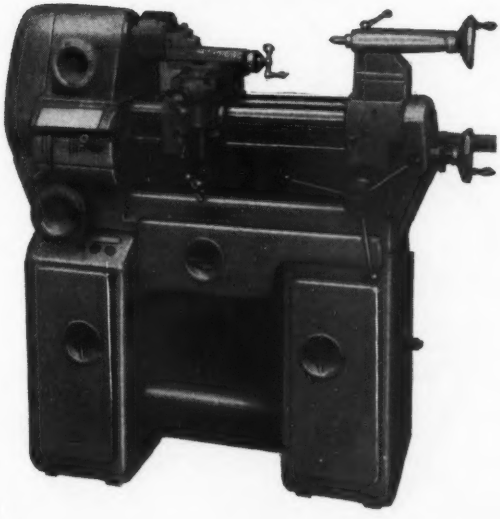

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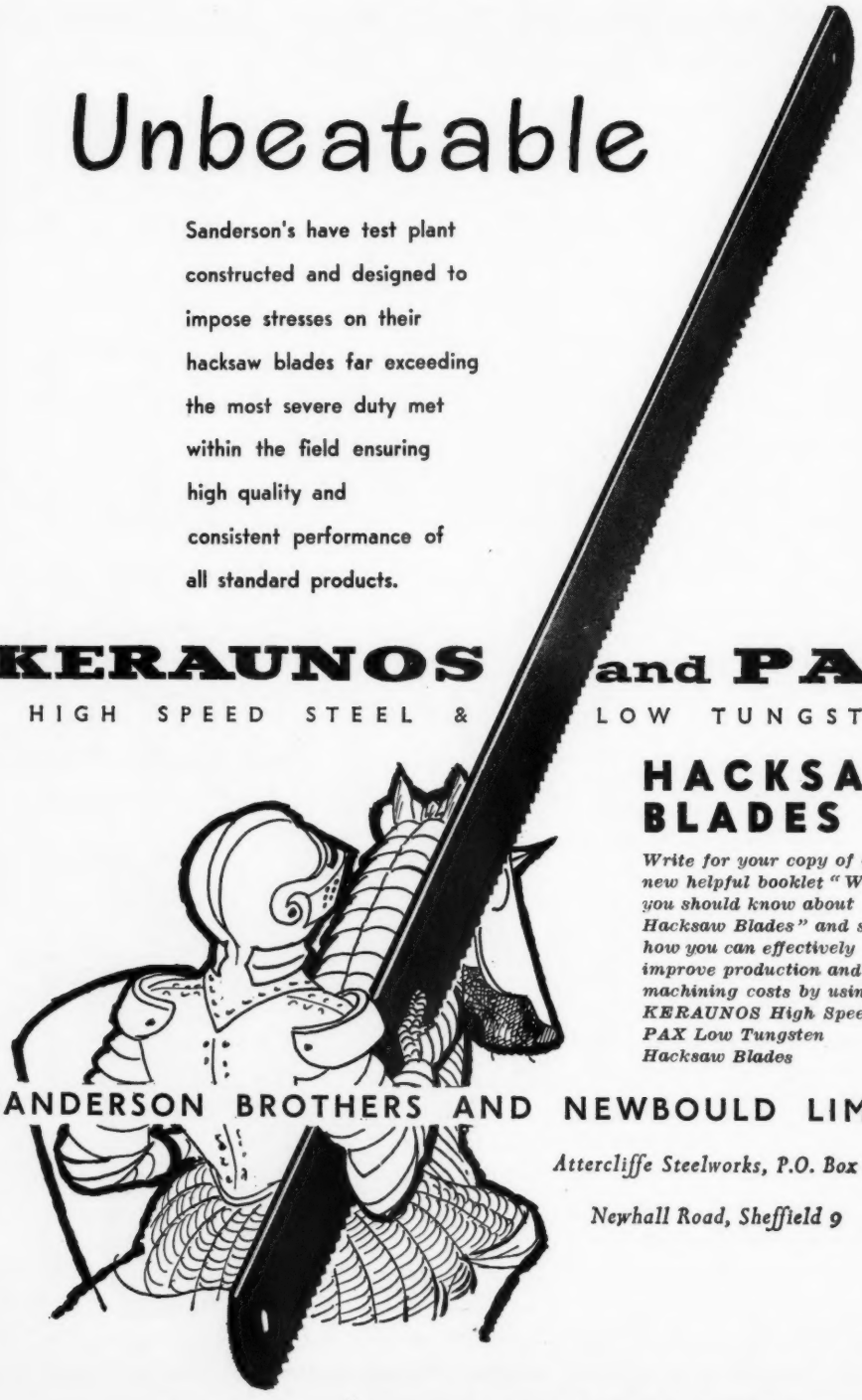

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NO. 61-6-9

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- Generating principle eliminates indexing.
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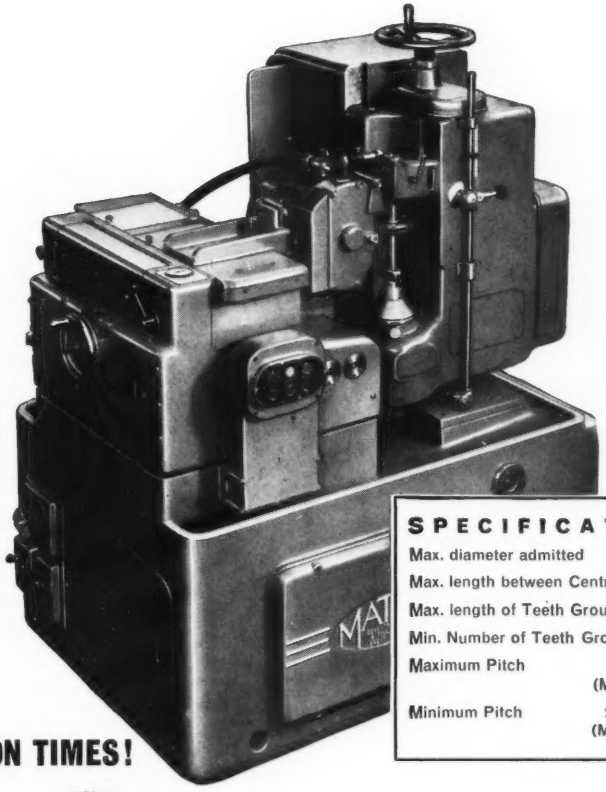
- Any diameter gears of similar pitch can be ground merely by altering the change gears for the number of teeth.
- Built-in wheel crushing unit is semi-automatic, type of pitch being governed by three easily fitted racks and segments.
- For gears of extreme precision, grinding wheel is diamond dressed by unit which is quickly interchanged with crusher.



SPECIFICATION

Max. diameter admitted	6″
Max. length between Centres	9″
Max. length of Teeth Ground	3″
Min. Number of Teeth Ground	12
Maximum Pitch	16 D.P. (Module 1.6)
Minimum Pitch	200 D.P. (Module·125)

Study these PRODUCTION TIMES!

4½ mins.
40 D.P. 120 Teeth.
3″ P.C.D.

12 secs. each
15 gears ground simultaneously
1.20 Module 40 Teeth.
48 mm. P.C.D.

2½ mins.
48 D.P.
24 Teeth.
0.5″ P.C.D.

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DUPLEX
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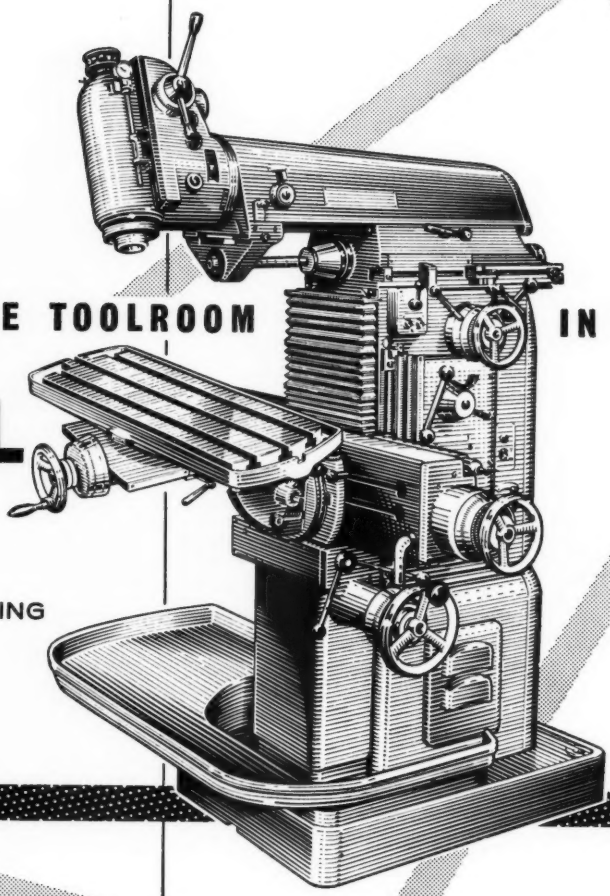

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One "U.S." Multi-Slide Machine has replaced as many as eight separate press operations on the production of a complex part. Two models are available which can be supplied completely tooled for the production of one or more components. If you manufacture formed stampings from material up to 3″ wide the "U.S." Multi-Slide Machine offers outstanding reductions in production costs. Substantial material savings, less parts handling, less floor space, are only some of the benefits.

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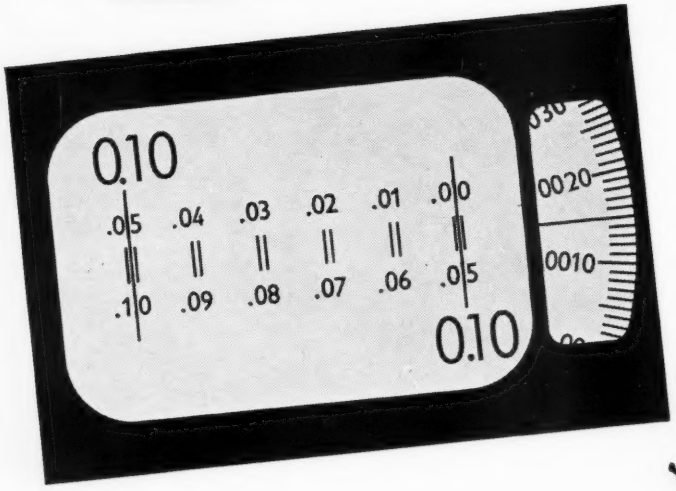
US 7A

The aba Precision Jig Boring Machine

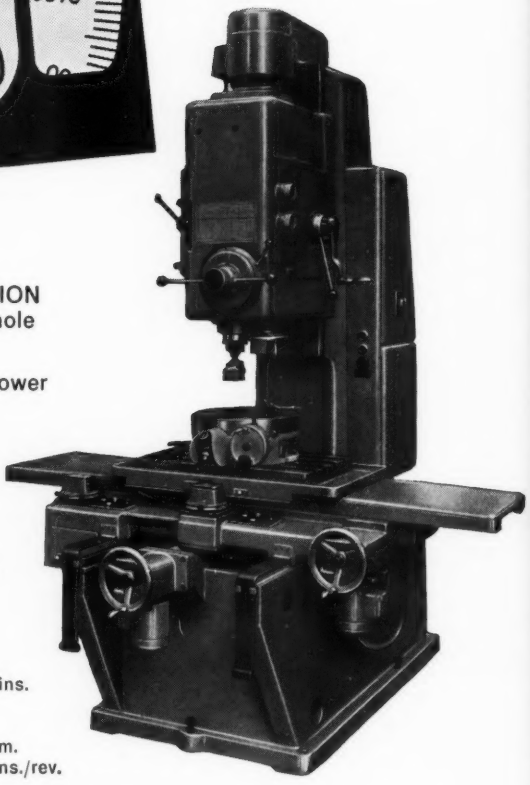
Model VLP600



now available with

PROJECTION OPTICS

by LEITZ



- Co-ordinate readings by LEITZ PROJECTION OPTICS with adjustment for setting from whole numbers.
- Twelve spindle speeds with four reversible power feeds for each speed.
- Automatic disengagement of feed at preset point.
- Hardened and lapped quill with spindle running in precision roller bearings.
- DC injection spindle brake with push button control.

BRIEF SPECIFICATION

Table size	28ins. by 16ins.
Longitudinal travel of table	26ins.
Cross travel of table	16ins.
Spindle speeds (12)	30-1420 r.p.m.
Spindle feeds (4)	0·0012-0·01ins./rev.

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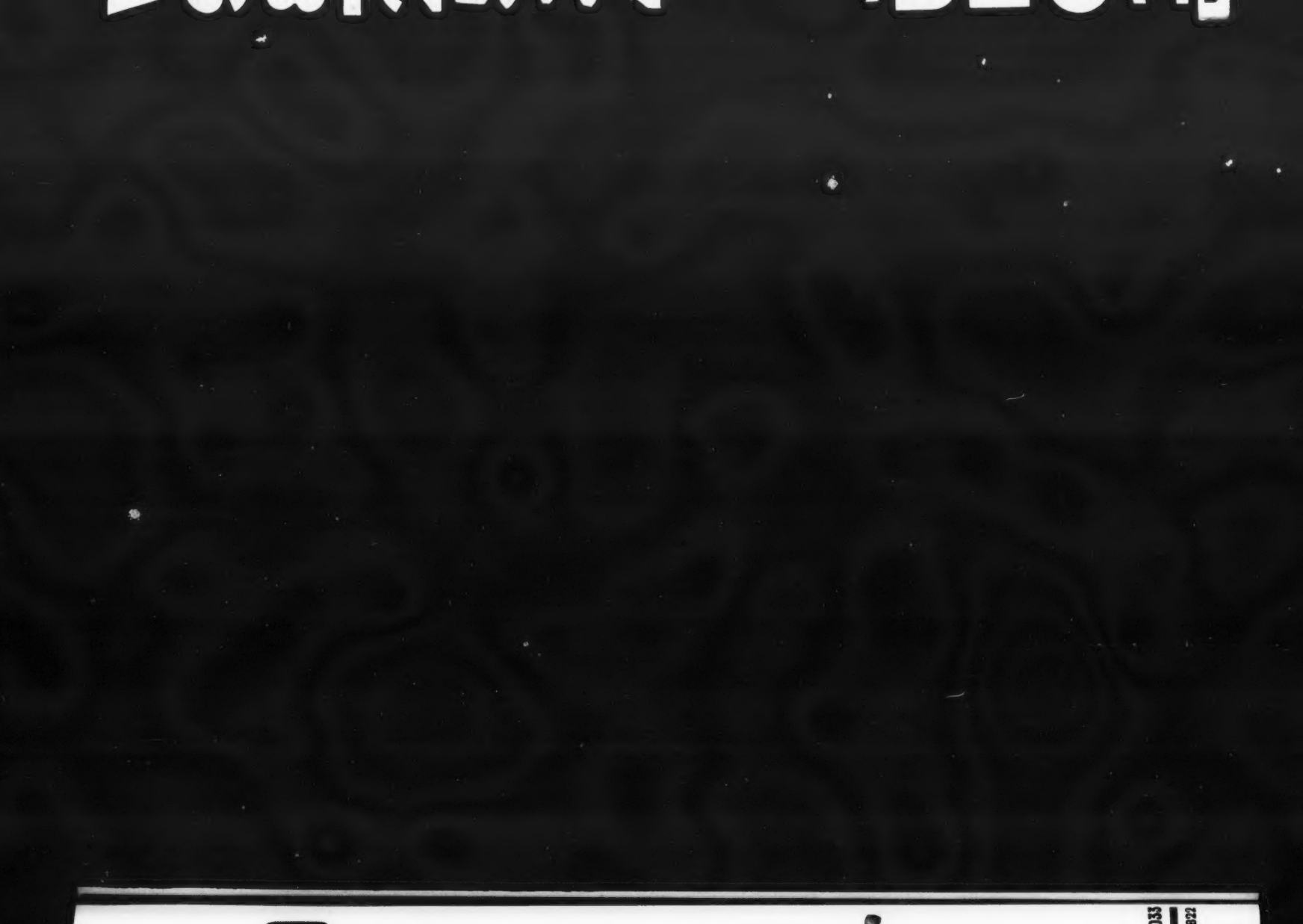
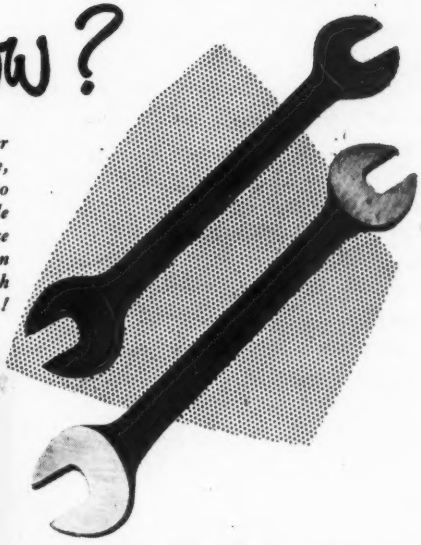
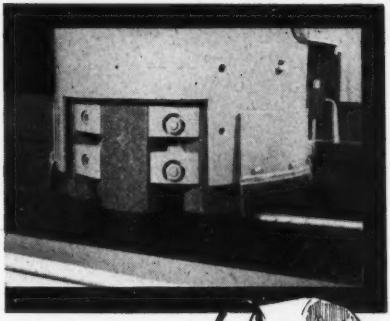


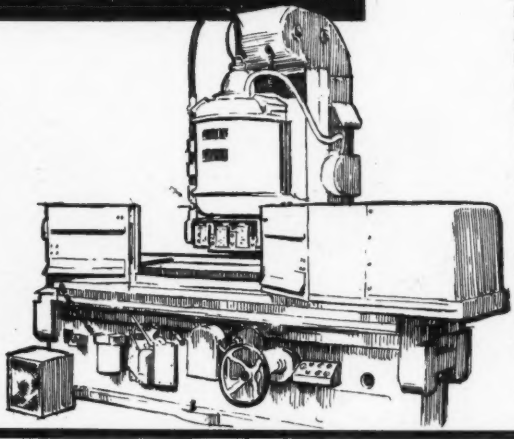
June 7

Do you know?

That you can get higher production with better finish at lower cost on vertical spindle, segmental surface grinding. By changing to ALOXITE vitrified segments, it was possible to reduce the abrasive cost of grinding these spanners by more than 5% — this is quite an item when you're grinding in quantities such as our customer does. And look at the finish!







Here are the production figures:

COMPONENT GROUND
Open-end spanners, 11" long x ⅜ and ½ Whit.

MATERIAL
EN47 chrome vanadium alloy steel.

ABRASIVE
Segments AA46 — J5 — VL.

NUMBER GROUND
200 dozen spanners per set of segments.

ABRASIVE COST
0·725 pence per dozen.

•

CARBORUNDUM can help you to achieve this kind of production and economy. And not only on segmental grinding. Whatever your grinding process, whatever your problem, we have experts who can advise on the best and most efficient use of abrasive materials. Write and ask for a representative to call.

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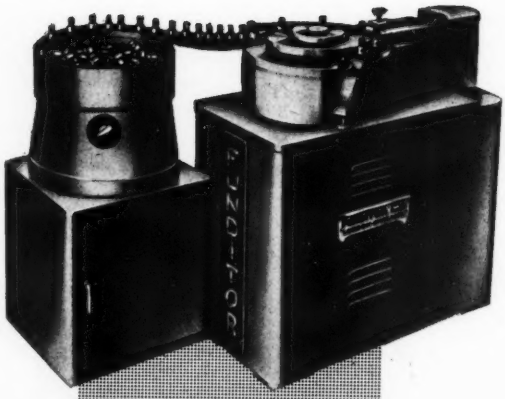
It's easy to create the right impression with



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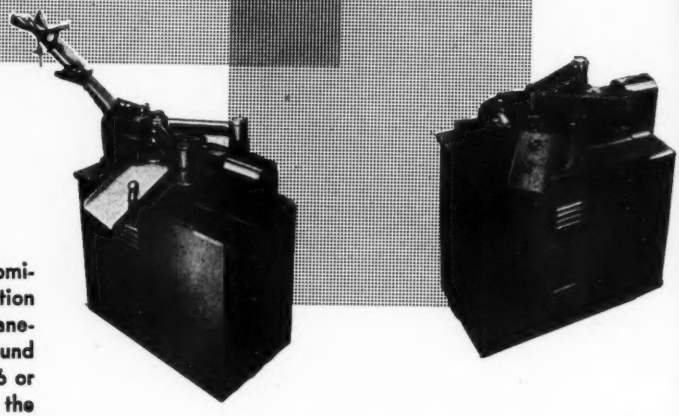

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IMMEDIATE DELIVERY FROM STOCK

MODEL JOH2

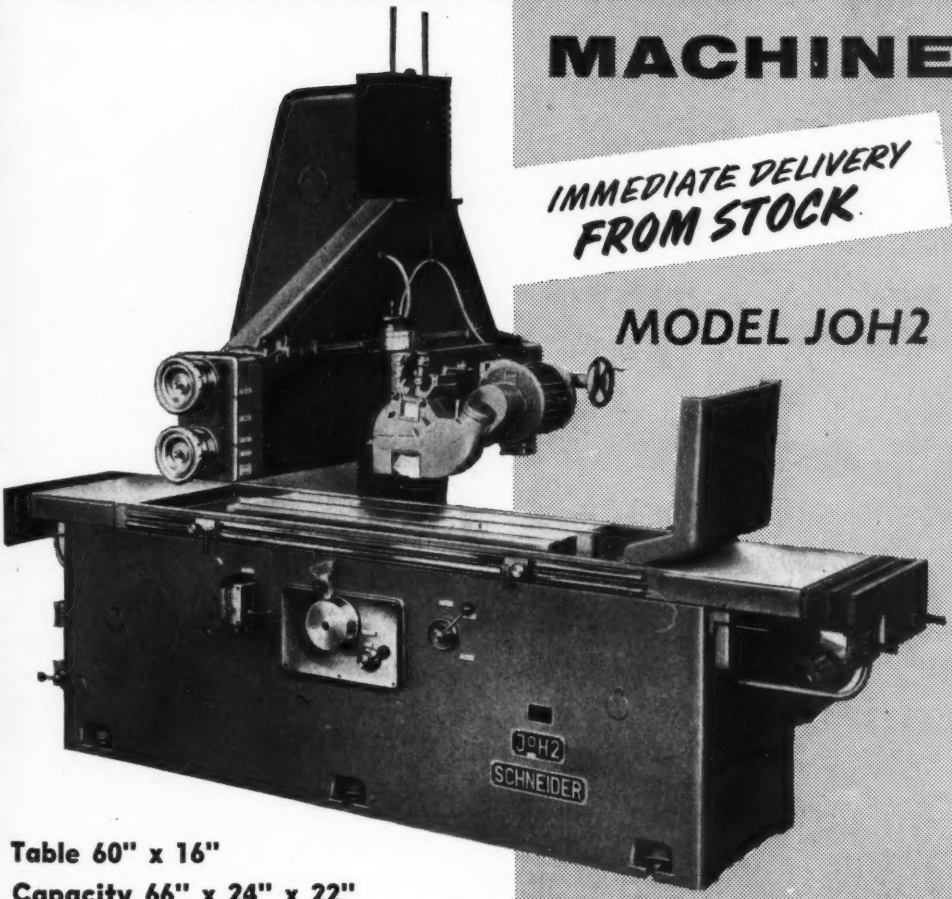

Table 60" x 16"

Capacity 66" x 24" x 22"

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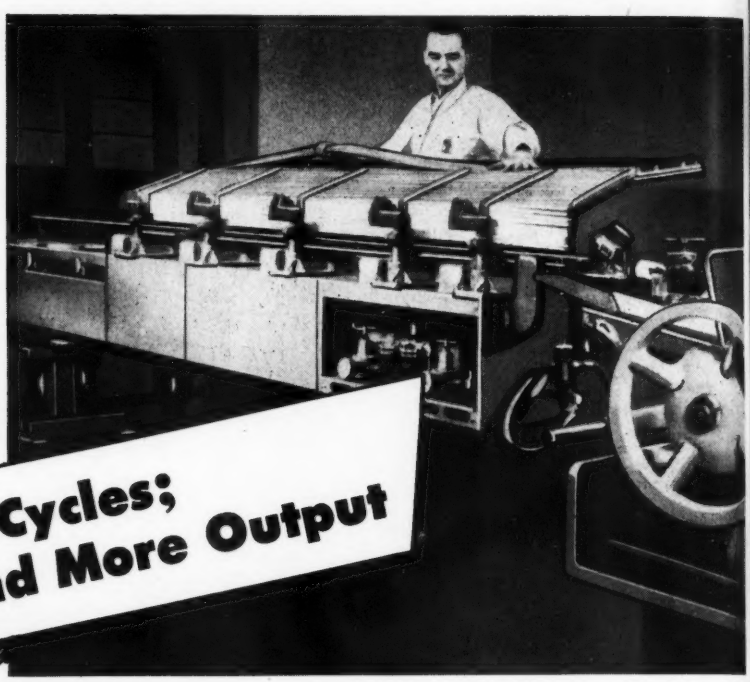

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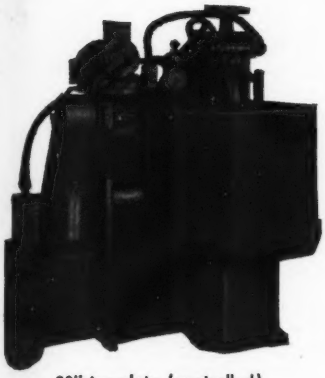

20" template (controlled)
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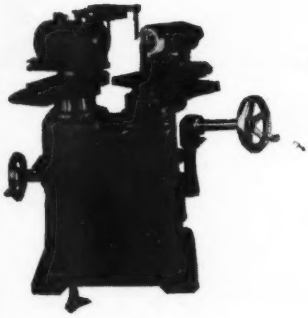

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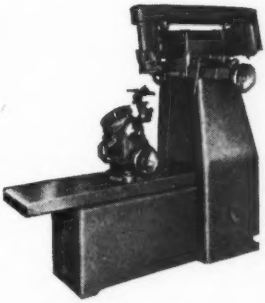
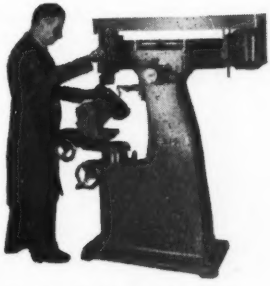


Oliver heavy-duty
'ACE' GRINDER



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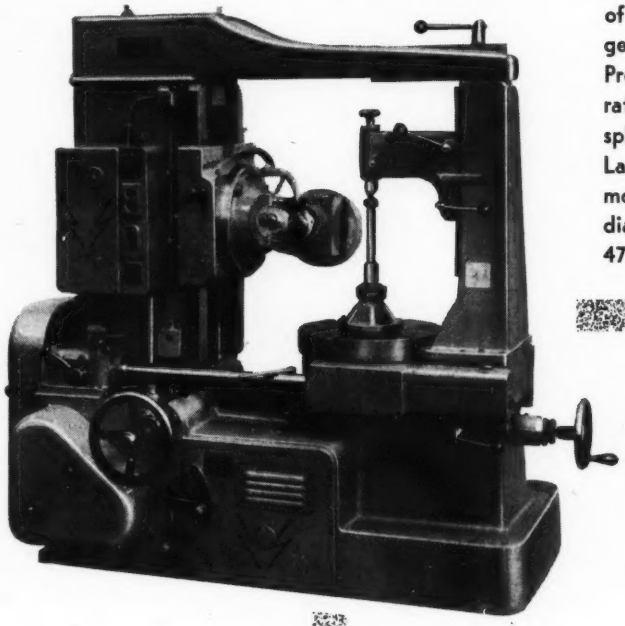
Larger machine available, model KF2, maximum gear diameter that can be hobbed 47".



ÄLMHULT AUTOMATIC GEAR HOBBER KF1

✳ ECONOMIC
✳ ACCURATE
✳ VERSATILE

SPECIFICATION

Max. gear diameter that can be hobbed	23½"
Min. centre distance, cutter spindle-table	1½"
Vertical travel of hob head slide	17 5/16"
Table diameter	19½"
Table worm wheel indexing diameter ...	16"

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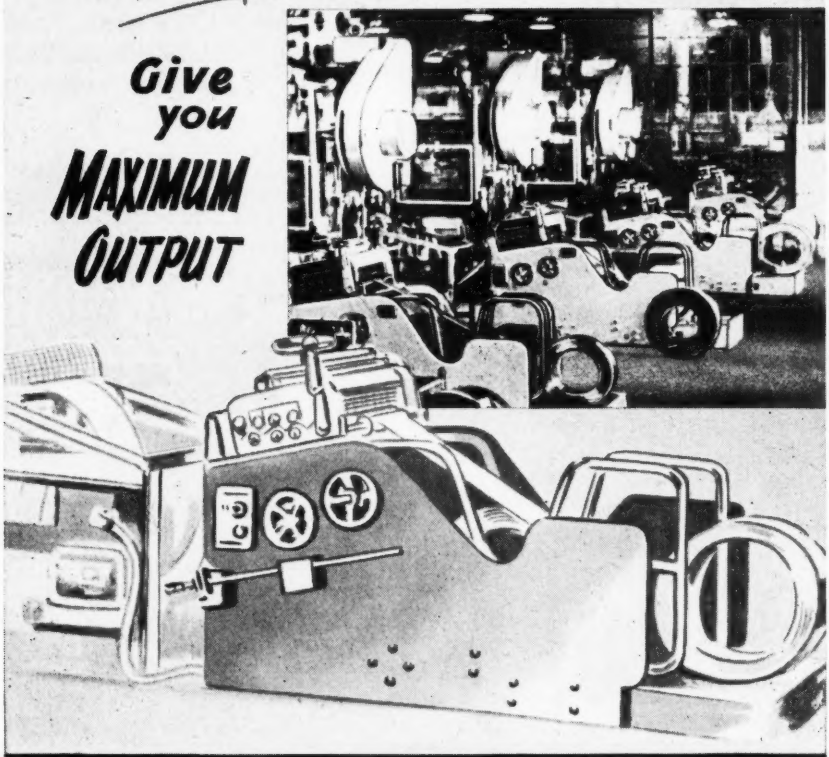

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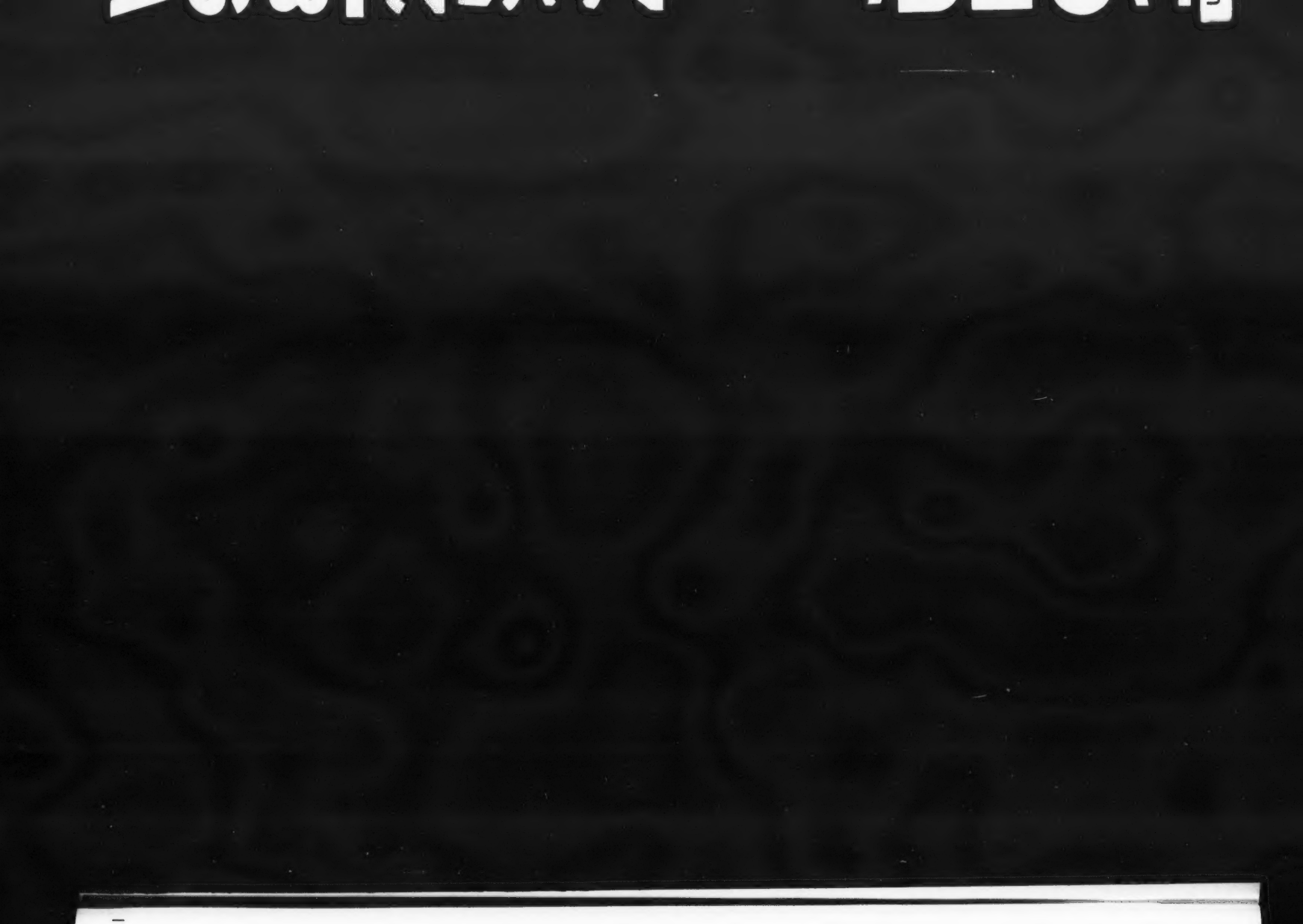

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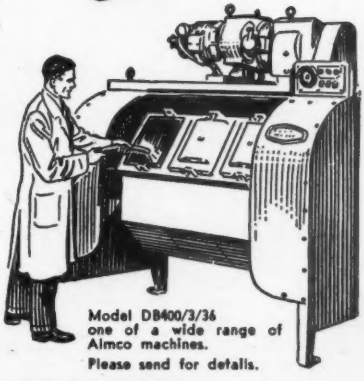

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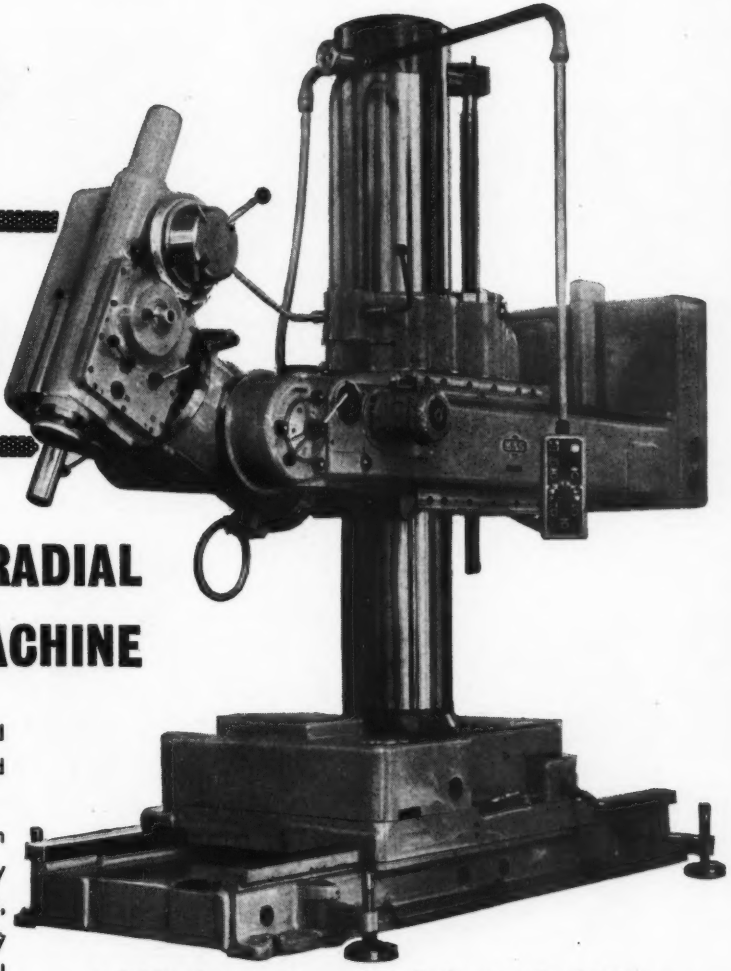

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For drilling, reaming and thread cutting large and bulky workpieces.
Ideal for heavy duty work in Production and Assembly shops such as bridge building, boiler construction, railway and shipbuilding yards. All movements are easily controlled by push-buttons on a pendant arm.

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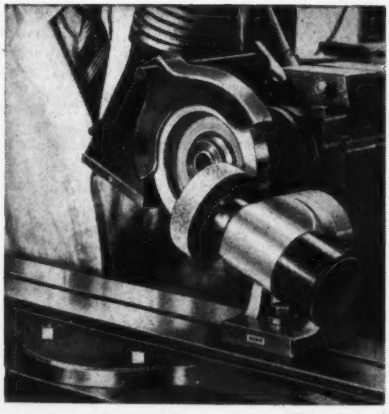

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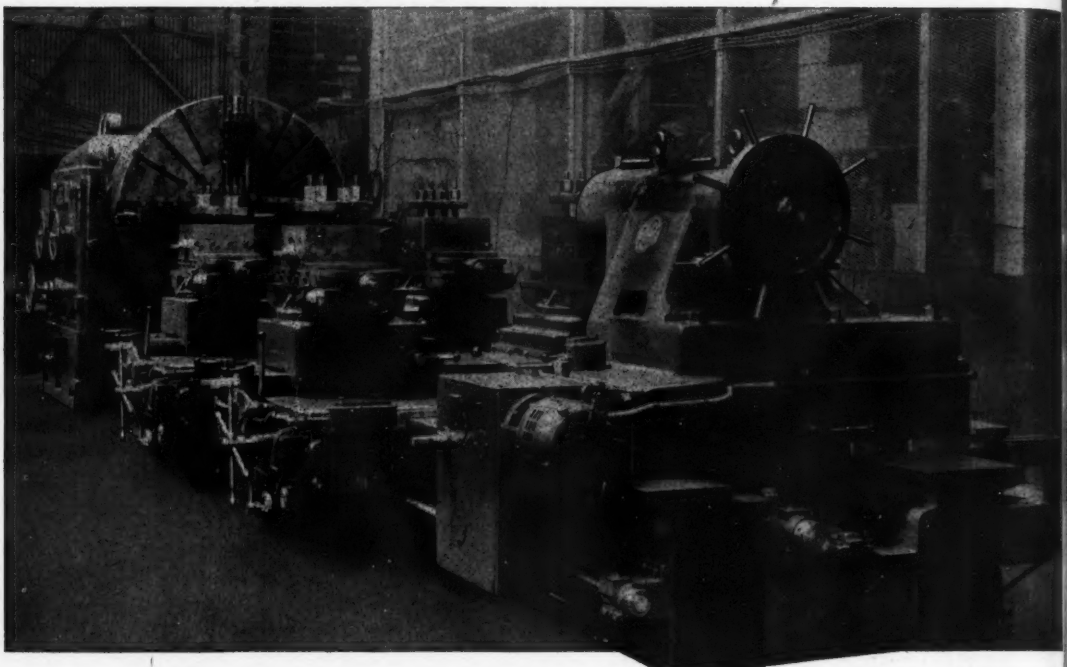

CLYDE BUILT SMT GLASGOW MACHINE TOOLS

HEAVY DUTY LATHES

This 36in. height of centres machine is typical of the heavy duty lathes which we manufacture, from 21in. to 60in. height of centres. In addition, we have available surfacing and boring lathes and sliding bed break lathes. All are built to the highest standards of accuracy and with the best materials and workmanship. In general, the range is designed for the heaviest class of work, but we also build some machines intended for light work on large and heavy components.

The lathe illustrated has two saddles, each with two tool posts and quick power traverses are applied to all motions. These traverses and the main drive are controllable from push button stations on each saddle, ensuring the maximum speed and ease of operation. Different ranges of spindle speeds are available to suit the class of work to be done and screw cutting can be provided or omitted as desired. Likewise power feed to the top slides is optional and, if specially required, a screw cutting motion is possible at this point.

The photograph shows clearly the massive construction of our lathes, the proportions of the bed being shown very clearly. The narrow guide for the saddle is on the front shear. The spindle bearings are of very ample size to deal with the loads involved and all fast running shafts are carried on ball or roller bearings. The loose head is of massive design and carries a running spindle. We have a number of types of loose head, including one with a full scale spindle, complete with chuck.

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We invite your enquiries for large lathes as well as the other machines which we build and we are always happy to arrange for a visit of one of our technical representatives to discuss your requirements and problems.

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PLANERS

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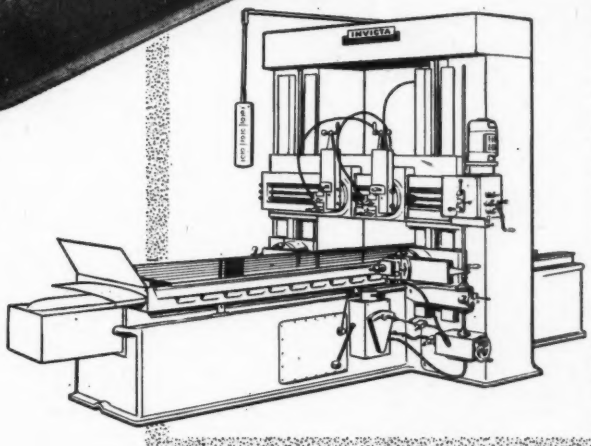
- **Infinitely variable table speeds with quick return.**
- **Hydraulic tool lift.**
- **Automatic lubrication of bed ways.**
- **Rapid vertical traverse of cross rail standard.**
- **Centralised controls.**

TWELVE DOUBLE COLUMN MODELS
8' x 4' x 3' — 14' x 5' x 3'



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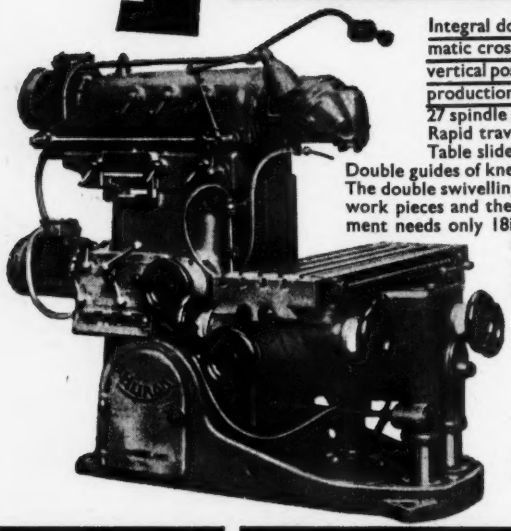
HURON SUPER UNIVERSAL MILLERS



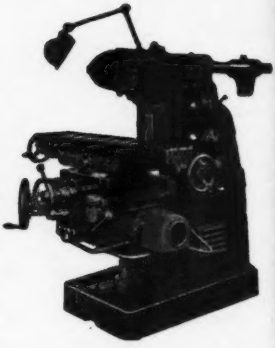
Integral double swivelling universal head provided with 27½in. automatic cross feed by the sliding ram, can be set to the horizontal or vertical position, or to any angle instantaneously—permits the heaviest production cuts. Head can be retracted completely from table line. 27 spindle speeds from 30 to 2,066 r.p.m., 27 feeds from $\frac{1}{16}$in. to 30in. Rapid traverses in all directions. All operating controls duplicated. Table slides directly in the knee without cross movement or swivel. Double guides of knee permit components in excess of 1½ tons to be machined. The double swivelling universal head requires an opening of only 14in. to enter work pieces and the whole sliding ram with its 27½in. automatic cross movement needs only 18in. clearance. OPTIONAL EXTRA FEATURES: Mounted spacing casting assemblies providing additional 8in. capacity under spindle. 26in. wide 8 T-slot tables and 39⅜in. automatic cross feed of sliding ram with special heavy duty knee and front operating position.

Type	Table	Automatic Feeds Long	Cross	Vert.
KU4	56⅛in. × 15⅝in.	43½in.	27½in.	19⅝in.
KU5	64⅛in. × 15⅝in.	51½in.	27½in.	19⅝in.
KU6	78⅛in. × 16½in.	59in.	27½in.	19⅝in.
KU55	64⅛in. × 26in.	51½in.	38⅛in.	18⅝in.
L83	157in. × 59in.	118in.	39⅜in.	59in.

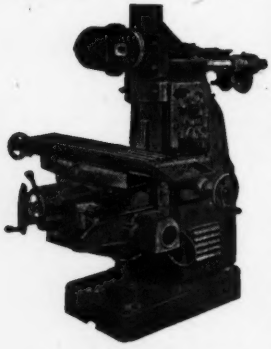
Type 'L' Open-side Traversing Head Universal Miller will mill, bore, slot and drill the largest work-pieces at one setting. The unique design permits greatest variety of operation on large work-pieces; the component remains stationary on the large work-table. Upright slides full length of base table and the sliding ram moves vertically and horizontally.

DUFOUR UNIVERSAL MILLERS

WITH DOUBLE UNIVERSAL SWIVELLING HEAD, RETRACTABLE SLIDE BRACKET AND SPACING CASTING GIVING 26" DAYLIGHT ON No. 59 AND 21" ON No. 61



FOR ALL MODELS Direct reading dial change for speeds and feeds. All parts subject to wear hardened and ground and completely interchangeable. Built to closest tolerances. Rapid traverses in all directions. Table swivels 30°. No. 40 taper for main horizontal spindle, double swivelling universal head, dividing head and rotary table. Hardened and ground centre guide for slideways. Twin overarms. Double swivelling sliding spindle heads with speeds 53-3000 r.p.m. Double swivelling universal head on retractable slide bracket providing with 5½in. Spacing Casting Drive assembly on 59 Machine 26in. daylight, and 21in. on No. 61.



MODELS 53 & 61. 16 universal head spindle speeds 21-1600 r.p.m.; 8 horizontal spindle speeds 21-1180 r.p.m.; 8 automatic feeds ½-18¾in.

MODEL 59. 36 universal head spindle speeds 14-1780 r.p.m.; 12 horizontal spindle speeds 21-1180 r.p.m.; 16 automatic feeds ½-20in.

MODEL 54. Automatic cross feed of universal head 20in.; 18 universal head spindle speeds 12-1500 r.p.m.; 36 horizontal spindle speeds 6-1500 r.p.m.; 18 automatic feeds ½-23½in.

Type	Table	Automatic Feeds Long.	Cross	Vert.
53	43½in. × 9⅝in.	27½in.	9⅝in.	15⅝in.
61	47½in. × 10⅝in.	30½in.	9⅝in.	15⅝in.
59	51⅛in. × 11⅝in.	34½in.	11⅜in.	21⅛in.
54	67in. × 14⅝in.	43½in.	14⅝in.	20⅝in.

Send for full particulars of our very extensive range of these machines; ask for demonstration.

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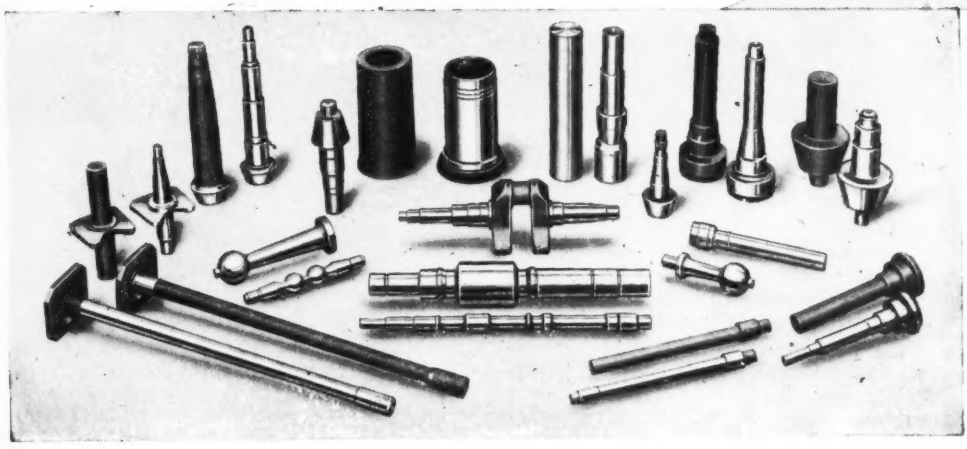

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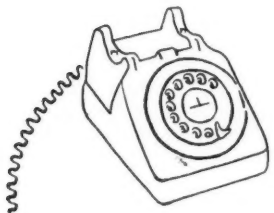

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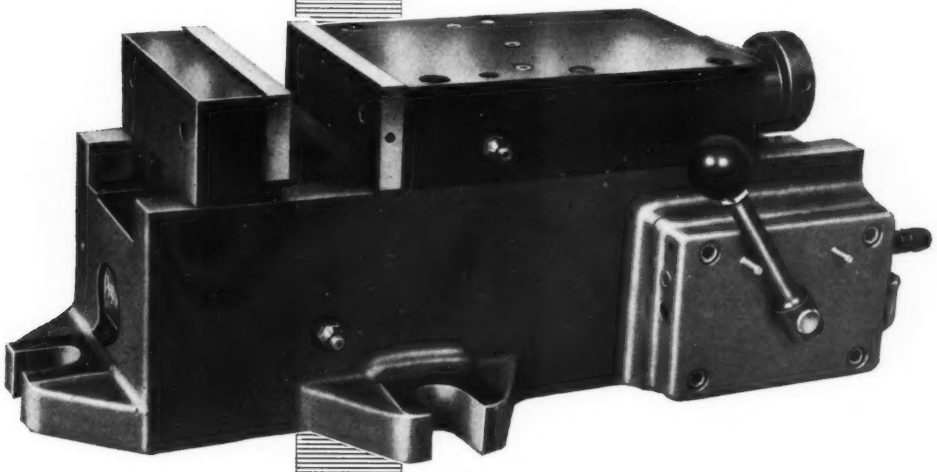

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Width of Jaw	4⅛″	6″
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Power Movement	½″	½″
Gripping Force at 80 P.S.I.	4,800 lbs	7,700 lbs
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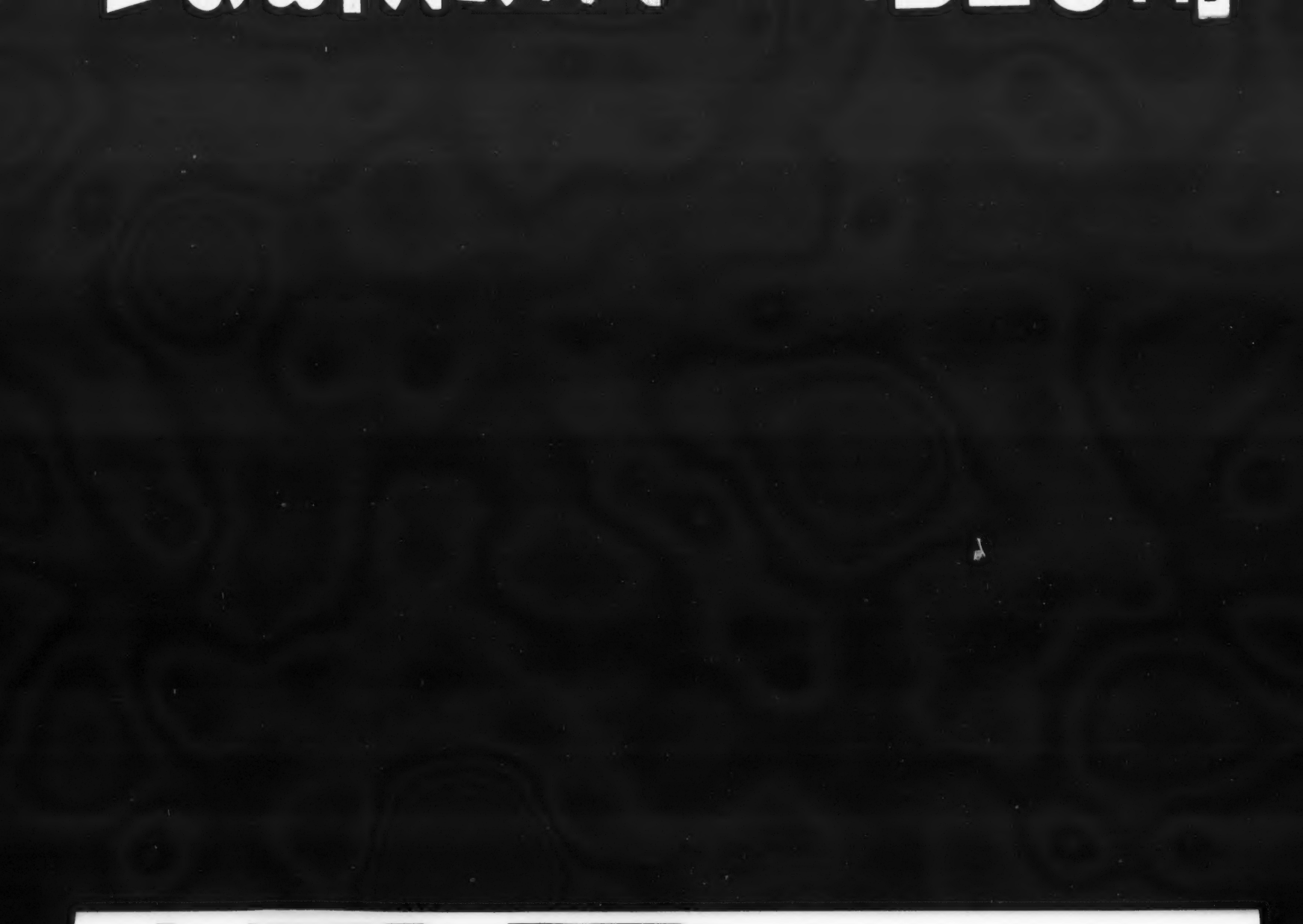

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HAVE EXCEPTIONALLY LONG LIFE

THEY CAN BE RE-GROUND 5 to 10 TIMES

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These Shell Reamers fit our standard range of arbors.

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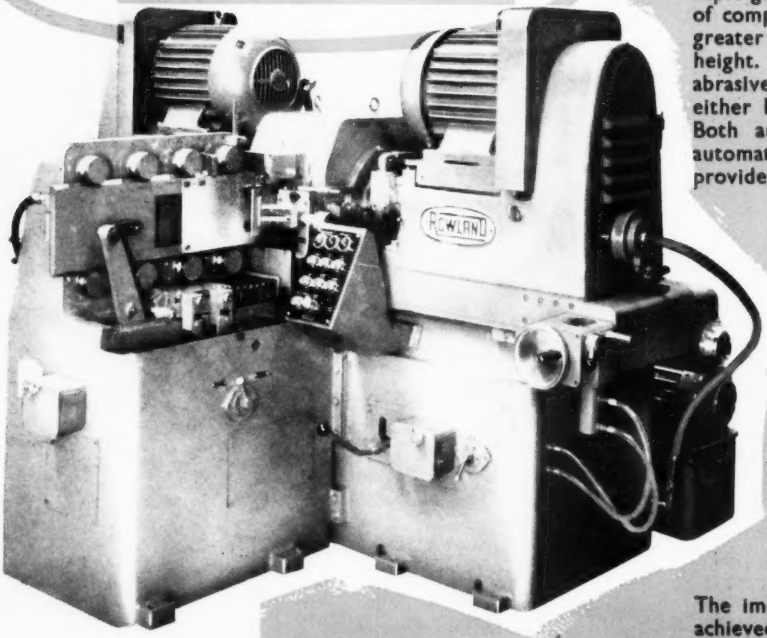

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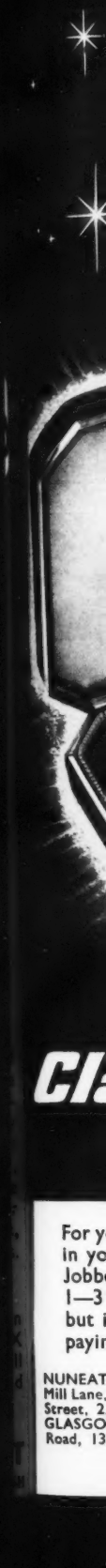
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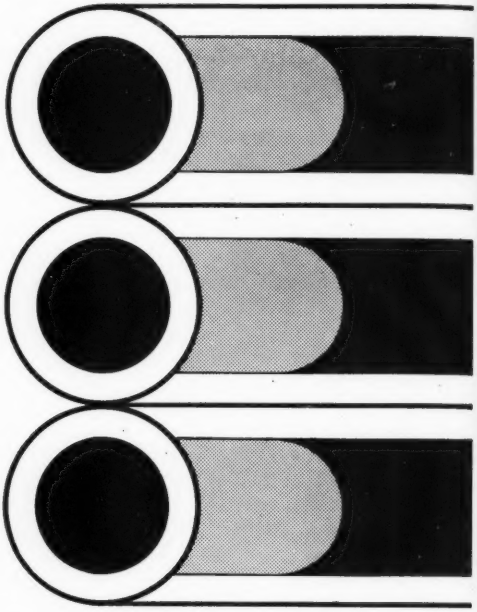
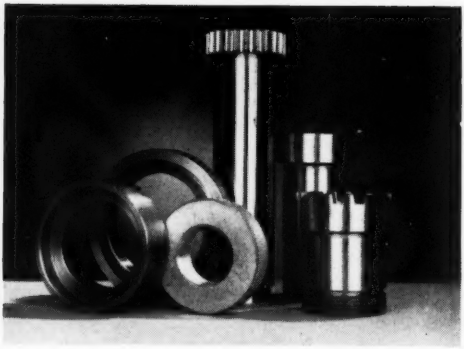
The saving is inside





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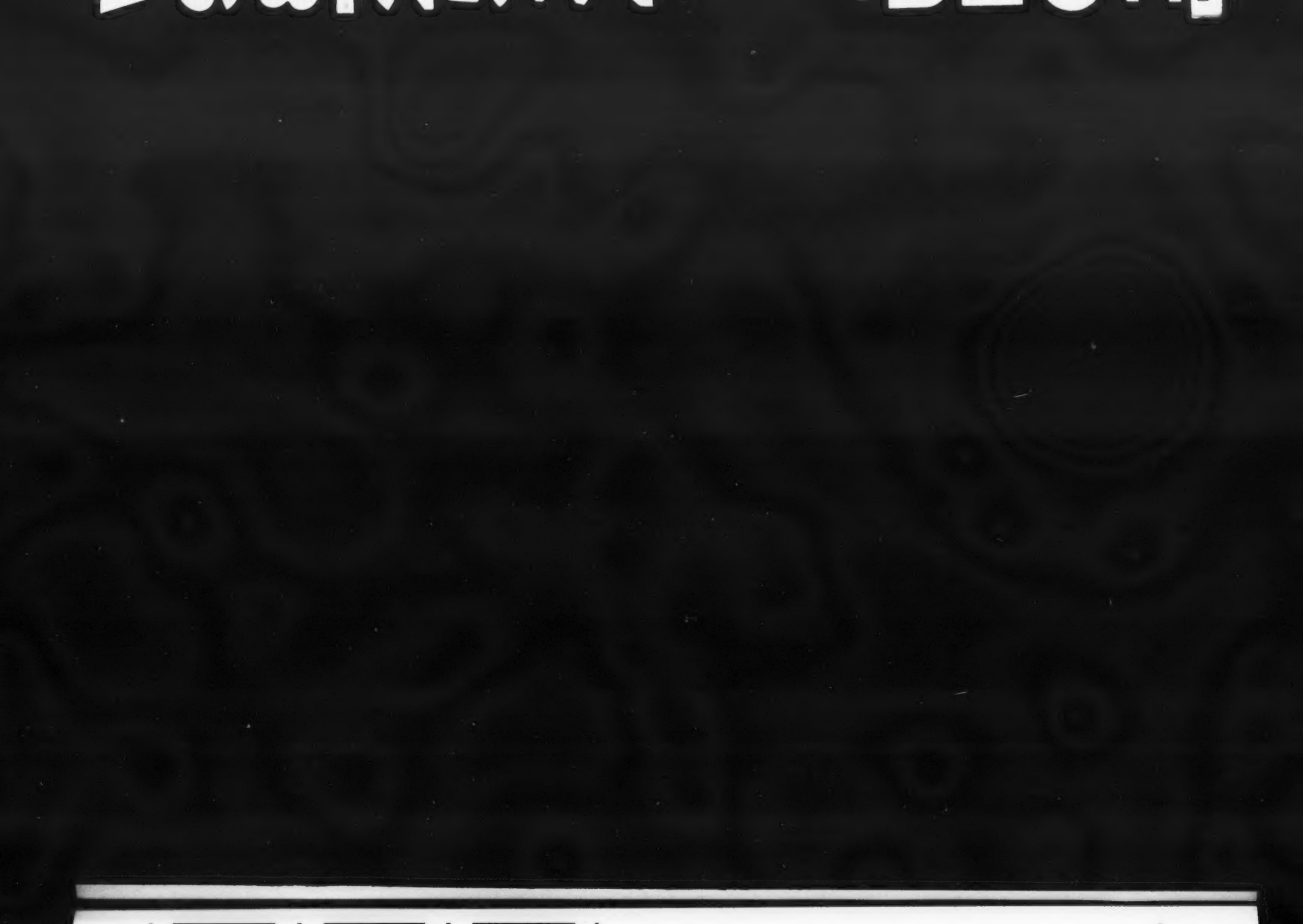

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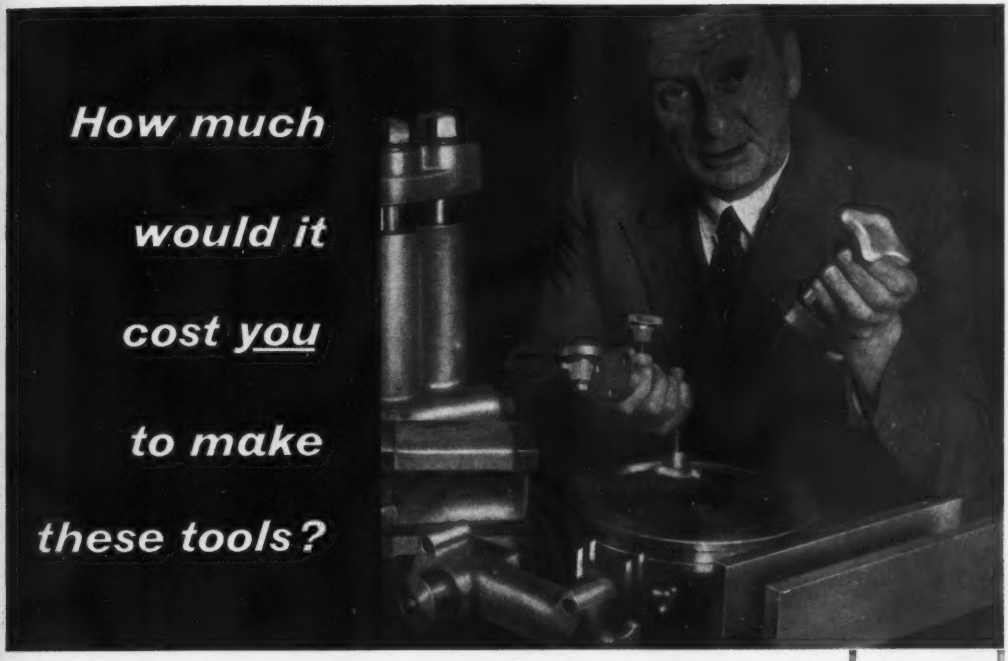

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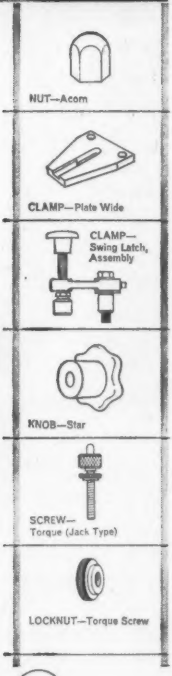

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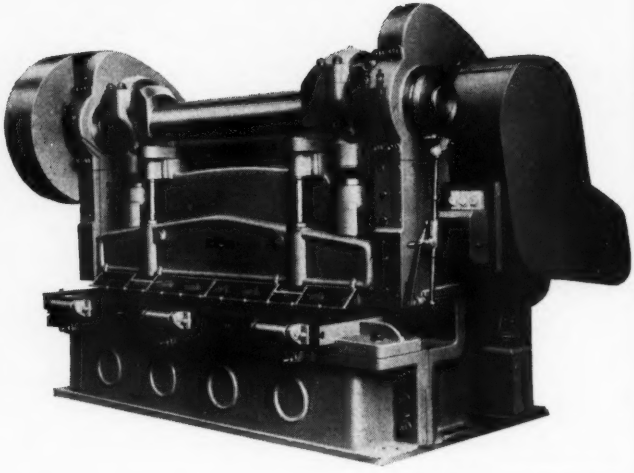

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⅜in. capacity **GUILLOTINE** with a cutting width of 8ft. 4⅜in. Complete with hold-down and calibrated rack and pinion adjusted back gauge.

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Both machines are motorised for 415 volts, 3 phase, 50 cycles supply.

Fuller details are available on illustrated specification sheets; please ask for copies.

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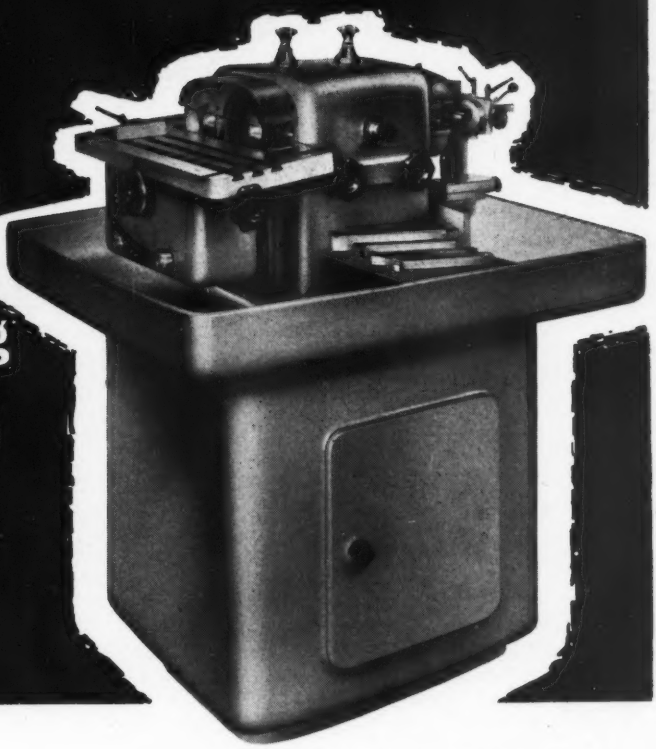
4 wheel combination carbide tool grinding and lapping machine



Specification

To take grinding & Lapping Wheels.	6in. dia.
Power of main motor.	1 h.p.
Size of inclinable table.	24in. by 9¾in.

Attachments Available. for Chip Breaker groove grinding, Nose radius grinding, twist drill grinding. Also oversize Table, Grinding Wheels, Lapping Wheels, Lighting equipment.

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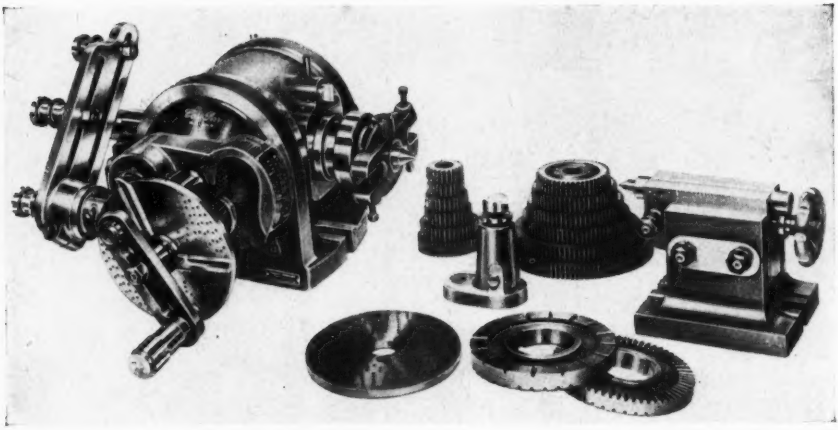
HIGH PRECISION

UNIVERSAL DIVIDING HEADS

MODEL ALFA



SPECIFICATION	ALFA 1	ALFA 2	ALFA 4	ALFA 5	ALFA 7	ALFA 9
HEIGHT OF CENTRES	4¼"	5¼"	5⅞"	6¼"	7"	7⅛"
BORE OF HOLLOW SPINDLE	⅝"	1⅛"	1⅛"	1⅛"	1⅛"	1⅛"
MORSE TAPER IN SPINDLE	No. 3	No. 4	No. 4	No. 4	No. 4	No. 4
MORSE TAPER IN TAILSTOCK... ...	No. 1	No. 2	No. 2	No. 2	No. 2	No. 2
DIVISION RATIO	1 : 40	1 : 40	1 : 40	1 : 40	1 : 40	1 : 40
DIVISIONS OBTAINABLE...	2-400	2-400	2-400	2-400	2-400	2-400
APPROXIMATE WEIGHT...	114 lbs.	161 lbs.	255 lbs.	260 lbs.	270 lbs.	280 lbs.
PRICE	£160	£180	£250	£275	£295	£310

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Superb performance
Attractive price
Quick delivery

All models complete with Standard Equipment including :

- Cos-par Universal Dividing Head
- Vertical Milling Attachment
- Arbor
- Front Support Braces

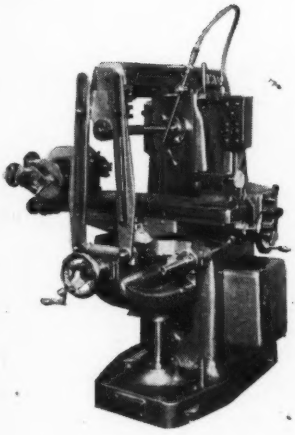
Specification :

	0	1	2
Table	34″ × 8¼″	39⅜″ × 9″	48″ × 11″
Long. Trav.	20″	26″	29″
12 Speeds	32-1000	60-1200	40-2000
Spindle Nose	No. 40	No. 40	No. 40
PRICE ★	£880	£1100	£1825

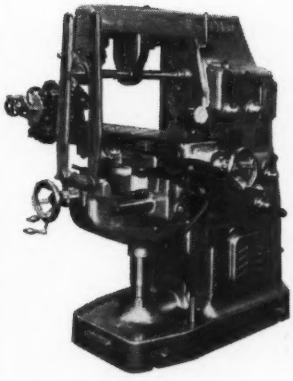
TEST

UNIVERSAL MILLING MACHINES

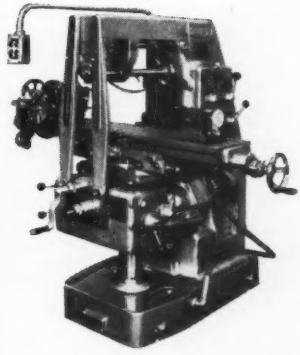
Model 0



Model 1



Model 2



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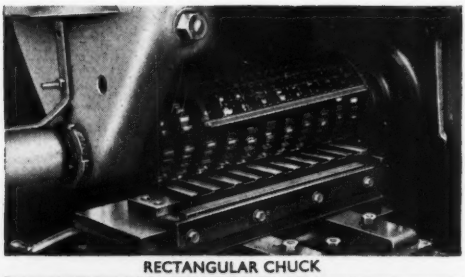

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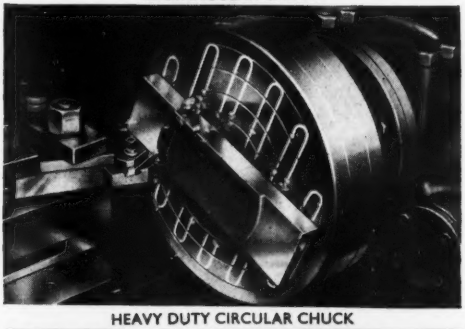
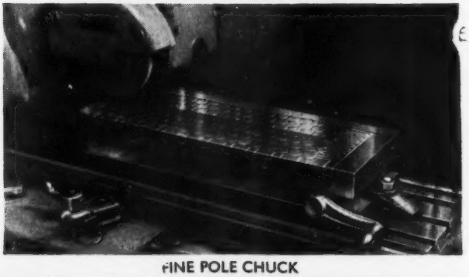


HEAVY DUTY CIRCULAR CHUCK



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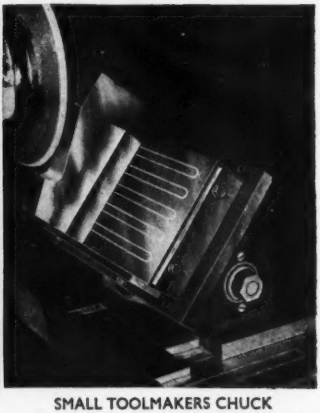

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300,000 RPM

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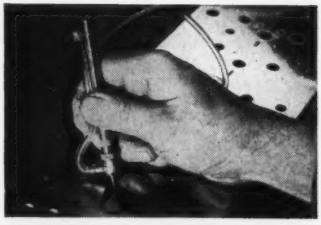

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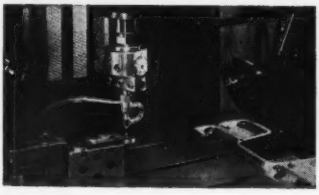

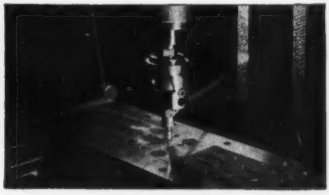

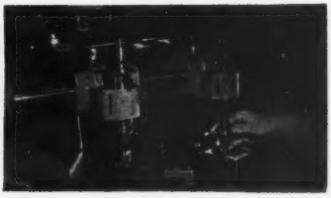

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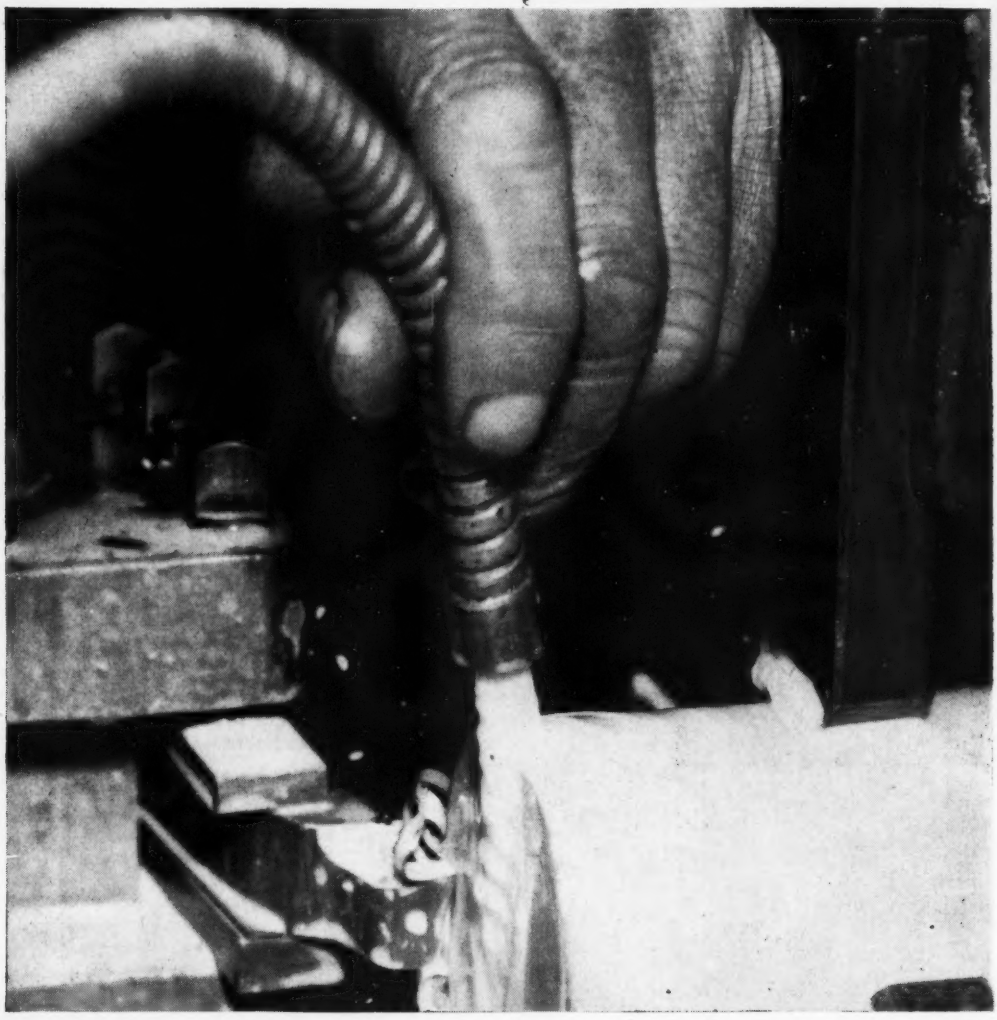

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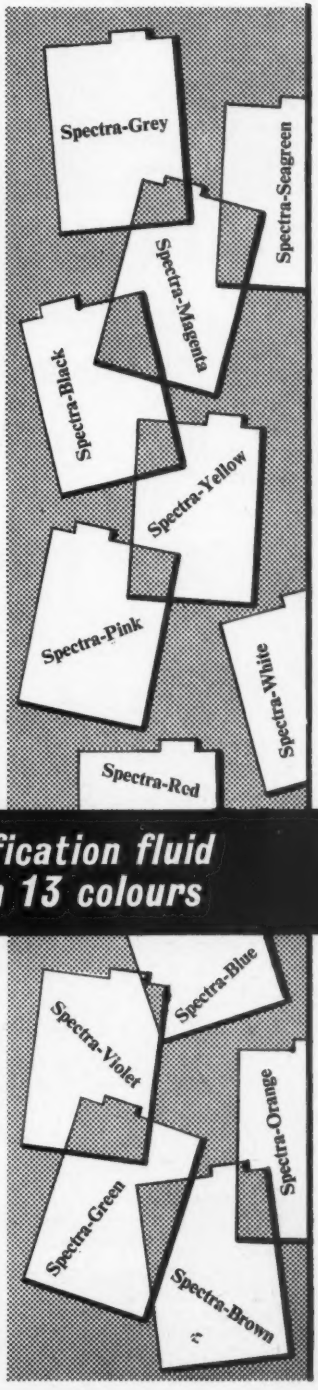

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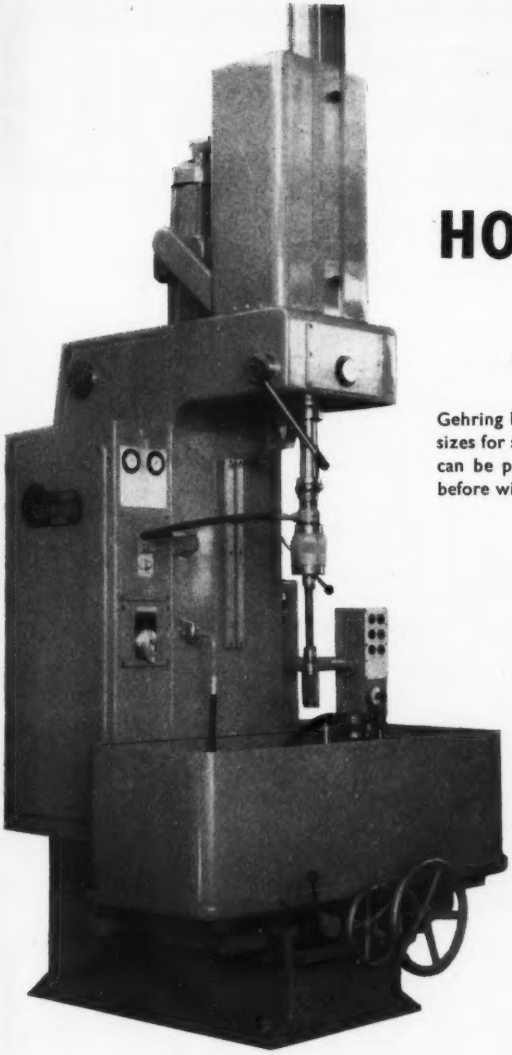

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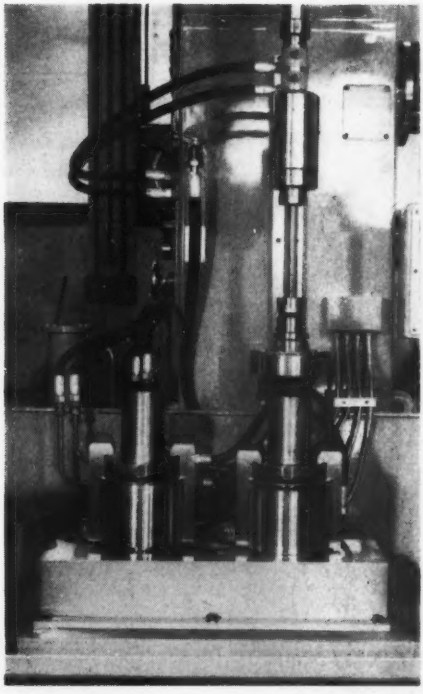

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The illustration on the right shows an automatic two-position table with automatic liner clamping fixture. Rotary tables and transfer equipment for incorporation as part of a transfer line can also be provided.

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Tecalemit Ribbon Elements filter to maximum purity

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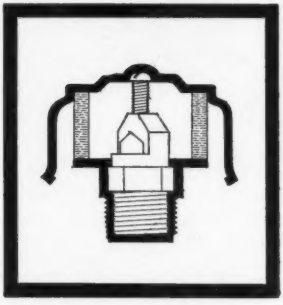
Tecalemit Breathers provide pure air cheaply and efficiently



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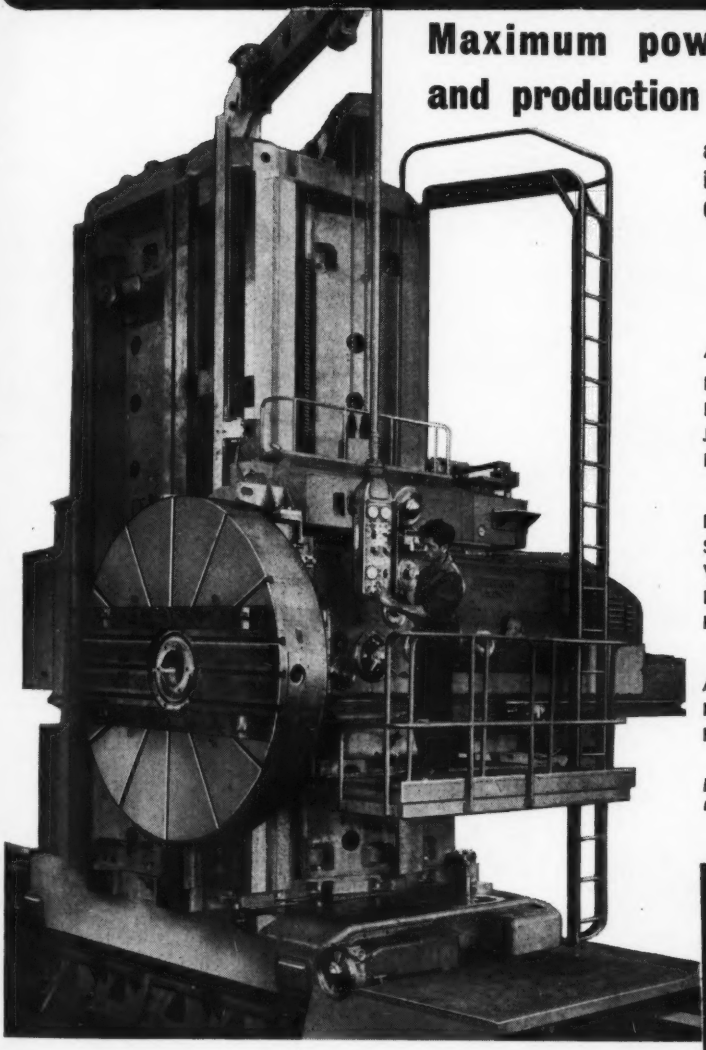

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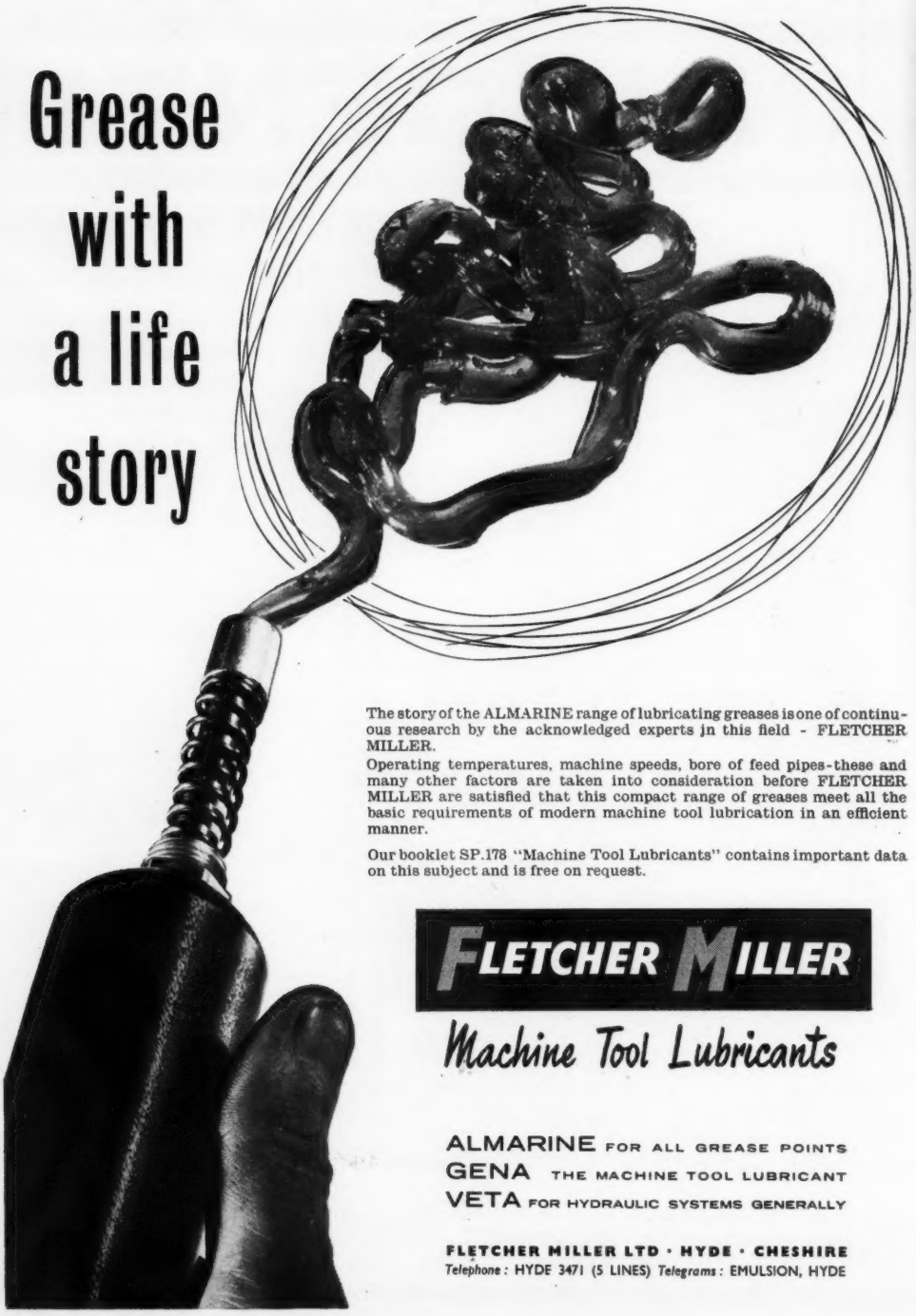

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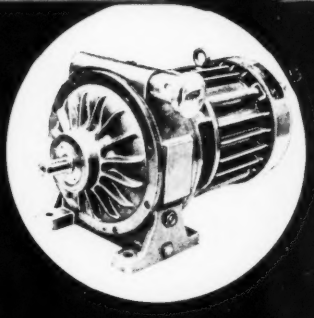

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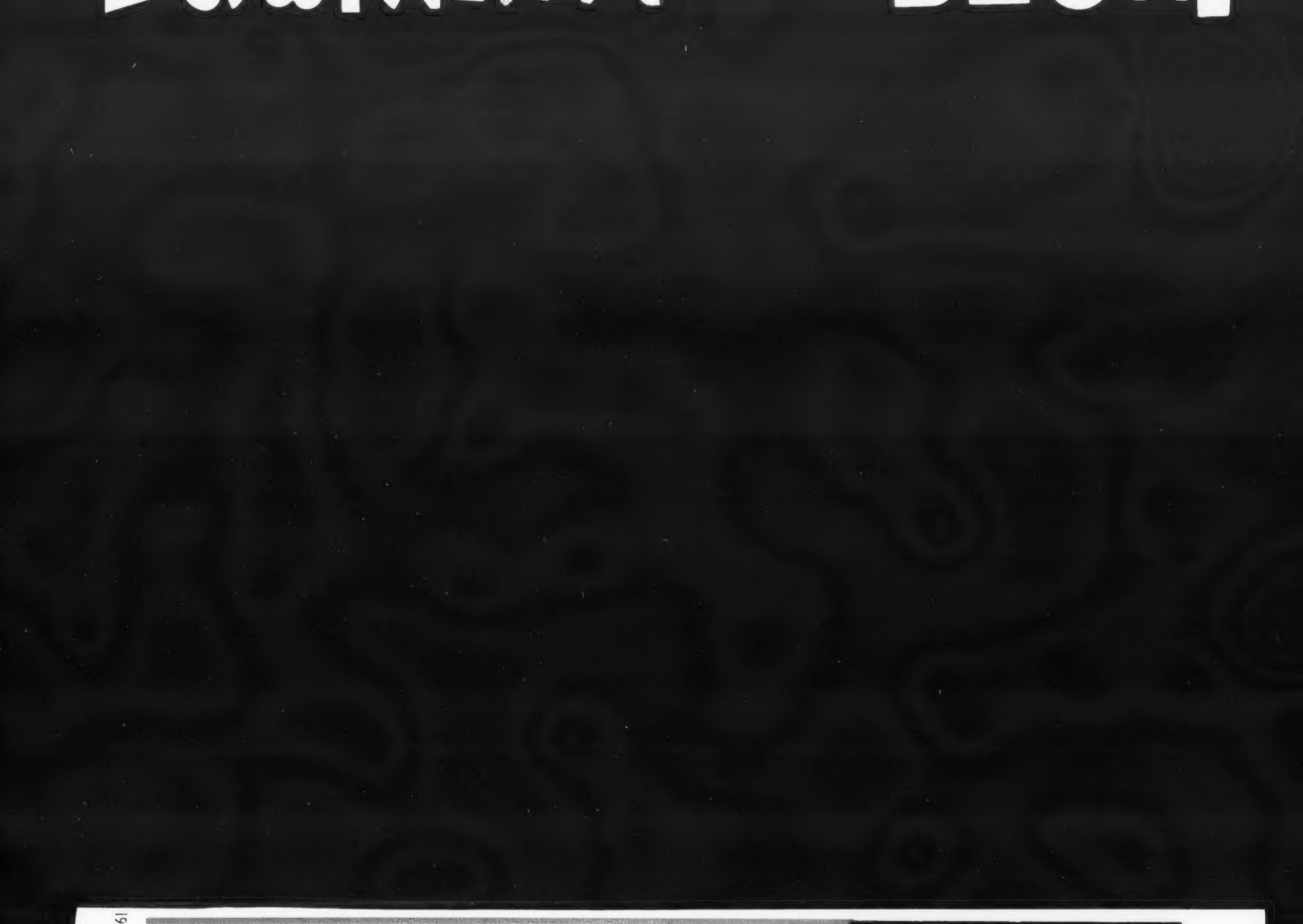

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For better service from any air line

Any air control system incorporating cylinders and valves, or which operates tools and equipment, will give better service if the air is properly filtered, the pressure is regulated to the job and adequate lubrication is provided. The Schrader LUB-AIR-ATOR is a combination of three units which perform these functions automatically, ensuring better and safer operation and longer, care-free service. It prevents wastage of high-pressure air and reduces frictional wear on installations and equipment. The LUB-AIR-ATOR is easily maintained. It has no moving parts to wear and can be serviced without disturbing the pipe connections. Available in three sizes with various flow capacities.

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Provide lubrication protection for cylinders, valves and pneumatic equipment. External flow adjustment. Visible oil level. Refilled without shutting off the air.

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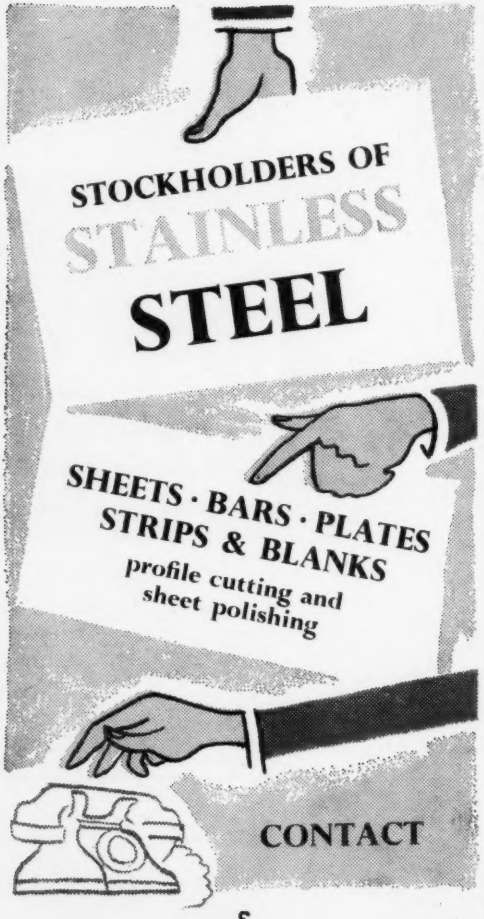

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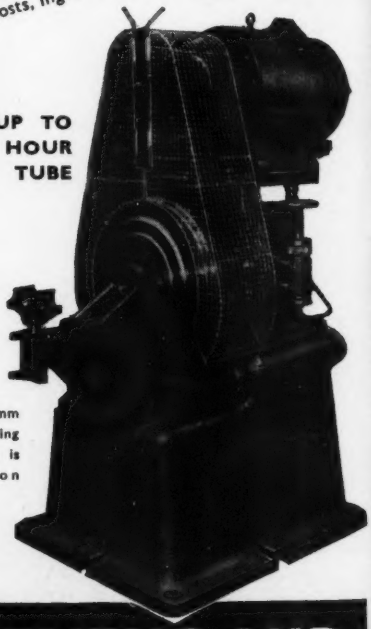

A short 16mm film describing this machine is available on application.

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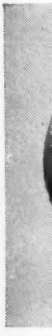

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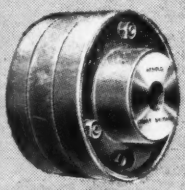

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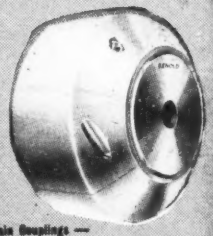

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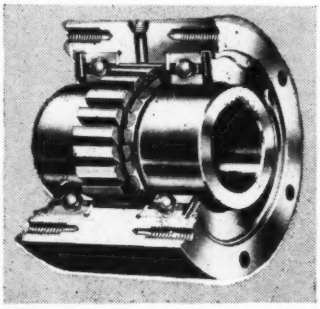

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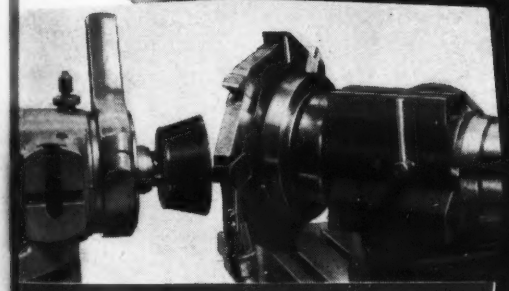

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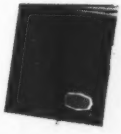

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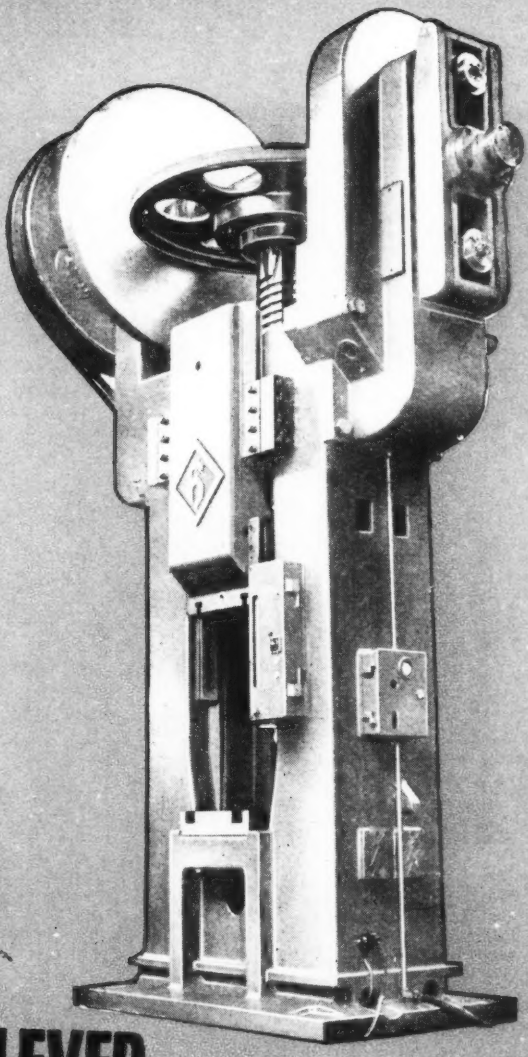

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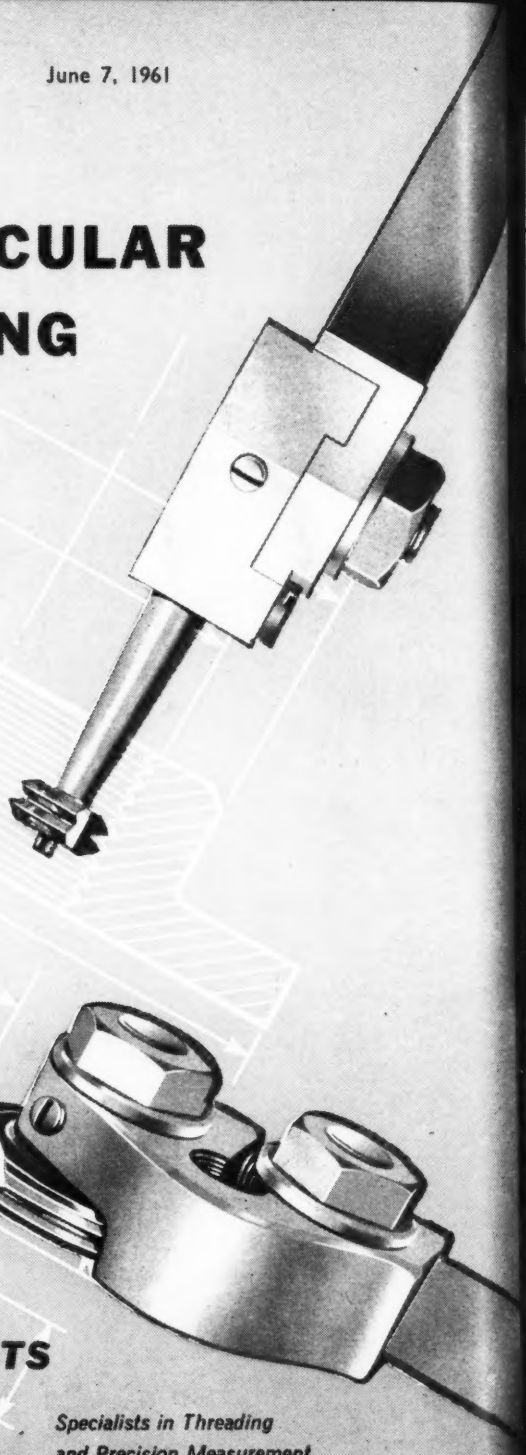

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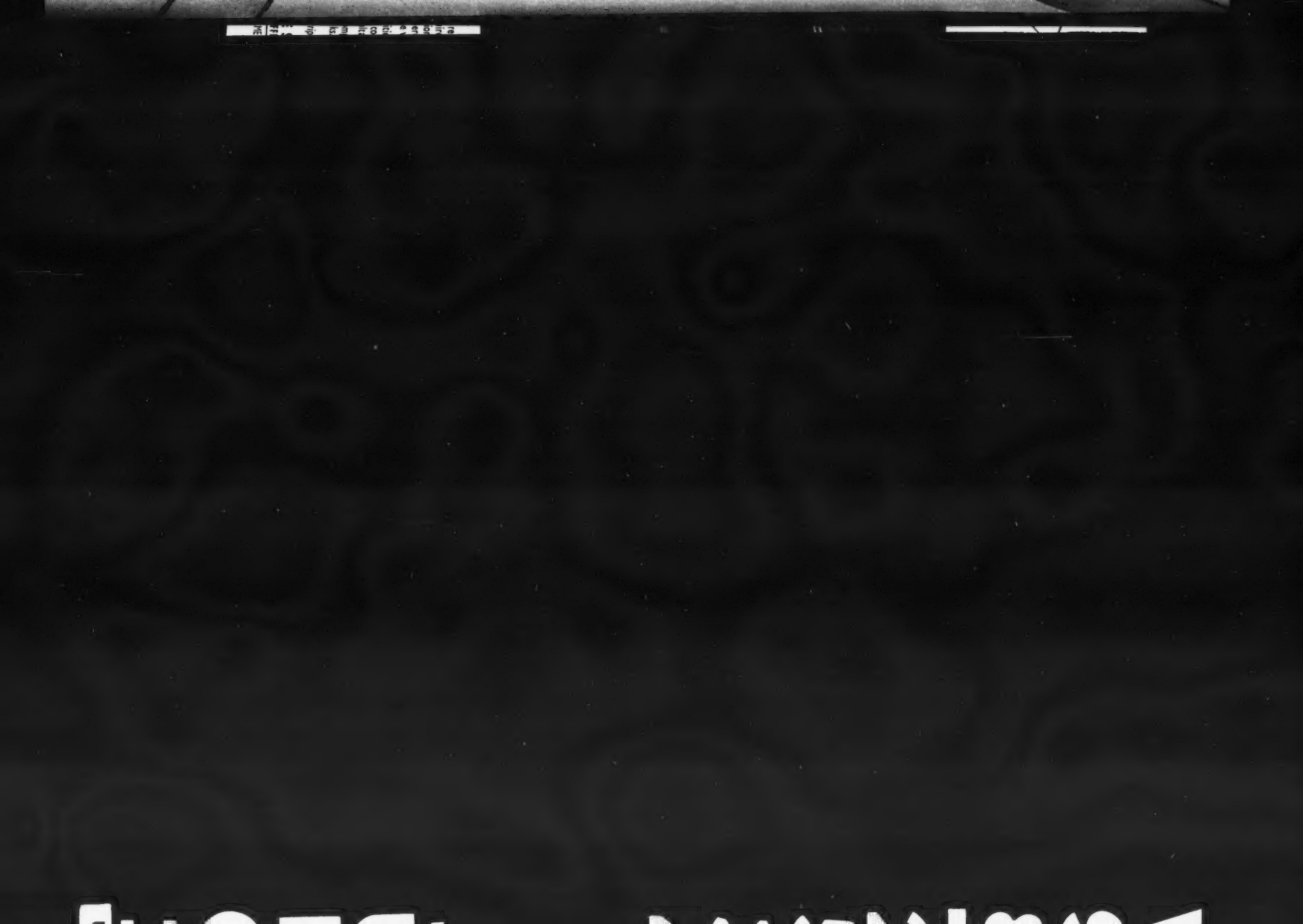

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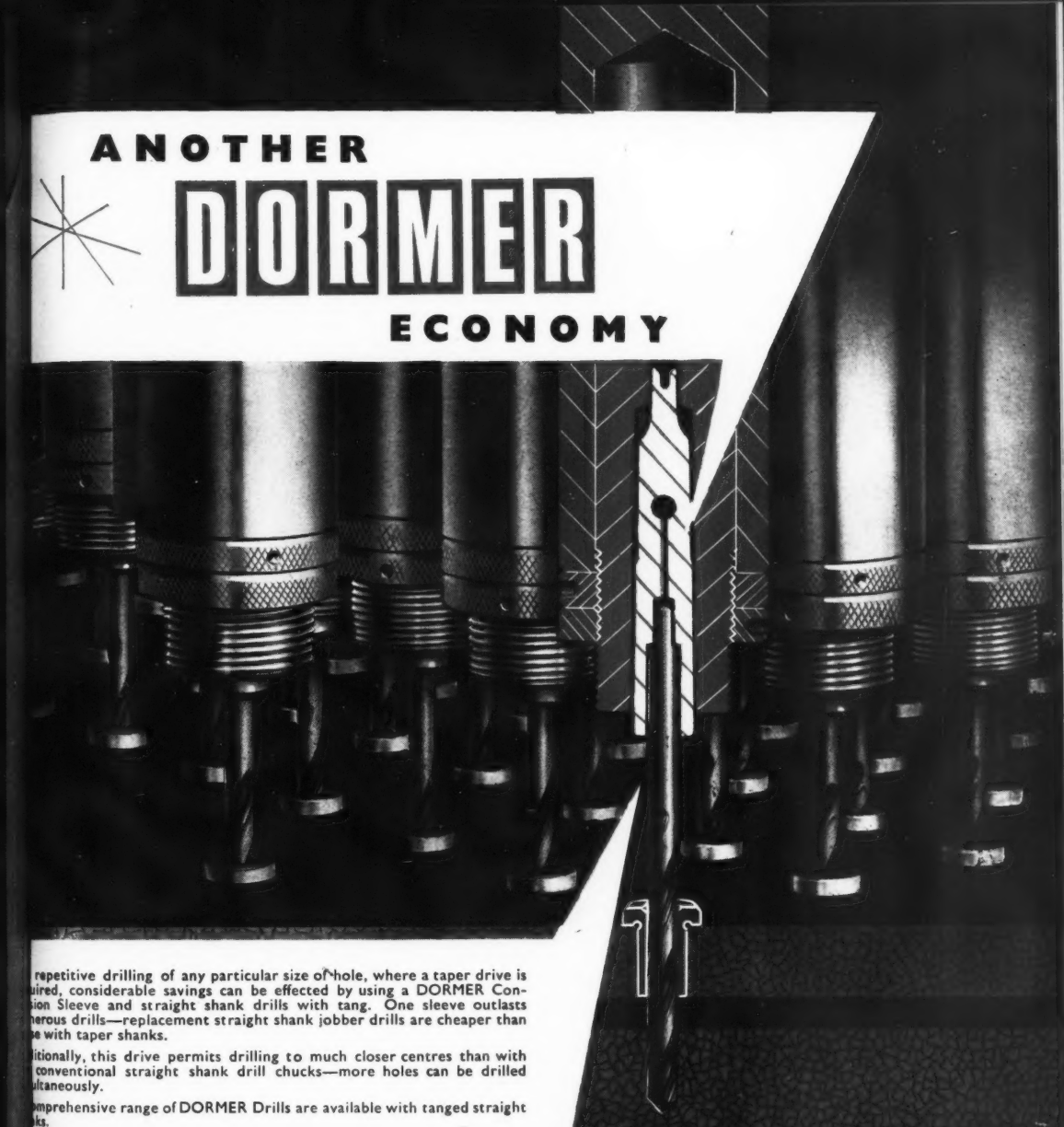

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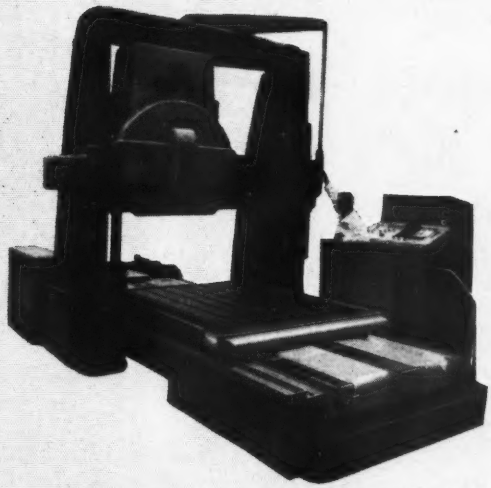

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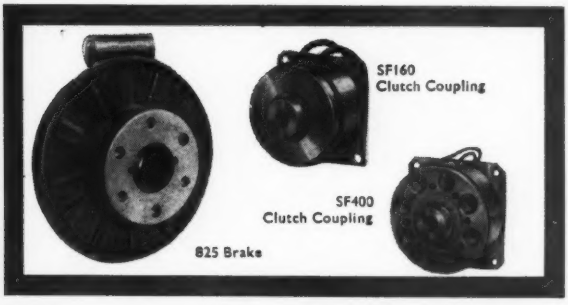

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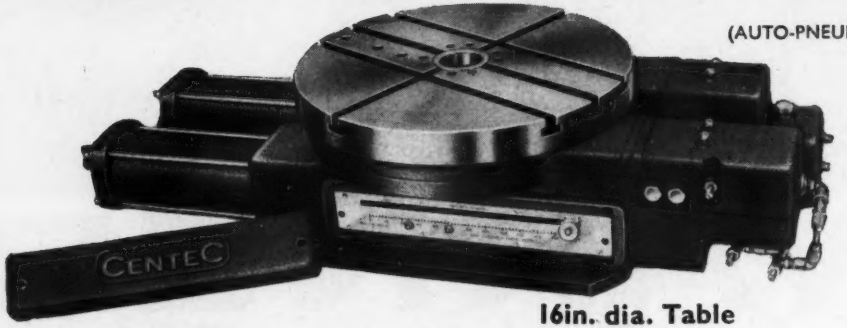

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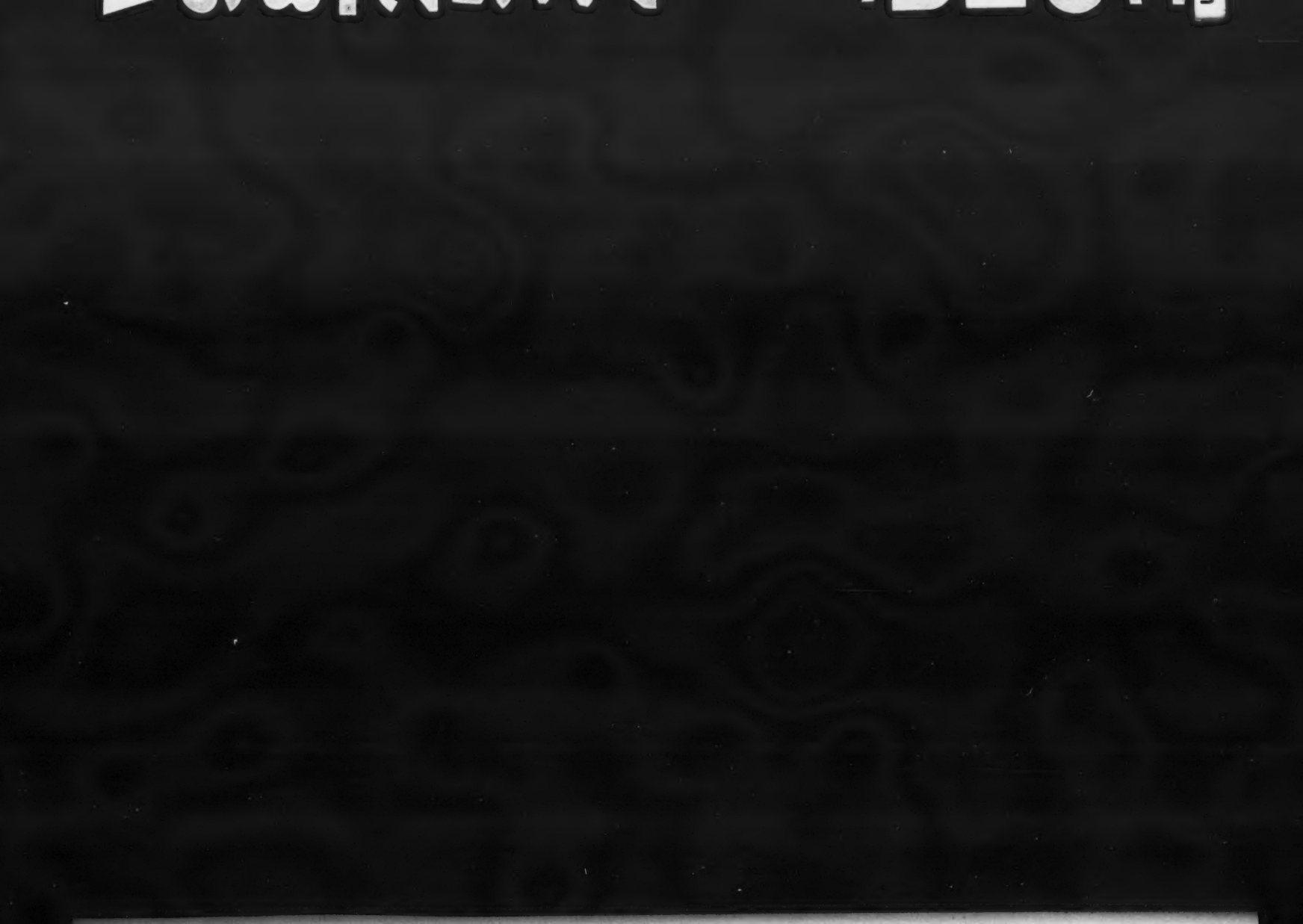

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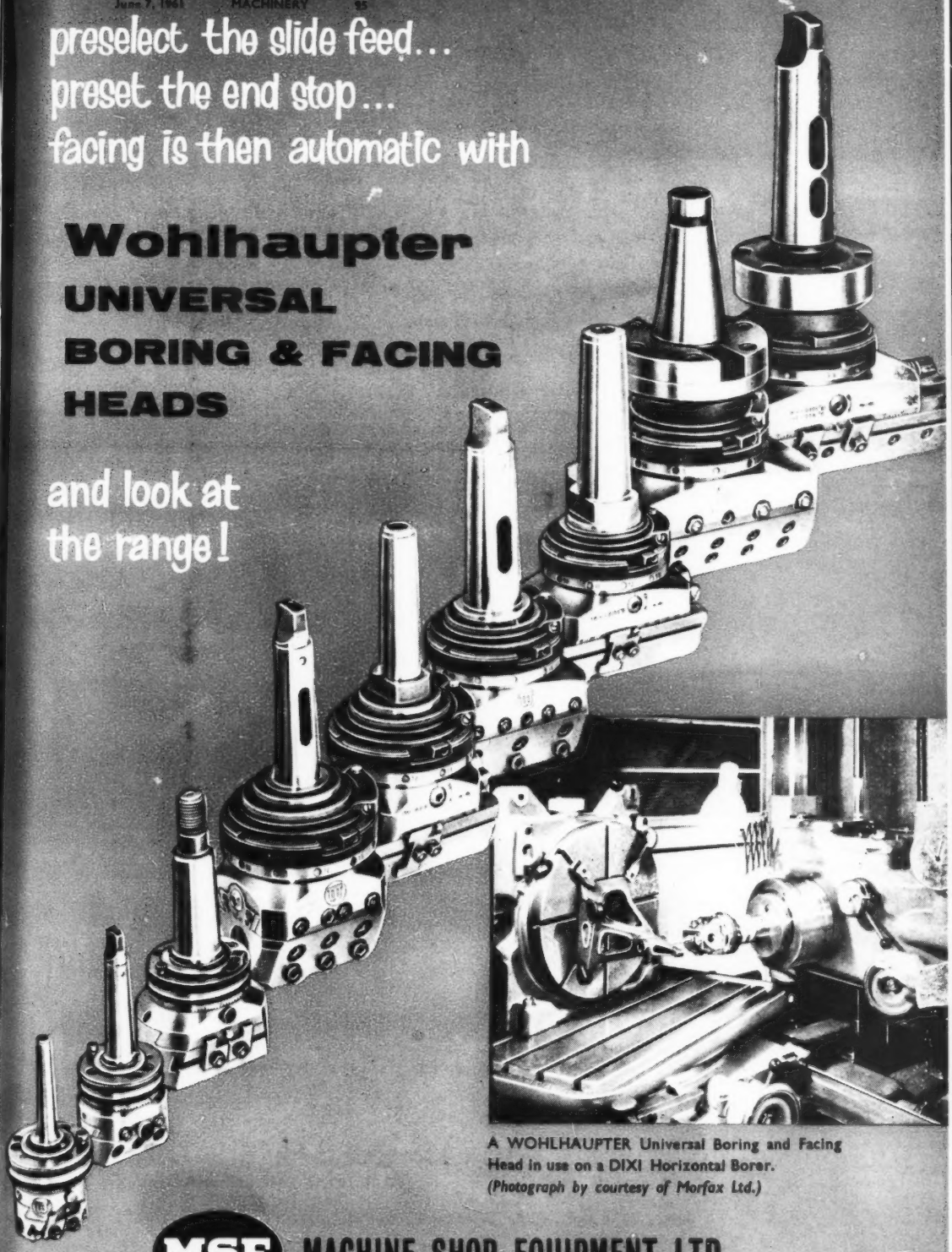

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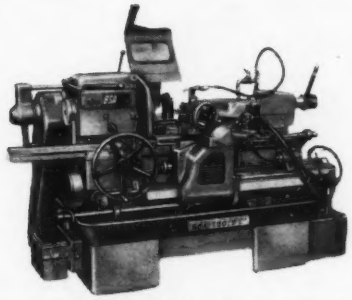

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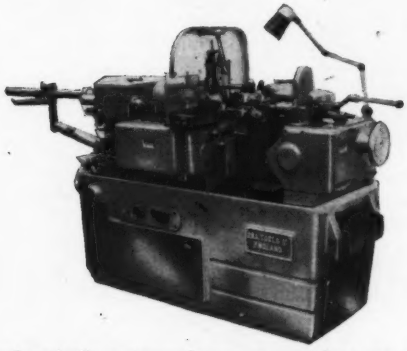

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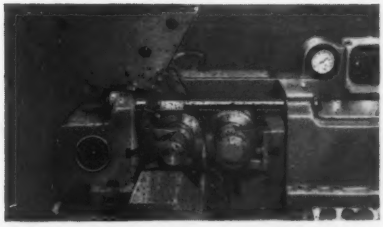

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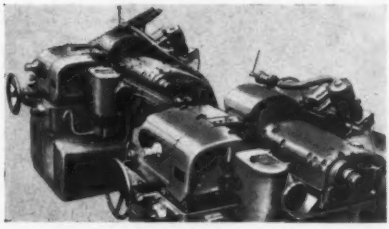
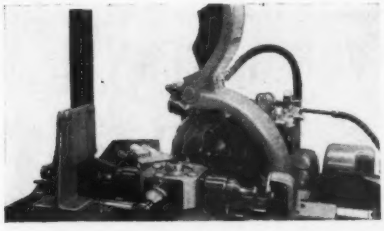


Two B.S.A. No. 8 centreless grinding machines linked for transfer of component for two operations. A chute type magazine gravity-loads workpieces to an endless chain conveyor. On completion of grinding on the first machine the components are passed by intermediate conveyor to the workplate between the wheels of the second machine for another grinding operation.



Cup type components delivered from a magazine are received by revolving collets on the turret faces and presented to the chuck for machining from the cross slides on this **B.S.A. 5M fully automatic chucking machine.** Turret index brings a finished component to the station where it is stripped from the collet pneumatically while the succeeding component is being machined. Cycle times: 9 to 15 seconds (depending on the size of the component for which the set-up is adjustable).

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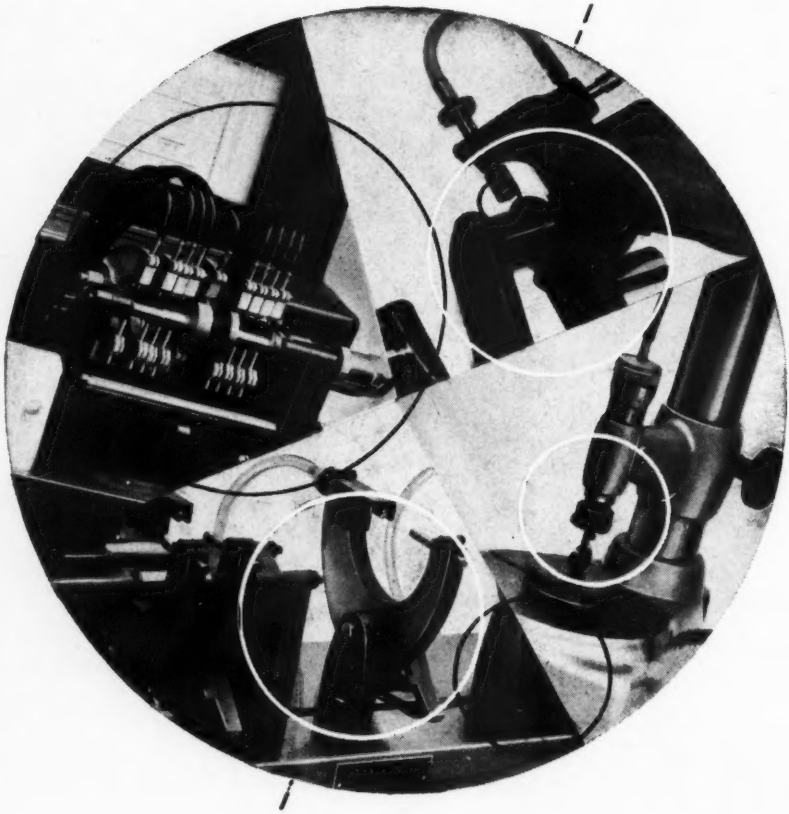

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Vol. 98, No. 2534 June 7, 1961

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CONTENTS

Editorial PAGE

Applications of Electrostatic Forces 1275

Principal Articles (*For abstracts see next page*)

The Quantity Production of Poppet Valves 1276
Equipment for Marking-out Castings and Forgings 1285
Cross Pallet-type Transfer Machine for Operations on Motor-car Steering Gear Housings 1287
Fosdick Numerically-controlled Jig Boring Machine .. 1290
Russian Automatic Transfer Machines at the Leipzig Fair .. 1293
Production of Components for Compressed Air Equipment 1303
The Staveley Group Research Department 1309
Assembling Domestic Radio Sets 1313

Short Articles

Crane Girder Used to House Equipment 1284
Rotary Coolant Filter for 72-in. Aluminium Rolling Mill .. 1289
Large Plastics Vacuum Chamber 1292
Use of Noral 28S Alloy for Lens Mounts 1302
B.O.C. Automatic Line Following Unit 1302
Staffa 18-in. Pipe Bending Machine 1308
Calor P4 Flame Cutter 1317
Machine Tool Industry Research Association 1318

News of the Industry

Tyneside 1319
Machine Tool Orders 1320
The South 1321
Industrial Notes 1322
Scrap Metals Report 1324
Machine Tool Share Market 1325
British Machine Tool Imports and Exports (Classified) .. 1326
Prices of Materials 1328

Classified Advertisements 147
Index to Advertisers 179

Abstracts of Principal Articles

The Quantity Production of Poppet Valves P. 1276

This article, which is the last of three, is concerned with the final operations on poppet valves for the range of passenger car and commercial vehicle engines produced by Vauxhall Motors, Ltd., Luton. The stem ends are hardened by an automatic machine on which the valves are loaded into fixtures on an indexing table, heated by high-frequency induction, and quenched in oil. Next, the stem ends are lapped on a machine with a capacity for 54 valves per load, which operates on a 2-min. cycle. Finishing of the stems on a centreless grinder is followed by marking on an automatic machine. Subsequently, the seats are ground on a battery of special machines, arranged for automatic loading. Inspection is performed on two automatic, multi-dimensional machines. Finally, details are given of a form-grinding operation for producing the collet grooves in valves for commercial vehicle engines. (MACHINERY, 98—7/6/61.)

Russian Automatic Transfer Machines at the Leipzig Fair .. .. .. P. 1293

Much interest was aroused by the two Russian-built automatic, in-line, transfer machines shown at this year's Leipzig Spring Fair. One of these machines, for milling, drilling, counter-boring, boring, facing, and tapping operations on aluminium-alloy oil filter housings for diesel engines, is here described. The cycle time is 1 min., and platen-type fixtures are employed in which the hand-loaded castings are power-clamped. Indexing is by a transfer bar moved by one of the face-milling heads. At one point, the platen is turned through 90 deg. for drilling and other operations, and after being returned to the original orientation it reaches a lateral track whereon it is moved to a station at which all the holes are simultaneously tapped. Subsequently, the platen is raised into a cleaning station for the disposal of swarf, and it then moves along return conveyors to the unloading and loading station. (MACHINERY, 98—7/6/61.)

Production of Components for Compressed Air Equipment .. .. .. P. 1303

Plant at the Farnham works of Martonair, Ltd., and Nuquip, Ltd., includes machines which have been built by the company for the quantity production of component parts for air cylinders and for performing various operations on pressure die-cast heads for lubricators incorporated in compressed air lines. Details are given of these machines which are fully automatic in operation, and compressed air equipment is extensively employed for such purposes as work feeding and clamping. One of the machines provides for drilling two intersecting stepped-diameter holes in brass end covers for air cylinders. Tie bars for air cylinders are chamfered at both ends in two stages at a fully-automatic cycle on another machine, and screwcutting is then carried out on an Edgwick machine, which has been fitted with work-handling equipment and converted for automatic working by the company. (MACHINERY, 98—7/6/61.)

The Staveley Group Research Department .. .. P. 1309

Formed in 1956, at the instigation of Sir Ben Lockspeiser, the Staveley Group research department is now housed in premises at Clapham, near Bedford, which have a floor area of 12,000 sq. ft., and a new building, of 3,000 sq. ft. area is planned. The department is intended to serve the machine tool companies within the group—including James Archdale & Co. Ltd., and Geo. Richards & Co., Ltd.—and has sections devoted to mechanical engineering, control systems and electronics. There is a staff of 50, of whom more than half hold H.N.C. or higher qualifications. Work of the department includes investigations into hydro-static slideways, thrust bearings, feed screws, and worm and rack drives; the investigation of machine structures with the aid of Perspex models; research into hydraulic motors for machine tool drives; and contour milling under the control of tapes produced with the aid of a computer developed by the department. (MACHINERY, 98—7/6/61.)

Assembling Domestic Radio Sets P. 1313

Corran Works, Ltd., a member of the Pye group of companies, was one of the first companies to establish a plant in Northern Ireland under the Government's post-war development scheme, and several million radio sets have so far been assembled. At peak periods, as many as 34 different types of radio sets, of conventional valve and transistor types, have been in progress through the works, and in this article some aspects of the practice and equipment employed are described. Attention is drawn to a mechanical aid for a small sub-assembly; mobile test equipment; a modified wire-cutting and stripping machine; and continuous flow-soldering equipment. (MACHINERY, 98—7/6/61.)

Contributions to MACHINERY

If you know of a more efficient way of designing a tool, gauge, fixture, or mechanism, machining or forming a metal component, heat treating, plating or enamelling, handling parts or material, building up an assembly, utilizing supplies, or laying out or organizing a department or a factory, send it to the Editor. Short comments upon published articles and letters on subjects concerning the metal-working industries are particularly welcome. Payment will be made for exclusive contributions.

EDITORIAL

Applications of Electrostatic Forces

In connection with various industrial processes, the incidental generation of electrostatic charges, which may be of considerable magnitude, is undesirable both on account of the effects that they may have on the behaviour of the materials that are being handled, and, in certain circumstances, the associated risks of shock or ignition. On the other hand, the fact that forces of attraction or repulsion are set up between objects or particles which carry artificially induced charges, has been turned to practical account for various purposes, and certain processes based on this phenomenon are of growing practical importance.

Among the better-known applications of the electrostatic principle is the precipitation of contaminating particles of dust or fluids in air to achieve the degree of cleanliness which is now essential for various manufacturing and assembly operations, or to ensure working conditions of the desired standard. In an electrostatic filter, the particles are first charged as the air passes through an ionizing section and are subsequently attracted to electrodes of opposite polarity on which they are deposited. It is stated that with such equipment particles as small as 0·01 micron diameter are removed from the air stream. A similar technique may be employed to cleanse air of the mist and smoke generated from cutting oil during machining operations. Electrostatic paint spraying, which has assumed such great significance in recent years, is similar in many respects to electrostatic filtration. Here, again, charged particles are effectively attracted to surfaces of opposite polarity—in this case the work to be painted—with the result that losses due to overspray, which may otherwise be so substantial, are greatly reduced. With this process, the paint particles are charged by the special atomizing units, and the work is normally earthed. As an indication of the economies that can be obtained, it may be noted that for one installation at a motor car factory, the estimated paint loss is now less than 2 per cent, as compared with 50 per cent for normal spray guns. The fact that paint is used more effectively also results in high output. It is claimed, moreover, that smooth and uniform coatings are obtained, and that duplication can readily be achieved owing to the elimination of variables. Further advantages are afforded by the fact that ventilation requirements are reduced, and that no special provision need be made for the collection and disposal of overspray.

In a more specialized field, advantage is taken of electrostatic effects to improve the quality of coated abrasive products. The backing paper or cloth, with the adhesive-treated surface downwards, is arranged to pass above a conveyor on which the abrasive grain is carried. Provision is made for simultaneously charging the grain and the backing material to opposite polarity, with the result that the grain is attracted upwards with considerable force and becomes embedded in the adhesive. A refinement associated with this method depends upon the fact that charges tend to be concentrated at sharp points. Silicon carbide particles, in particular, are normally of elongated shape with pointed ends, and such particles approach the adhesive film end-on and are securely anchored. Moreover, the points at the opposite ends of the grains project to form an effective cutting surface. A further advantage is that the charged grains repel one another and therefore assume an even spacing before entering the adhesive.

Other specialized electrostatic processes, which are of considerable interest to engineers, provide for copying documents or drawings and for forming X-ray images. For the latter purpose, a metal plate with a thin layer of selenium is sensitized by application of a uniform electrical charge. On exposure, the selenium conducts the charge to the backing plate in proportion to the intensity of the X-rays and an electrical image results. The latter is then rendered visible by blowing a charged powder across the surface, and can be observed under side lighting in a special viewer.

A more ambitious application of electrostatic forces is for work-holding on machine tools, which should form a valuable addition to the available methods of securing parts made from non-magnetic metals or other materials which do not conveniently lend themselves to mechanical clamping. These methods, it may be noted, include vacuum chucking, the use of double-sided adhesive tape, and—in special circumstances—the anchoring of workpieces in ice or solidified wax. The electrostatic chuck, to which reference has previously been made in MACHINERY, has a ceramic body with a thin film of epoxy resin on the upper surface, and metal fences at one side and end, with which the workpieces must be in electrical contact, either directly or indirectly. Before the work is placed in position, the chuck surface is treated with dielectric

(*Continued on page* 1322)

The Quantity Production of Poppet Valves

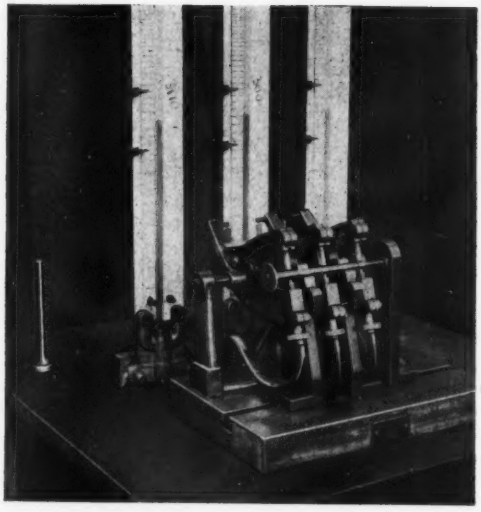
Methods Employed by Vauxhall Motors, Ltd., Luton

By R. E. GREEN, Associate Editor

TWO ARTICLES IN MACHINERY, 98/808—12/4/61 and 98/1164—24/5/61, have been concerned with machining and other operations on poppet valves for the range of passenger cars and commercial vehicles made by Vauxhall Motors, Ltd., at their Luton works. Cutting off from the bar, flash butt welding of lengths of dissimilar metals, electrical upsetting, forging, and heat treatment, were considered in the first of these articles. In the second, reference was made to the straightening of stems in an adapted flat-die thread-rolling machine, cutting-off and grinding stems to length, an automatic transfer conveyor whereby the valves are fed to a centreless grinder for semi-finishing the stems, an automatically-loaded multi-spindle automatic for turning the outside of the head and the seat, and a special machine for plunge-forming the oil seal and cotter grooves at the rate of 12 valves per min.

The next operation provides for hardening the stem end to between 50 and 51 Rockwell C, and is performed on the special machine shown in Fig. 1 which was designed by Vauxhall Motors, Ltd., and built for them by the Middlesex Tool & Gauge Co., Ltd. On this machine, the valves are automatically loaded, heated by the Radyne (Radio Heaters, Ltd.) 9-kW. high-frequency induction unit at the right, and ejected, at the rate of 12 per min. Valves are placed by the operator in the chute *A*, formed from two parallel steel bars, in which they are suspended by the heads. The valves slide down the curved chute to a position at which they are arrested by the upper of two stops attached to the top of the long escapement lever *B*, the lever being pivoted just below the centre.

These two stops are so shaped that they project towards the valves in the chute from either side, and there is space for one valve between them. The lever pivot shaft is connected to the armature of a solenoid in the adjacent box, and when the solenoid is energized, the upper end of the lever is moved in a direction away from the camera,



against the pressure of a spring. This movement brings the upper of the two stops clear of the lowest valve in the chute, permitting it to slide down into contact with the second stop, which has been advanced by the same lever movement. When the current to the solenoid is cut off, the lever is returned by its spring and the second stop releases the valve which is free to pass down the chute. Other valves in the chute are, however, retained by the first stop, as before.

At the lower end of the chute, the valve is supported by two stops at the bottom of the lever *B*, these stops being so arranged that they hold the stem at an angle of about 30 deg. above the edge of a rotary indexing table. At the periphery of this table are 18 similar holding fixtures, also arranged at an angle of 30 deg., and successive movements, imparted by a continuously-driven Geneva mechanism, bring the fixture, in turn, into position beneath the lower end of the chute. Each fixture has a fixed and a moving jaw, the latter, which is spring-loaded towards the closed position, being opened by a cam beneath the table as the fixture approaches the bottom of the chute.

When the lever *B* is next operated, the stops at the lower end are retracted, and the valve is allowed to fall into the open jaws of the fixture, in which it is held between V-grooves in the opposing

faces. As the table is subsequently indexed, in an anti-clockwise direction as viewed from above, the lever whereby the moving jaw is operated is carried clear of the cam, and the jaw is closed by the spring to grip the valve. Further indexing movements of the table carry the valve round until the outer end of the stem comes into contact with the cam *C*, on a bracket at one side. As the valve is moved past this cam, it is pushed down in the fixture to a pre-determined level.

Subsequently, the valve is indexed into engagement with the first of two water-cooled heater coils supplied from the Radyne unit with current at a frequency of 450 kc. per sec. These heater coils are carried on a slide, on which they can be adjusted to bring them into the correct position for the length of valve stem to be hardened, and clamped in place, and they serve to heat the stem to a temperature between 850 and 870 deg. C. The period between the indexing movements of the machine is 5 sec., and each of two valves is heated by a coil for this period. On leaving the second coil, the valve is at the required temperature, and is immediately carried through a copious flow of light quenching oil from a sheet metal trough at the far side.

This trough extends over about four fixture positions, and the oil is pumped up from an open tank beneath the machine, and returns by gravity from the centre of the table. After leaving the trough, the fixture reaches the position at which the cam operates the moving jaw, and the valve slides out of the fixture, down a chute at the centre of the table, and out of the machine at one side. Hardness checks on the stems are carried out on sample valves twice during each shift, on a Reicherter (Lerche Machine Tools, Ltd.) testing machine installed in the shop.

LAPPING THE STEM ENDS

From the hardening machine the valves are passed to the 24-in. Lapmaster (Payne Products International, Ltd.) machine shown in Fig. 2, on which the ends of their stems are lapped flat, smooth, and at right angles to the axes. The flat lapping table on this machine supports three plates with deep grooves which assist in the continuous distribution of the lapping compound. These plates, which are of 10 in. diameter, are prevented from being carried round by means of brackets secured to an annulus surrounding the table. Each bracket has two rollers which are in contact with the outside of the plate, so that the latter can revolve on its own axis.

The plates are caused to turn owing to the difference in the surface speed of the table at the centre and the periphery, and their motion assists in maintaining the surface of the table flat and smooth. Each plate carries a holder with 18 bushed holes of a bore diameter in which the stems are a sliding fit, and these holders can be changed when valves of a different stem diameter are to be lapped. Columns at each side of the machine support slotted bridge pieces, and the latter carry brackets on which three vertical air cylinders are mounted, one directly above each of the plates.

On the ram of each cylinder is carried a floating flat disc, to which is attached a pad of resilient plastics material, whereby a light load is applied to all the valves in the holder during the lapping operation. A valve at the side of the cylinder

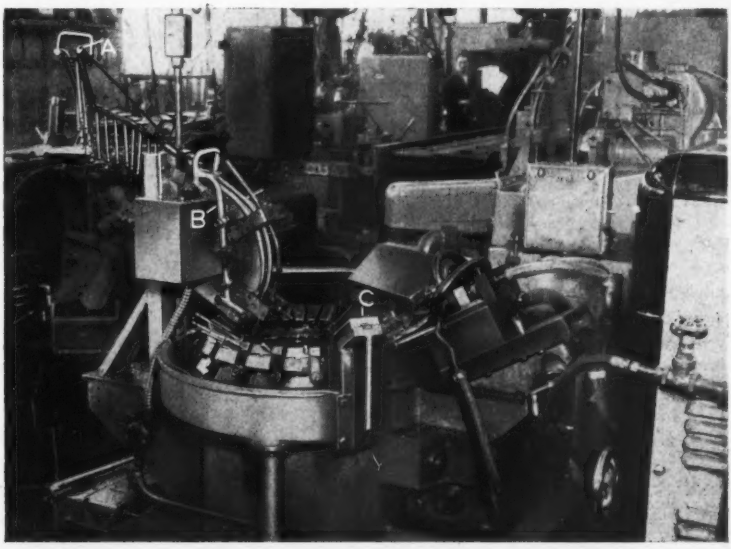


Fig. 1. On this automatic machine for induction-hardening valve stem ends, the valves are placed in the chute *A* by the operator and are discharged automatically at the end of the hardening cycle

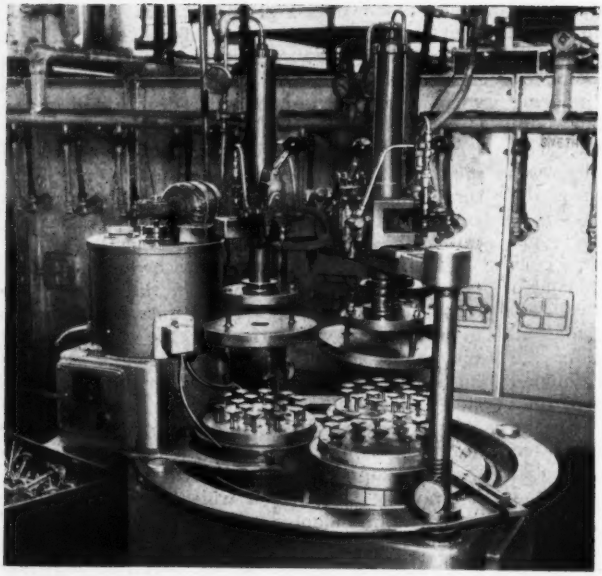


Fig. 2. After the hardening operation, the ends of the stems are finished on this Lapmaster machine which has a capacity for 54 valves per load. Steel pads, covered with resilient material, apply load to the valve heads during lapping

provides for lowering and raising the ram, and when the latter is fully lowered the flat disc rests freely on the valve heads, no pressure being applied by the cylinder. Lapping is performed with the table rotating in an anti-clockwise direction, and number 2220 lapping compound, supplied by Payne Products International, Ltd., is delivered through a capillary tube from the tank at the left, which is fitted with a motor-driven agitator.

The cycle time on this machine, governed by a timer on the housing beneath the compound tank, is 2 min., which is sufficient for cleaning up the end faces of the valves, and the compound used gives a surface finish of 12 micro-inches r.m.s. From this machine, the valves are transferred to one of a series of Cincinnati centreless grinders on which the stems are finished, to a diameter of 0·3410/0·3417 in. for the Velox and Cresta exhaust valves, for instance. The machine is provided with automatic loading and unloading equipment, as described in MACHINERY, 86/1438—24/6/55, in the form of an indexing table on which the valves are held in peripheral slots at a slight angle to the horizontal, with the heads projecting.

From this table, the valves are automatically lifted by a pivoting arm, fitted with gripping fingers, and placed on the work rest between the grinding and control wheels. During the grinding cycle, the pivoting arm is returned in readiness for picking up the next valve, and the ground valve is thrust from the work rest between the wheels by an ejector rod. The grinding cycle occupies about 3 sec., and loading and unloading, 2 sec., so that a table slot must be reloaded by the operator every 5 sec. For inspecting the diameter of the stem at three positions, the Solex gauge shown in the heading illustration is employed.

AUTOMATIC MARKING MACHINE

At the next operation, each valve is marked on the stem with the company's symbol, on the automatic Funditor machine shown in Fig. 3. Automatic loading equipment on this machine incorporates a parallel-bar chute similar to that provided on the induction hardening machine, down which the valves pass to a double stop on the lever *D*. This lever is similar to that indicated at *B* in Fig. 1, with the upper end spring-loaded towards the right, and was formerly operated by a solenoid in the box at the right. With the arrangement now employed, a wire connects the lever with a stud on the marking slide of the machine, so that when the slide reaches the end of its travel towards the left, the lever is pulled in the same direction.

As the slide returns to the right, the wire follows the stud, and the spring returns the lever *D* to its original position. At each operation of the lever, a valve passes between the two stops at the top and slides down to two other stops, at the lower end. When these stops are retracted, at the next movement of the lever, the valve falls out of the chute on to a conveyor. This conveyor has two vertical plates which provide bearings for shafts carrying pairs of chain sprockets. Small slotted brackets to hold the valves are riveted to the two endless chains that pass over the sprockets.

The conveyor is mounted on a slide, on which it can be adjusted towards or away from the machine column to bring it into the required position in relation to the marking head. On the left-hand shaft of the conveyor is mounted a toothed indexing wheel, in addition to the sprockets, and

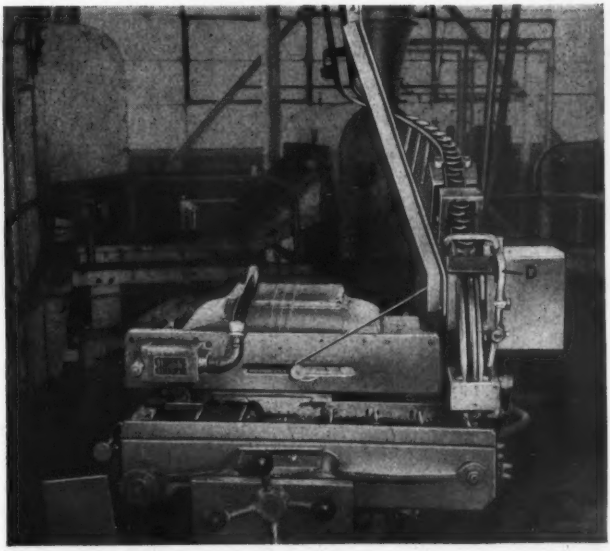


Fig. 3. On this Funditor marking machine, the company's trade mark is impressed on each valve stem. The transfer conveyor is operated by a pawl on the marking slide, and marking is performed on the return stroke

the teeth of this wheel are engaged by a pawl on the marking slide in the head of the machine. As the slide moves to the left, the conveyor is indexed one space in the same direction, and a fresh valve is carried into the marking position. At the same time, a valve is loaded into the empty conveyor position at the right-hand end.

At the marking position, the valve is supported by two rollers beneath the point at which marking is to be performed. As the valve moves into this position, it is lifted slightly so that it rides over the first of the two rollers and comes to rest between them. The marking slide, which is continuously driven, is then returned to the right, and the head passes across the valve which is supported by the rollers, turning it slightly, and impressing the symbol into the stem. When the slide again moves to the left, the indexing pawl automatically advances the conveyor.

The marked valve is thus carried away from the marking position, riding over the second supporting roller, and a fresh valve is moved into place. At the left-hand end of the conveyor, the valves fall from the carrier-slots and slide down a chute.

FINISH-GRINDING VALVE SEATS

Finish-grinding of seats, to angles of 29 and 44 deg. ±15 min., for the inlet and exhaust valves respectively, is performed on a battery of Landis machines, each of which is arranged for entirely automatic operation. In the general view of one of these grinders given in Fig. 4, may be seen the parallel-

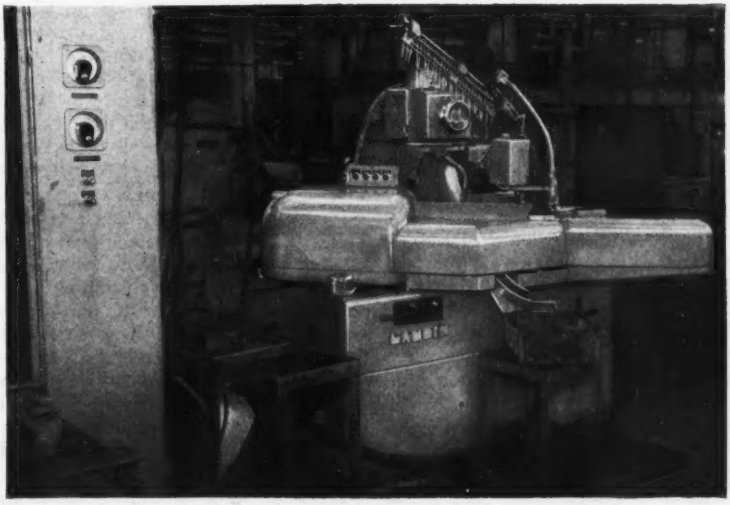


Fig. 4. A general view of one of the Landis machines employed for finish grinding valve seats to angles of 29 and 44 deg. ± 15 min. Approximately 0·007 in. is removed from the seat in a period of 8 sec.

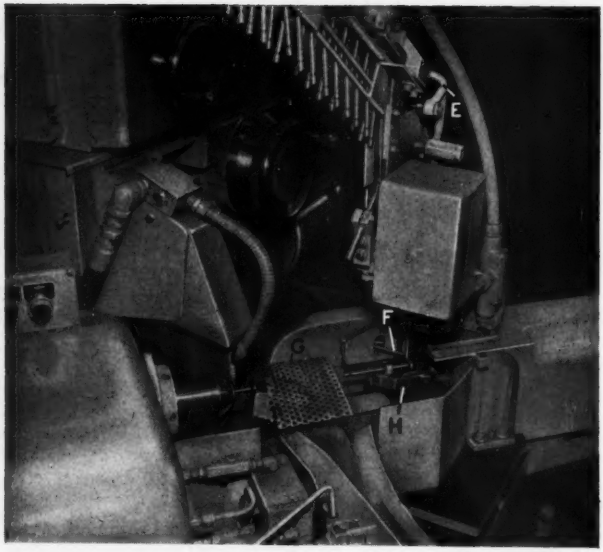


Fig. 5. This close-up view of the working area of the Landis machine shows the loading mechanism and the hinged chute *G* which is raised by an air cyclinder when the valve is advanced

bar chute into which the valves are loaded by the machine-minder, who tends three machines. The table of the machine can be adjusted to any desired angle in relation to the wheel spindle axis by means of special length blocks, which are interposed between datum faces on the side of the table and a bracket on the bed.

The escapement mechanism at the bottom of the loading chute is similar to that provided on the machine in Fig. 1, and is shown in the close-up view in Fig. 5. The lever *E*, operated by a solenoid in the adjacent box, allows the valves to pass down, one at a time, to the bottom of the chute. Here, each valve is arrested by the stop *F*, at the bottom of the lever, and when this stop is withdrawn, after the completion of the previous loading operation, the valve is allowed to fall into V-locations in a bracket. This bracket is attached to a slide, which is operated by a horizontal air cylinder, carried on an extension at the right-hand end of the table, and when the previously-finished valve has been ejected, the slide is advanced to the left.

As the slide moves forward, the hinged end of the chute *G*, which has a cover of perforated sheet metal, is lifted clear by an air cylinder. The loading slide can then advance the end of the valve into the collet. As the loading slide continues to advance after the end of the valve has entered the collet, a stop on the table comes into contact with a downward extension of the centrally-pivoted lever *H*, which supports the outer end of the valve stem in a V-block. This stop causes the lower end of the lever to rise, with the result that the upper end is lowered, and the V-block is carried down, clear of the collet. The valve can then be pushed into the chuck up to a stop, formed by the end of the air-operated ejector in the work spindle.

With the valve fully home, the work spindle collet is closed to grip the stem and the grinding cycle of the machine is started. The cycle is automatically controlled by equipment in the cabinet at the left in Fig. 4, which includes timers for setting the length of the spark out period, after the wheel-head has been fed to a fixed position, also for setting the number of complete grinding cycles to be performed before the automatic dressing cycle is initiated. At the start of the cycle, with the loading slide withdrawn, the wheel-head is brought forward, in a direction at right angles to the valve seat, to the grinding position, and is subsequently fed through a distance of about 0·012 in. during a period of 8 sec.

At the end of this movement, the head is caused to dwell for 3 sec. before being automatically retracted. The wheel employed is of Universal MA 46/60 N-V specification, and during the operation it is oscillated sideways at the rate of one complete reciprocation per sec. to distribute the wear across the wheel face and prevent the formation of a groove. At the end of the dwell period, the wheel-head is retracted, the collet is opened, the ejector cylinder is energized, and the valve is pushed out into the chute *G*. The cycle time is 14 sec., and after 12 of the two-piece Velox and Cresta exhaust valves (seen in Fig. 5) have been ground, the automatic dressing cycle is initiated.

During dressing, the diamond, in the unit above the wheel, is advanced by 0·0015 in. for each of two passes, to remove a total of 0·003 in. At the same time, the wheel-head is advanced through a similar distance to compensate for the material removed. A light cutting oil is applied to cool the work during the grinding cycle and is cleaned before recirculation by passing it through a centrifuging unit supplied by Machine Shop Equipment,

Fig. 6. Inspection of finished valves, at the rate of 4,000 per 8-hour shift, is performed on this Sigma, multi-dimensional, 2-stage automatic machine, which is one of two installed in the valve department

Ltd., the rotor of which runs at 2,800 r.p.m. At this operation, the dimension from the stem end to the seat centre-line is held to limits of ±0·0075 in., and the eccentricity of the seat with the stem to 0·002 in.

INSPECTION OPERATIONS

After the seat-grinding operation, the valves are washed in readiness for inspection on one of two automatic Sigma (Alfred Herbert, Ltd.), multi-station, two-stage machines, as seen in Fig. 6, where Victor exhaust valves are being checked. Before the valves are fed into the automatic machine, the condition of the seat, stem, cotter and oil seal grooves, stem end, and head face are inspected visually for blemishes. Valves which pass this visual test are placed on a flat inclined platform at the front of the machine, on which they are supported only by the stems, with the heads overhanging the left-hand edge. The valves roll down the inclined surface, one at a time, to a stop at the lower edge.

In the close-up view of the machine given in Fig. 7, a valve may be seen at the lower end of the chute. Beneath the chute there is a loading slide, operated by an air cylinder, and this slide has a recess into which the valve drops when the chute is retracted. The valve is then carried forward to the first gauging position, at which the concentricity of the seat with the stem, and the run out of the stem end face are checked. For these checks, the valve rests on carbide-faced locating pads, and the head face is engaged by a friction pad on the end of a shaft driven by a small Klaxon geared motor unit. The pad is moved sideways, into contact with the head face, by a small single-acting, air cylinder *J*, and the motor runs continuously.

True running of the stem is checked at two positions, by two of the gauging heads *K*, and the nearer head, of

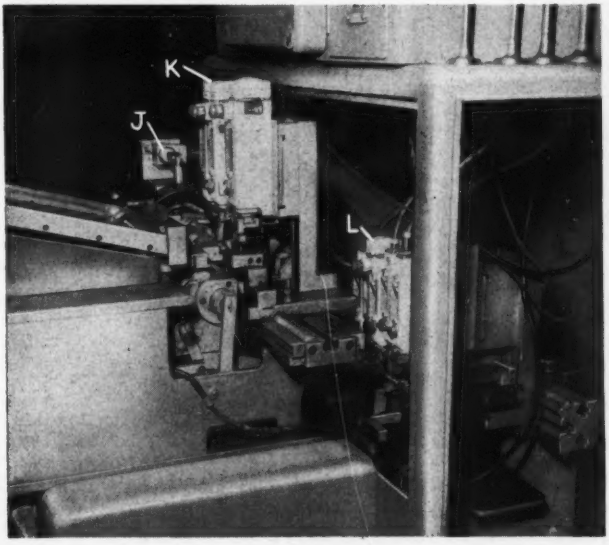


Fig. 7. A close-up view of the Sigma machine from one side, showing the air cylinder *J* whereby a pad, driven by a small geared motor unit, is pressed against the head face to rotate the valve during gauging

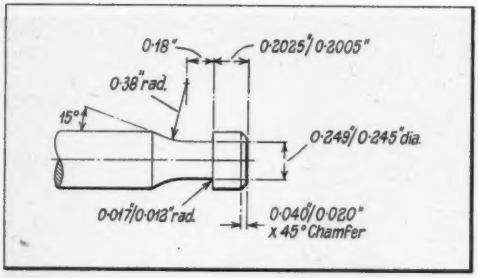


Fig. 8. Drawing showing details of the collet groove required in the exhaust valve for a commercial vehicle engine. Because of the hardness of the stems of such valves, the grooves are ground from the solid

similar type, is provided with a bell-crank lever which makes contact with the stem end of the valve. Eccentricity of the seat is checked by another electronic head, fitted with a caliper, which is mounted horizontally at the far side. At the completion of this first stage, the valve is withdrawn on the loading slide, from which it is then pushed by small stops, and falls into a slot in a transfer drum. Partial rotation of this drum delivers the valve to a second loading slide beneath, whereby it is carried to the second measuring station.

Valves rejected at the first stage are automatically ejected from the drum, and pushed out of the machine into a box at the far side. Those valves which pass the first inspection stage are carried forward by the second loading slide, and rest on another set of carbide-faced pads while checks are made by the lower set of gauging heads *L*. Three of these heads are fitted with floating caliper contacts which measure the diameter of the stem at the ends and near the centre, and a fourth head measures the diameter of the collet groove. Another head is employed for checking the length of the valve from the seat to the stem end.

From this position, the valve is withdrawn by the loading slide, and passes down a chute, over shutters which are automatically operated to direct it to one of three outlets leading to containers or to a conveyor. Valves are thus separated into groups which are too large or too small on one or more dimensions, and those which are acceptable and can be passed straight to the packing area. Here, the valves are dipped in a lanolin-oil emulsion, drained, and packed in waxed paper in tins for consignment either to the assembly or the spares department.

An automatic Lindberg machine is shortly to be installed for aluminizing the heads of most of the exhaust valves produced. This operation, which we hope to describe at a later date, will be performed after the valves have been inspected on the Sigma machine.

SPECIAL PLUNGE-GRINDING MACHINE FOR COLLET GROOVES

Plunge-forming of the collet grooves in the stems of valves for passenger cars, on a special machine of Vauxhall design, was described in a previous article, and this operation is also per-

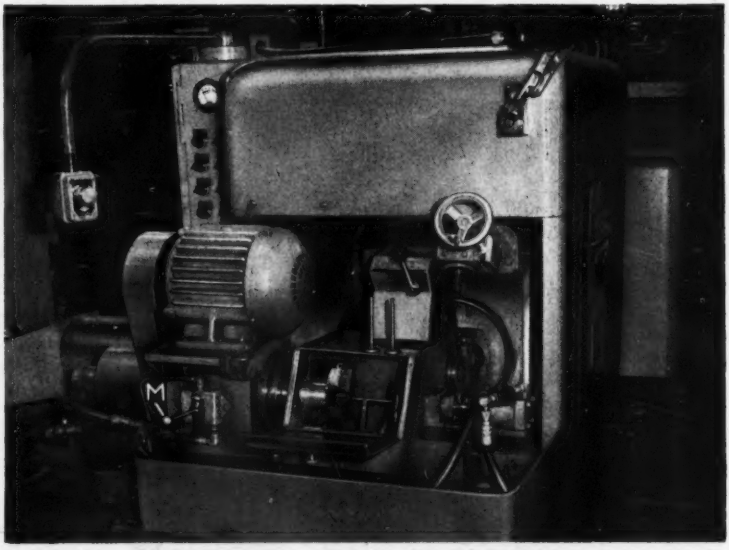


Fig. 9. Grooves of the type shown in Fig. 8 are plunge-ground on this type E Jones & Lamson machine in a cycle time of 15 sec. Mist-laden air extracted from the cabinet is filtered in a Precipitron electrostatic unit

formed on a battery of Britan lathes when extra capacity is required. As mentioned in the first article, however, the heat treatment applied to commercial exhaust valves is such that they are left in an extremely hard condition, and the collet grooves in these valves can only be machined by grinding. The dimensions of a typical groove, in an exhaust valve for a commercial vehicle engine, are shown in Fig. 8.

Such grooves, in hard valves, are ground from the solid on the Jones & Lamson (Buck & Hickman, Ltd.), type E, automatic form-grinder shown in Fig. 9, in a cycle time of 15 sec. On this machine, the wheel-head spindle, which is driven by a 5-h.p. motor, is run at 2,400 r.p.m. for a new, 20-in. diameter wheel, to provide a surface speed of 12,500 ft. per min. As the wheel is reduced in diameter, the spindle speed is increased by the use of different pulley combinations to maintain this surface speed, and the wheel is discarded when it has been reduced to 17½ in. diameter.

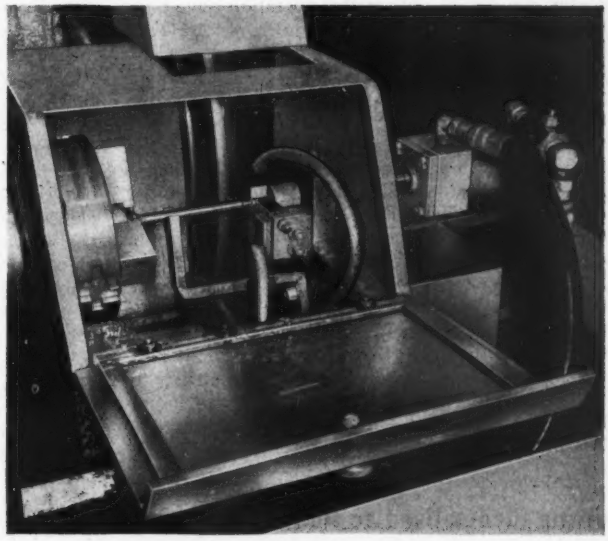


Fig. 10. Close-up view of the working area on the Jones & Lamson machine showing the method of holding the valve by the head in a 3-jaw chuck, and supporting the stem end against the grinding thrust

A close-up view of the work-spindle is given in Fig. 10. It is equipped with a 3-jaw, pneumatically-operated chuck, with jaws of special design which grip the valve on the outside of the head. Location is taken from the end face of the stem, since a tolerance of 0·002 in. must be held between this face and the shoulder of the groove. For loading, the valve is placed in a V-groove in the upper end of a bracket, with the stem end resting between carbide-faced pads clamped to the tailstock quill. When the valve *M*, Fig. 9, is operated to close the chuck, an air cylinder advances the tailstock quill, to push the valve into the chuck jaws, against a spring-loaded ejector. This ejector holds the stem end in contact with a carbide-faced locating pad on the tailstock quill while the chuck is closed.

As the valve enters the jaws, it is lifted slightly, so that it is held clear of the V-groove in the bracket. The automatic grinding cycle of the machine is then started, and with the work-spindle running, the wheel-head is advanced by a cam which provides for roughing, finishing, and sparking-out periods during a total time of 9 sec. The wheel is then withdrawn and the work-spindle is stopped in readiness for unloading the valve. A copious flow of a light cutting oil is applied to the work during the grinding cycle, and the fine mist produced is confined within the cabinet. This mist is of a potentially explosive nature, and the cabinet is therefore connected to a Westinghouse Precipitron electrostatic filter which continuously extracts air and removes both the oil mist and other particles. A Barnesdrill magnetic separator is provided to clean the cutting fluid.

Two dressing diamonds are carried on a slide at the rear of the wheel—one for each corner—and their movements during the automatic dressing cycle are controlled by cams. Each diamond is accurately located in a holder which is set by means of special blocks, and they are moved across the face from left to right in succession. The leading—right-hand—diamond dresses the surface of the wheel which produces the parallel portion of the collet groove, the radius at the edge for the corner of the groove nearer to the stem end of the valve, and the side of the wheel for the adjacent shoulder. The second diamond comes into action after the first has cleared the wheel, to dress the 15-deg. angle, and the 0·38-in. radius which blends with the parallel portion.

This dressing cycle occupies about 30 sec., and is selected by the operator after about 20 to 30 valves have been ground, depending on the hardness of the material and the quality of the wheel.

So far, the best results at this operation have been obtained with a Universal wheel of A-8OU-B specification. The profile produced in the groove is inspected by the operator on a Heliscope (Salisbury Precision Engineering, Ltd.) projector, fitted with a lens of 25 × magnification, installed adjacent to the grinding machine. With this instrument, an image of the groove can be aligned with a drawing on which there are lines showing the upper and lower limits, and wheel dressing is normally performed when the image outline approaches one of these lines.

Since wear tends to be most pronounced on the wheel edge which produces the 0·012/0·017-in. radius at the stem end of the groove, it is the condition at this point that determines when dressing of the wheel is necessary. Concentricity of the parallel portion of the groove is also important, and is normally held within 0·001 in. on this machine.

Crane Girder Used to House Equipment

In large, overhead, travelling cranes made by the Harnischfeger Corporation, International Division, 4329 West National Avenue, Milwaukee, Wis., U.S.A., the interior of one of the main girders is now being utilized to house the electrical controls and certain components for the electrical power supply system.

View inside the main girder of a Harnischfeger travelling crane, showing the control equipment installation

The first two cranes incorporating this feature have been installed at the plant of the Ash Grove & Portland Cement Co., Chanute, Kansas, and a view of the girder interior is shown in the accompanying illustration. The working aisle measures 8 ft. high by 5 ft. wide, and extends almost for the full length of the 120-ft. girder. To protect the electronic and electrical equipment from the harmful cement dust, the interior of the girder is pressurized by means of a motor-driven blower unit, that forces the air through wool-bag filters which are self-cleaning. A pressure of about 2 lb. per sq. in. above atmospheric is maintained.

To facilitate handling the equipment inside the girder, an electric travelling hoist is provided on a rail just below ceiling level, and a dust proof hatch is incorporated in the floor which permits tools and equipment to be lifted from ground level, 80 ft. below.

Another feature of these cranes is that the four main travelling wheels are individually driven through gearing by separate electric motors. The travelling, hoisting, and cross traversing motors of the crane, and opening and closing of the bucket, are controlled by only two joystick levers, and the electronic equipment provides steplessly-variable speeds. The operator's cab is pressurised and air conditioned because of the dust-laden atmosphere.

CRC 2-26 ANTI-CORROSION AND ANTI-MOISTURE TREATMENT.—Hellermann, Ltd., Gatwick Road, Crawley, Sussex, are the sole distributors in the United Kingdom for the CRC 2-26 anti-corrosion and anti-moisture treatment for electrical and electronic equipment, developed in the U.S.A. by Corrosion Reaction Consultants, 116 Chestnut Street, Philadelphia, Pa. The liquid employed has an unusually low surface tension and will readily penetrate cracks or holes to displace absorbed moisture. A molecular film is formed which, it is stated, does not dry, become brittle or crack, and insulates metal surfaces from chemical or electro-chemical action that may cause corrosion, although it is not difficult to remove. The liquid will also provide protection for painted surfaces.

The treatment, it is claimed, enables equipment which has been damaged by excessive exposure to moisture, or by total immersion, to be restored to operation.

Non-toxic, stable and inert, the liquid can be applied by brushing or immersion, and is also obtainable in aerosol dispensers for convenient use on production lines.

Equipment for Marking-out Castings and Forgings

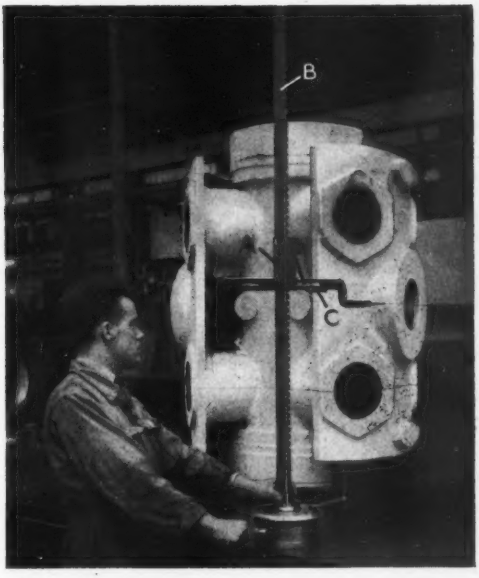


Fig. 1. Special equipment which has been designed and built by Harland & Wolff, Ltd., Belfast, to facilitate marking-out castings and forgings in the company's engine works

TO FACILITATE MARKING-OUT OPERATIONS on castings and forgings at their Queens Island works, Harland & Wolff, Ltd., Belfast, have designed and built special equipment, and a view of the unit for horizontal applications is shown in Fig. 1. A feature of this unit is the speed and ease with which it can be set to the required height, for scribing a number of lines, each of which is at a known distance from a datum, for example.

The scriber is carried at the end of a cranked arm, and the latter is secured to a block *A* which can be raised and lowered on the vertical triangular-section post *B*. This post has a number of square notches in one edge, spaced at 1-in. intervals, and these notches are engaged by a pawl housed within the sliding block. The pawl is engaged with, and withdrawn from, the slots by means of the lever *C*, the travel of which is limited —in the "engaged" position—by a peg projecting from the side of the block *A*. In use, therefore, the gauge is set to the nearest 1 in. of the required dimension by raising or lowering the block *A*, and engaging the pawl with the appropriate notch. Graduations at 1-in. intervals are engraved on the post *B*, and are visible through a small window provided in the block *A*.

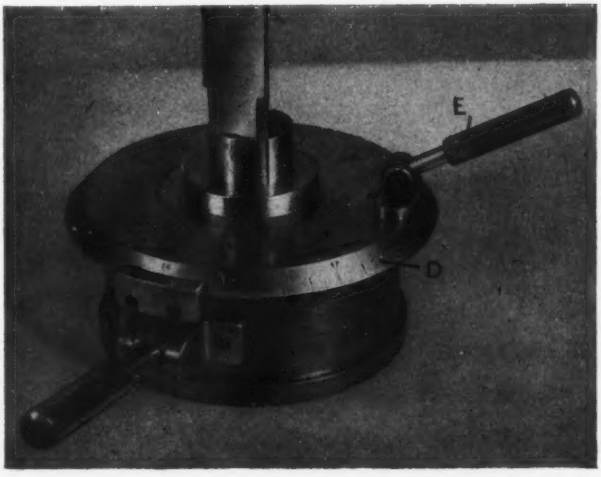


Fig. 2. Close-up view of the base of the marking-out equipment seen in Fig. 1

For setting the remainder of the required dimension, the post is raised and lowered vertically, as a complete unit, by means of a screw arrangement in the base of the stand, and a close-up view of this portion is given in Fig. 2. It will be seen that the lowermost portion of the post is of cylindrical section, and it is a sliding fit in a hole at the centre of the graduated disc *D*. This disc can be turned, by means of the handle *E*, and serves to rotate a nut whereby

the post is raised and lowered vertically. One complete revolution of the disc *D* moves the post vertically through a distance of 1 in., and there are 20 full length divisions equally spaced around the periphery of the disc.

These divisions are widely spaced, and are subdivided by shorter lines, in the conventional manner. It will be appreciated that by turning the disc from one full-length division to an adjacent half-length division, the post is moved vertically through a distance of 0·025 in., and owing to the wide spacing of the divisions, the gauge can readily be set, by interpolation, to within 0·005 in. The handle seen projecting from the base member is used to steady the gauge while the disc *D* is being turned, also to apply a clamp when the post has been set to the required height.

The arm carrying the scriber point, seen in Fig. 1, is also of special design, in that the point is pivoted and can be moved angularly through about 10 deg., for initial setting purposes. This angular movement is effected by means of a small eccentric, which is turned by a knurled-head knob, and there is another, similar, knob which clamps the scriber in the required position after adjustment. With this arrangement, the need to tap the scriber up and down, by hand, to align it with a previously scribed line, for example, is eliminated, and the accuracy and speed with which this operation is carried out are greatly improved.

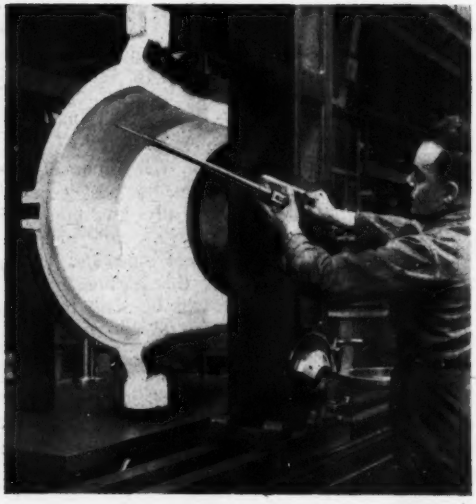


Fig. 3. To facilitate marking out workpieces in the vertical plane, this special trolley-mounted unit has been developed

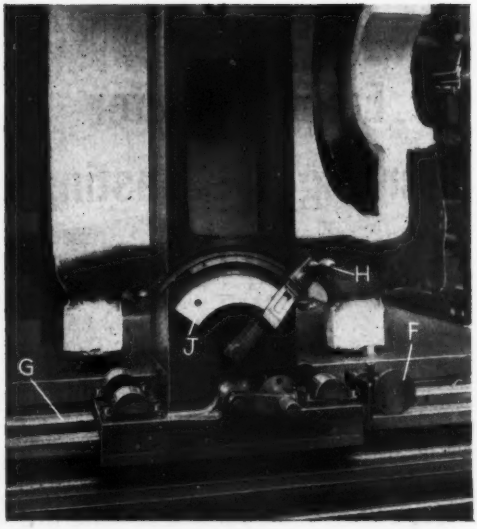


Fig. 4. Close-up view of the roller-type trolley of the unit shown in Fig. 3. Final settings are made by means of the lever *H* with reference to an arcuate scale

MARKING-OUT VERTICAL LINES

The unit which has been developed by the company to facilitate marking out vertical lines is shown in use in Fig. 3, and it incorporates a square-section cast-iron pillar, of ribbed construction, which is secured to a trolley-type base and can be moved on a long, narrow, cast-iron bed. Both sides of the pillar are accurately machined flat and parallel, and serve as vertical surfaces whereon a hand scriber and block can be used, as shown in the figure.

A close-up view of the base of the pillar, showing the trolley whereon it is mounted, is given in Fig. 4. The trolley has four wheels which roll on the flat surfaces of a conventional bed member, and there are orthodox retaining plates which engage with the under-sides of the ways. At the right-hand end of the base there is a plain disc, as indicated at *F*, which is in rolling contact with the bed and serves to drive a drum-type counter. As the unit is pushed along the bed, this counter indicates the distance, in inches, that it has travelled from the datum, and there is another counter which shows the distance travelled in millimetres.

These counters provide a rough guide to the distance moved, but the unit is finally located, to

the nearest whole number, by means of a plunger and the notched bar *G*, which can also be seen in Fig. 3.

Final setting of the unit is effected by means of the lever *H*, which is turned, and set with reference to the arcuate scale *J*. When this lever is turned, a mechanism housed within the base advances the trolley by an amount equal to the reading selected on the scale *J*. The latter has two sets of graduations, one of which reads from 0 to 1 in., in ⅛-in. increments, and the other from 0 to 20 mm., in 1-mm. increments. These graduations are read through a cursor-type window in the lever *H*, and the latter is located in the required angular position by plungers which can be brought into engagement with one of the two notched segments seen above the scale.

The outer segment is used in conjunction with the inch graduations on the scale, and the inner with the millimetre graduations. On the outer segment, there are ten notches in the angular distance subtended by one division on the scale *J*—equivalent to ⅛ in. of movement of the trolley—so the unit can rapidly be set to within 0·012 in. It may be noted that patents are pending on both the marking-out units here described.

Cross Pallet-type Transfer Machine for Operations on Motor-car Steering Gear Housings

The Cross Co., Detroit, Michigan, U.S.A., have recently built the transfer machine shown in Fig. 1 for performing milling, boring, drilling, tapping, deburring, and bush-assembly operations on malleable-iron housings for motor-car power steering gear units.

This machine is of the closed-loop type and the workpieces are located and clamped on circulating pallets. The latter are handled two at a time at each station, and the cycle time is 24 sec. A view of a pallet, with a workpiece secured in position is given in Fig. 2. The casting is clamped from above, by a screw which is applied to a sliding cross-head carrying a fixed and a pivoted pad to ensure a balanced action. This arrangement permits access to four faces of the workpiece, and at two of the machine stations, the pallets are automatically indexed through 90 deg., to enable certain operations to be performed on the side faces of the work. At the loading station, the casting is automatically aligned in the fixture by means of an air-operated pusher, and the screw is tightened by an electrically-powered wrench. When the pallet is transferred to the unloading station, the clamps are automatically released.

The first two machining stations are concerned with rough and finish-milling the pitman cover faces, the vertical spindle heads being equipped with brazed, tungsten-carbide tipped cutters. These cutters are mounted on adjustable adapters,

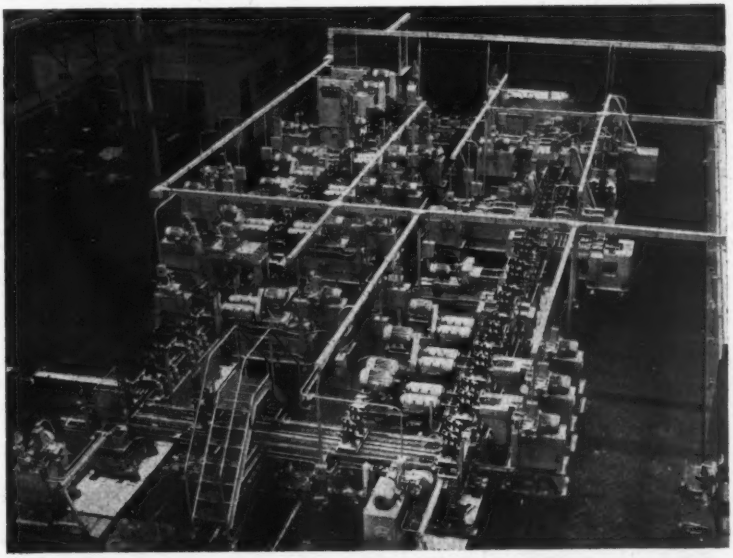


Fig. 1. Cross closed-loop transfer machine for handling power steering gear housings for motor cars

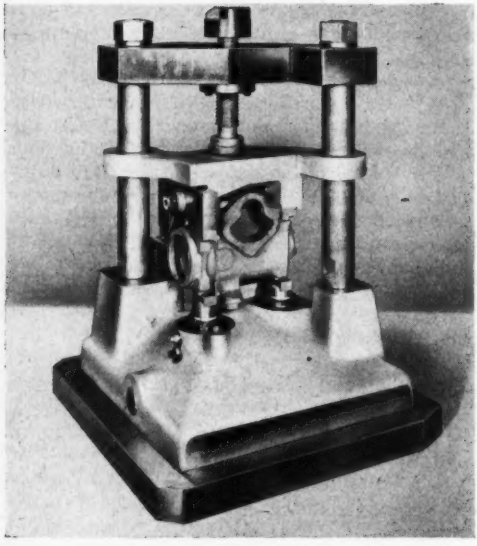


Fig. 2. One of the fixture pallets for the Cross machine, with a workpiece in position

which enable them to be pre-set for cutting size, in a department away from the transfer machine.

Rough and semi-finish boring are next carried out with bars provided with outboard supports, in preparation for finish boring with a standard Cross unit. The pitman and steering shaft holes are bored concentric within 0·004 in. total indicator reading, and to limits of ±0·001 in. on diameter.

BROKEN TOOL DETECTION

At the drilling stations, the drills are monitored by Cross Protect-O-Tool units which are arranged to stop the machine if a drill breaks. At the subsequent tapping operation, after the taps have been withdrawn, the spindle heads are automatically moved longitudinally, and probes, mounted on the same heads, are presented to the holes, to detect the presence of a broken tap. The various internal edges and holes are deburred, mainly by rotating wire brushes which are carried in eccentric housings to provide adjustment for wear.

Gauges are provided at three stations along the machining line for use by patrol inspectors. After all the machining operations have been performed, and before the deburring and assembly stages, the pallets pass to a position from which one or both can be pulled off the transfer conveyor, by an operator, and located at an inspection station as shown in Fig. 3. Here, there are surface plates, a pallet tipping mechanism and various gauges which enable the workpiece to be completely inspected. Provision is made for replacing pallets and workpieces removed from the conveyor, with others that have already been checked, so that no production time is lost.

AUTOMATIC ASSEMBLY

A thrust bearing cup for a worm, and a bush for a pitman shaft, are assembled in each housing after the deburring operation, and Fig. 4 shows the station at which this work is carried out.

Bushes and thrust bearings are fed down chutes from overhead hoppers on the right, and are picked up, in turn, by shouldered assembly mandrels whereby they are automatically pushed into the workpieces.

The latter are supported against the thrust by power-operated mandrels that move forward from the left. If, for any reason, a workpiece is missing from either station, the support mandrel senses the absence of the part, and the assembly mandrel is

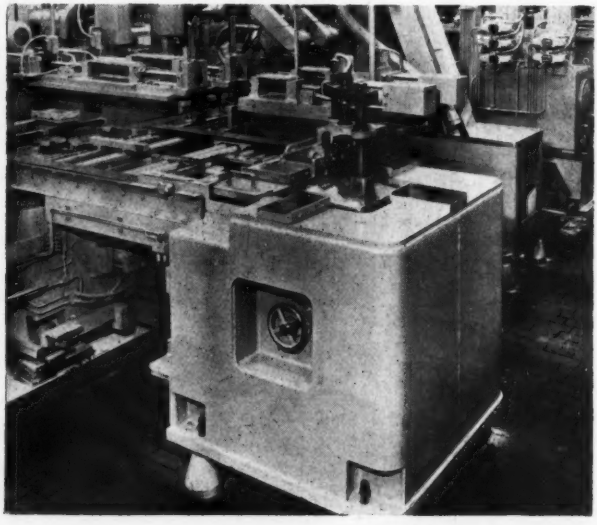


Fig. 3. A pallet which has been withdrawn from the conveyor is here seen at the inspection station

prevented from performing its cycle. In this way, wastage of components is avoided. Since the thrust bearing cups are not symmetrical, they are automatically orientated to face in the correct direction before being delivered to the assembly point. To guard against the possibility of presenting unmachined bushes to the housings, they are checked for diameter before they reach the assembly point.

Capacity has been provided on this machine to enable larger sizes of steering gear housings to be accommodated in the future, if required. Standard Cross units are employed and there are several idle stations that could be tooled-up for any additional operations that may be found necessary at a later date.

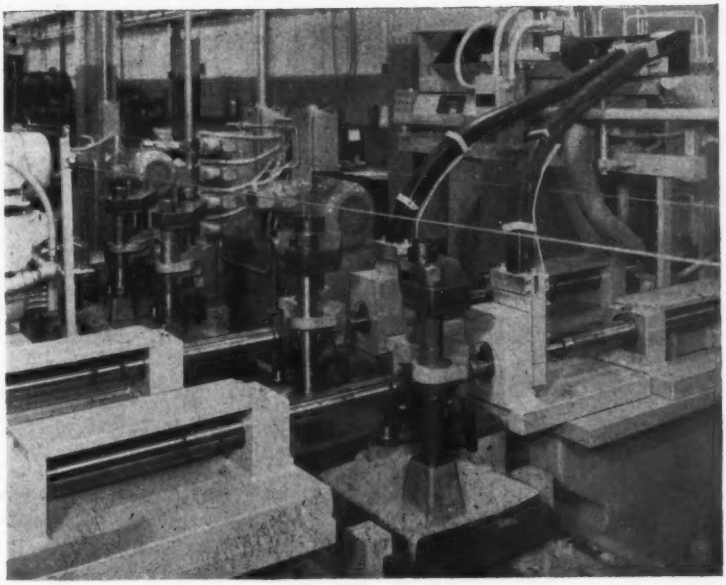


Fig. 4. At this station, the bushes and thrust bearings are assembled, with the castings supported by mandrels which move in from the left

The Cross Co. are represented in Europe by an associate company, Cross International A.G., P.O. Box 300, Fribourg, Switzerland.

Rotary Coolant Filter for 72-in. Aluminium Rolling Mill

A large rotary-type coolant filter has recently been developed for use with the new 72-in. cold mill which is now being installed at the Kitts Green, Birmingham, works of James Booth Aluminium, Ltd. The purpose of the unit is to keep the mill coolant clean, and thus ensure that the rolled products have the required high-quality finish.

The filter unit, which was designed by the Loewy Engineering Co., Ltd., Wallisdown Road, Bournemouth, in conjunction with the company's engineers, was constructed by Windshields of Worcester, Ltd., St. John's Works, Worcester. It measures 12 ft. high, by 10 ft. wide, is more than 20 ft. long, and contains 8,000 gal. of paraffin coolant, the filtration equipment, and two coolant pumps, each with a capacity of 830 gal. per min.

Basically, the unit comprises a large storage tank with a 10-ft. diameter drum, 9 ft. long, mounted transversely across the inside, and free to rotate about a horizontal axis. The outside of the drum is of fine wire mesh, and over it are led two, 50-in. wide, continuous, tensioned webs of filter paper, the feed and take-up mandrels being located above the tank.

Used coolant enters the storage tank through metal filter screens and passes through the filter paper into the centre of the drum. All solids larger than four microns are thus removed, before the coolant is transferred to the pump suction compartment. An automatic system monitors the liquid levels inside and outside the drum, and to compensate for reduced filtration rates, due to the accumulation of sludge on the surface, the dirty side is wound up, and clean paper is fed from the supply reel. The winding mechanism is driven by an air motor.

An agitator unit, oscillated by a geared electric motor and connecting rod, fits closely round the periphery of the drums, to prevent the deposition of sludge on the bottom of the tank. Light alloy extrusions and plate, mainly Duralumin H and MG5, and stainless steel nuts and bolts, were used in the construction of the plant, and with this arrangement, the possible contamination of the coolant by rust is effectively prevented.

K

Fosdick Numerically-controlled Jig Boring Machine

REFERENCE WAS MADE IN MACHINERY, 97/949—26/10/60, to the numerically-controlled Fosmatic jig boring machine displayed by the Fosdick Machine Tool Co., Cincinnati, Ohio, U.S.A., at the Machine Tool Exposition held in Chicago last year, and it was stated that two sizes were available. The machines are designated No. 44P and 54P, and have T-slotted work-tables measuring 44 by 22 in. and 54 by 22 in., respectively. A distance of 27½ in. is obtainable between the spindle nose and the table surface, and the maximum throat depth, which is available for a height of 22 in. above the table, is 25¼ or 30¼ in., according to the size of the machine. The larger type is shown in Fig. 1, in which is also seen the arcuate tool rack referred to in the earlier article. Up to 100 tools can be stored in this rack, and are transferred to and from the spindle, under tape control, by a pivoted arm.

The table and saddle have longitudinal and lateral traverses by hand or power, of 42 and 22 in., or 48 and 28 in., respectively, depending upon the size of the machine, and the counterbalanced spindle head can be adjusted vertically on the column through a distance of 15 in. Each of these slides is mounted on flat ways, and is guided by spaced, inwardly-facing surfaces which form, in combination, a way of truncated V-section, with a small included angle.

Provided with a quick-acting, precision tool-holder at the nose end, the spindle is counter-balanced by a separate system, and runs in matched and pre-loaded, class 9, angular contact bearings. It is housed in a 4⅜-in. diameter hardened alloy steel quill, which is mounted in the head in two re-circulating linear ball bearings and has an axial travel of 9 in. The rack through which movement is applied is attached to the upper end of the quill, to avoid distortion due to thrust from the driving pinion, and the accuracy of the entire assembly is such that spindle run-out at the end of a 12-in. checking bar is guaranteed not to exceed 0·0002 in.

Main drive is taken from a 3-h.p. motor, and 16 spindle speeds from 30 to 1,800 r.p.m. and 8 feed rates from 0·0005 to 0·015 in. per rev. are obtained by means of electro-magnetic clutches in a gearbox. This box is of unit construction, and may be removed without the need for disturbing the remainder of the transmission. In addition, milling feed rates can be obtained for the table and the saddle, also rapid traverse for these members and the quill.

Excluding the tool rack, the machine weighs approximately 9¾ or 10½ tons, according to size, and requires a floor space of 12 ft. square or 13 ft. 4 in. by 13 ft.

Control equipment for automatic positioning is built in, although it may be omitted, if desired, and can then be added at a later date.

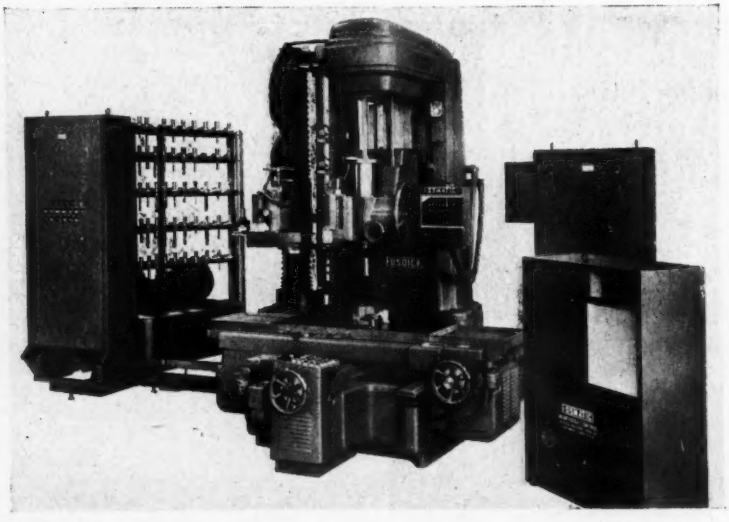


Fig. 1. Up to 100 tools can be stored in the arcuate rack seen at the left of the Fosmatic No. 54 P tape-controlled jig boring machine, and are automatically transferred to and from the spindle by a pivoted arm

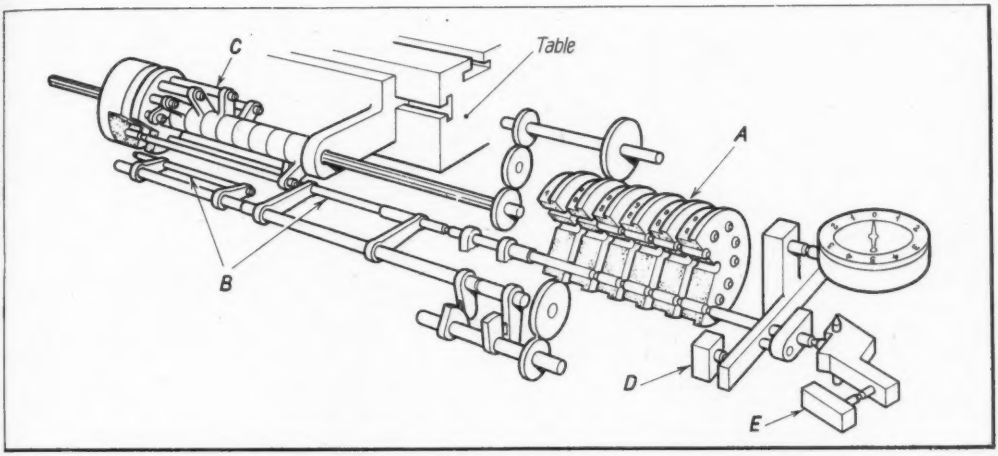


Fig. 2. Diagrammatic illustration of the measuring system for the work-table of the machine shown in Fig. 1, whereby length bars corresponding to the required setting from a zero point are selected by means of dials *A*. Similar systems are provided for positioning the saddle laterally, and for the spindle traverse

The measuring system, and the method by which the table and saddle are traversed to fresh settings, is identical to that provided on manually-controlled Fosdick machines, and there is a set of length bars, made to Class A tolerances, associated with each slide. Positioning is made with reference to a zero point, which may be altered to facilitate setting-up the workpiece, and the required dimensions are selected by means of a series of coaxially-mounted, direct-reading dials. These dials are indicated at *A* in Fig. 2, which is a diagrammatic drawing of the arrangement for measuring in the longitudinal direction.

A number of 10-in. length bars is mounted individually on carriers which are pivoted on a longitudinal shaft, as at *B*, and are swung upwards to the measuring position, as required, by means of the dial at the left-hand end of the series. Movement of this dial is transmitted to a camshaft, and thence through followers which are connected with individual carriers. Bars with lengths that differ by increments of 1 in. provide for obtaining the inch units of the required dimensions, and are housed in the turret *C*, which is attached to the table. This turret is operated by the second dial in the series, motion being transmitted through gearing and a hexagonal shaft. In this way, the required bar is brought into position in line with the previously-selected 10-in. bars. The remaining dials in the series, which provide for obtaining 0·1-, 0·01-, 0·001-, and 0·0001-in. units, house the associated length bars, and the latter are moved directly to the measuring line when adjustments are made. The entire measuring system is totally enclosed, and the bars are chromium plated.

Prior to setting up a dimension, the table is adjusted so that it is farther from the zero point than the required position, thus allowing clearance for the required length bars. After completion of the operation, a push-button is depressed, whereupon the table is traversed towards the zero position at a rapid rate. The stack of bars is closed up during this movement, and eventually operates the limit switch *D* when the table is $\frac{1}{16}$ in. from the final position. Rapid traverse is thereby disengaged, and the remaining movement is made at a slow rate, motion being stopped when the bars operate the limit switch *E*. Finally, the traversing screw is reversed, to release end thrust, and the slide is automatically clamped. A dial gauge, graduated in divisions of 0·0001 in., is provided for checking purposes. Positioning movements of the table and saddle are controlled by separate push-buttons, and may be made simultaneously, if desired.

This system is adapted for numerical control by the addition of electric motors, for turning the selector dials. Drive is taken through gearing, and there is a commutator associated with each dial. A segment of this commutator, corresponding to the required setting, is energized prior to turning the dial, and when it is contacted by a pick-up brush, drive is automatically disengaged by means of a solenoid-operated clutch unit in the transmission.

Vertical movement of the spindle is controlled by a system similar to that employed for table and saddle positioning, and two sets of length bars are provided, for setting the rapid approach distance to 0·010 in., and the feed stroke to 0·0001 in. The system whereby compensation is made for varying tool lengths was described in the earlier article.

Dimensional information is supplied by means of a 1-in., 8-channel punched tape, which is prepared with the aid of Flexowriter or similar unit, and this tape also provides for vertical positioning of the spindle head, and selecting the spindle speed and the feed rate. The tape reader and the information storage system is housed in a separate floor-mounted cabinet, and at the front of this unit there are switches for selecting manual or tape control of the individual functions, also dials whereby dimensional data may be supplied by hand, for transmission electro-mechanically to the measuring system.

Fosdick machines are marketed in this country by Gaston E. Marbaix, Ltd., Devonshire House, Vicarage Crescent, London, S.W.11.

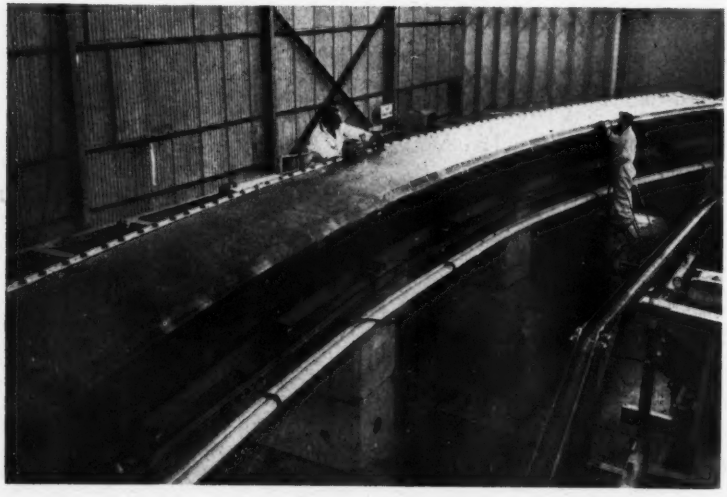
Large Plastics Vacuum Chamber

In the accompanying figure is shown one of a number of arcuate sections which are required for the double-wall vacuum vessel for the Nimrod 7 GeV proton synchrotron now under construction at the Rutherford High Energy Laboratory of the National Institute for Research in Nuclear Science, Harwell.

The vacuum vessel will incorporate outer and inner rings, each composed of eight arcuate portions, and the section shown in the figure is for the outer ring and is 50 ft. long. When the vessel is assembled, it will have a diameter of more than 150 ft.

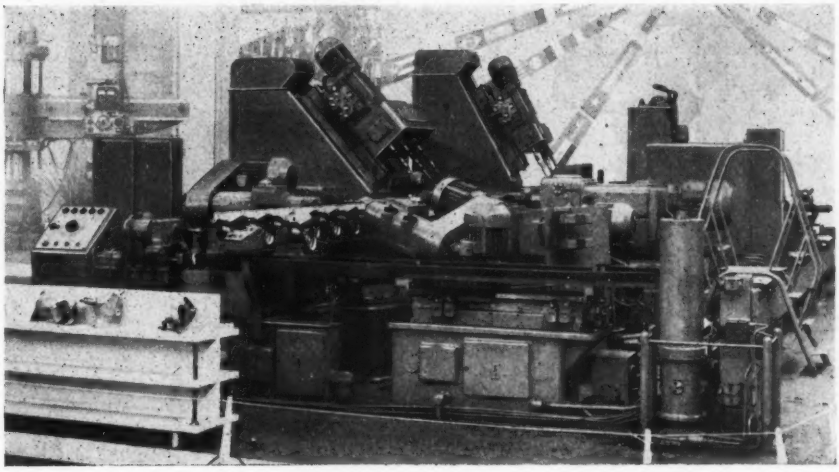
Each arcuate section is made from CIBA Araldite epoxy resin and glass-cloth [CIBA (A.R.L.), Ltd., Duxford, Cambridge] in matched tools, and the section in the figure is claimed to be the largest structure yet made in this manner. The synchrotron, it is stated, will be the first in which laminated plastics have been employed for the vacuum chamber. Considerations which led to the selection of this material included its non-magnetic and non-conducting properties, and high mechanical strength.

The sections are being made by Marston Excelsior, Ltd., Fordhouses, Wolverhampton, and the tolerance on wall thickness for the 50-ft. sections is 0·005 in. In operation, protons will be accelerated through the vacuum vessel to velocities approaching the speed of light.



Made from epoxy resin and glass-cloth, in matched tools, the arcuate section here shown is one of a number which will be assembled to form the vacuum vessel of a 150 ft. synchrotron

CENTRE CUT VICES FOR RAPIDOR MACHINES. Edward G. Herbert, Ltd., Atlas Works, Levenshulme, Manchester, 19, introduced a patented centre-cut vice when the Rapidor Manchester medium duty hack-sawing machine was placed on the market five years ago. Due to the success of this vice, they are making two sizes, one of which can be used on No. 1 and 1A (6- by 6-in. and 8- by 8-in.) machines, and the other on No. 2 and 2A (10- by 10-in. and 12- by 12-in.) machines. With this vice, the saw blade reciprocates through steel-lined slots at the centres of the vice jaws so that both the blank to be cut and the bar stock are held rigidly. It is therefore possible to cut short lengths of material. These are suitable for straight sawing only.



Russian Automatic Transfer Machines at the Leipzig Fair

By R. E. GREEN, Associate Editor

EARLIER ARTICLES in this series on machine tools exhibited by communist countries at the recent Leipzig Spring Fair, have been concerned with the products of the East German factories*, and with standard Russian machine tools† made, for example, by the Ordzonikidze, Krasnoi Proletarii, ENIMS, Dimitrov, Gorki, Kuibyshev, Krasnodar, Stalino, and Odessa plants. Two automatic, in-line, transfer machines, built by the Ordzonikidze machine tool factory, Moscow (MACHINERY, 93/137—16/7/58), for operations on cast aluminium oil filter housings and cast iron main bearing caps for diesel engines, were also shown, and attracted considerable attention.

As in the case of several of the standard machines, these larger units were not for sale but were shown as typical products of the Russian industry. Placed at opposite ends of the large pavilion, the machines were demonstrated in operation for about 5 min. in each hour, and explanatory commentaries in German were then relayed over loudspeakers for the benefit of the large crowds which gathered. The machine for oil filter housings, which operates on a 1 min. cycle time, is here described, and the bearing cap machine will be the subject of a separate article, to be published later.

TRANSFER MACHINE FOR OIL FILTER HOUSINGS

A general view of the machine for oil filter housings—designated type ID 93—from the loading end, is given in the heading illustration, and platen-type fixtures are employed, in which the sand castings are carried to successive stations. A return track for the platens is provided at each end and at the right-hand side of the machine, and unloading and loading are carried out at the same station, so that only one man is required for the operation of the machine. Two finished castings from the machine are shown in Fig. 1, and they are required for diesel engines for vehicles made by the Z. I. Likhachjov Automobile Works, Moscow (MACHINERY, 93/1096—12/11/58), to which the machine will be delivered.

* MACHINERY, 98/939—26/4/61, 98/1006—3/5/61, 98/1074—10/5/61 and 98/1119—17/5/61.
† MACHINERY, 98/1191—24/5/61 and 98/1251—31/5/61.

The castings are of complicated shape, with two rectangular faces measuring approximately 4·12 by 3·25 and 5·75 by 2·5 in., which are disposed at a compound angle to one another. Both these faces require milling, drilling, counterboring and tapping operations, and there is a third, circular, opening, to which the oil filter body is attached in service. This opening has a diameter of about 5·75 in. and a stepped bore for an oil sealing ring of about 4·95 in. diameter is required to be machined, also a central boss which is faced, drilled, counter-bored and tapped. Apart from operations on these faces, several other holes require to be machined in the sides of the casting.

There are six positions at which cutting operations are performed on the machine, usually on more than one casting at a time, and there are 13 unit heads for milling and boring operations, with a total of 35 spindles. The unit heads are from the range of sizes made by the Ordzonikidze factory, and a total of 21 separate motors is employed on the machine, hydraulic pressure being provided by individual floor-mounted units. A continuously-driven, screw-type conveyor extends for the full length of the transfer line, in a trough, and delivers swarf into a container.

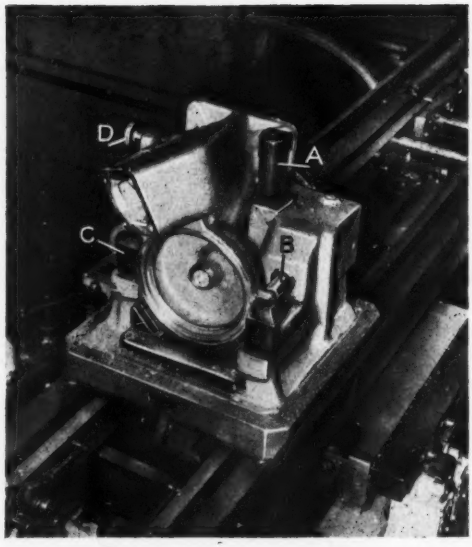


Fig. 2. In the platen fixtures employed on the transfer machine, castings are positioned from the circular housing by V-locations

CLAMPING OPERATIONS

A close-up view of one of the platens—of which there are 41 in all—on the return track, with a finished casting still in position, is given in Fig. 2.

Fig. 1. Views of the oil filter housings for diese engines which are handled on the Russian transfer machine shown in the heading illustration in a cycle time of 1 min.

Of cast construction, the platen has a thick base measuring about 11·75 in. square, with two central T-slots in the under-side, arranged at right-angles, for clamping purposes at the machining stations. In the fixture, the circular housing rests in a V-location with the projecting edge of the larger rectangular flange engaged behind a post *A*, at the top of the fixture. Clamping force is applied to the casting by means of a horizontal screw, turned by a power-driven shaft at the loading station, as shown in Fig. 3.

When it is turned, this shaft moves an elongated plate towards the fixture body, to apply thrust to two horizontal plungers. One of these plungers is seen at *B* in Fig. 2, and it presses against the small cylindrical projection on the side of the circular housing, to clamp it against a fixed abutment on the platen. The second plunger acts in a similar manner, to clamp an angular surface on the casting against the abutment *C*. A knurled-head screw *D*, at the side of the fixture, is then tightened to steady the casting and to reduce vibration

during sequence of machining operations performed.

In Fig. 3, the platen fixture is in the unloading position, at which the sequence of operations just described is performed in reverse. The shaft *E* carries the driving socket which is moved forward into engagement with the teeth of the driven member on the fixture by means of the small hydraulic cylinder *F*. The ram of this cylinder has a slot which is engaged by a lever *G*, secured to the end of a cross-shaft, and this shaft also carries a forked lever, extending upwards. The fork of this second lever engages a groove in the socket shaft, and when the cylinder is energized, the socket is thus moved axially on a splined shaft, into or out of engagement with the fixture coupling.

PLATEN TRANSFER, LOCATING AND CLAMPING ARRANGEMENTS

On the transfer line, each fixture is aligned by means of the central T-slot, which is engaged by a longitudinal tenon between the supporting ways. Transfer is effected by a single long shaft which extends for the length of the machine between the ways, on the left-hand side facing the direction of transfer. Other references, hereafter, will imply this direction, except where stated. Short dowels of about 0·75 in. diameter, projecting from the bar at intervals, engage the cross T-slots in the platens when the bar is turned through 45 deg. Turning is effected by a single hydraulic cylinder, the ram of which is connected by a lever to an axially stationary splined bush on a corresponding portion of the bar.

The bar is moved longitudinally, to transfer the platens from one station to the next, through a distance of about 12 in., by a travelling milling head on the left-hand side of the track. This head is seen at *J* in Fig. 3, and it has a side projection which is connected to the bar. Before the milling traverse of the head—towards the camera—is started, the bar is turned to disengage the dowels. At the end of the milling pass, the bar is turned to re-engage the dowels, and as the head is returned to its starting position, the platens are moved from one station to the next.

Operations on castings are performed on groups of two or three in adjacent platens, so that one unit head, fitted with a suitable adapter, can be employed to full advantage. This arrangement also enables locating and clamping mechanisms for the platens to be operated in groups by single hydraulic cylinders. No other provision is made for the location of the platens at the idle stations apart from the tenon mentioned, but bushed holes of about 1 in. diameter are provided at the corners of the platens, on the under-side, for accurate location at the loading station and those employed for machining.

Two plungers are raised into engagement with the holes in each platen by means of a hydraulic cylinder, acting through linkages and racks and pinions, at each station or group of stations, the cylinder for the plungers at the loading station being seen at *H* in Fig. 3. For clamping the platens there are two T-headed plungers at each machining station, the thin portion of each plunger-head being aligned with the guiding tenon so that the T-slots in the platens engage the heads automatically. When the plungers are

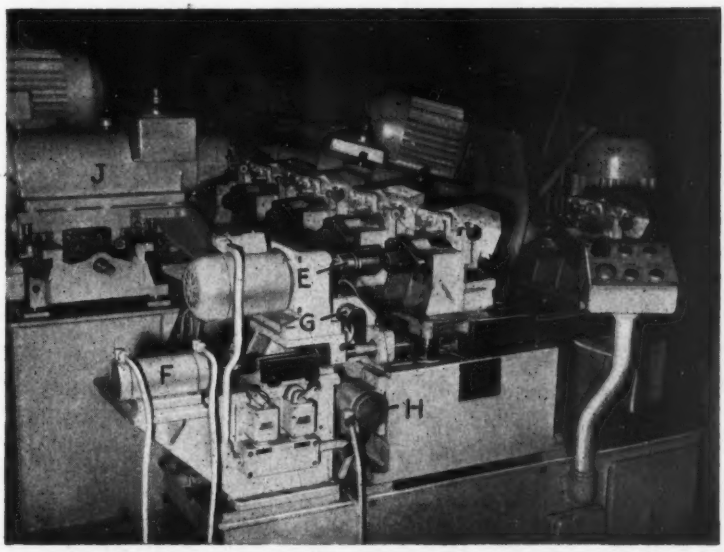


Fig. 3. This close-up view of the loading station shows the automatic unit for tightening and releasing the clamps on the platen fixtures. The hydraulic cylinder *H* raises locating dowels for the platen

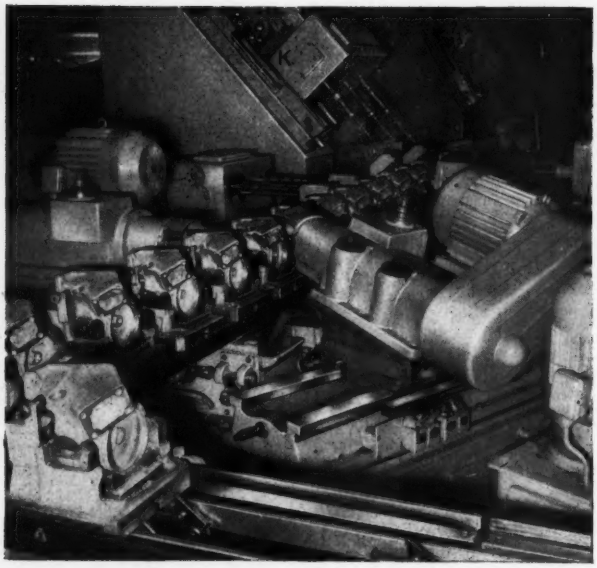


Fig. 4. Face milling operations on the two rectangular faces of the casting are performed at the first machining station. The head at the left also serves to move the transfer bar

moved down by their actuating cylinders, the platens are clamped to the supporting ways.

MACHINING OPERATIONS

Although there was no coolant supply on the machine as demonstrated, a soluble oil emulsion is to be used when it is finally installed, for all but the tapping operations, for which paraffin will be provided. Machining speeds for milling, drilling and tapping are of the order of 1,300 to 1,380, 115 to 130, and 32 to 39 ft. per min. respectively, and the feeds have been calculated to ensure that all operations are completed within the 1 min. cycle time. After leaving the loading position, each platen passes through three idle stations before reaching the first working station, at which the rectangular faces at each side of the casting are machined.

The spindle of the travelling milling head *J*, Fig. 3, is fitted with a face-milling cutter of the inserted-blade type, of about 4·5 in. diameter, with six carbide-tipped inserted blades, which machines the narrower of the two rectangular faces. On the right-hand side of the transfer track, at this position, there is a second milling head, arranged at the required compound angle, as seen in Fig. 4. The spindle of this head is fitted with a cutter of 6 in. diameter, again with six carbide-tipped inserted blades, and the head travels towards the loading position for the milling operation on the angular face.

The heads are of similar, simple design, the spindles being driven directly through multiple V-belts, and each head is mounted on a slide which carries a hydraulic cylinder, the ram being coupled to the stationary base. Movements of the heads are controlled by adjustable dogs at the sides, which operate lever-actuated limit switches on the bases. The compound angle on the side of each casting is obtained by locating the slideway base at the required angle to the transfer track, and inserting a wedge of the appropriate angle between the slide and the spindle head.

Three more idle stations follow, before the platens reach a station at which operations are performed on two castings simultaneously by spindles in common heads, as seen in the background in Fig. 4. The four spindles in the head at the left operate on the narrower rectangular face, three holes of 0·375-in. diameter being drilled near three corners of the face of one casting, and a larger hole, of about 0·45 in. diameter, near the centre of the face of the casting in the adjacent platen. There are two spindles in the head at the right-hand side of the track and while the boss at the centre of the circular housing of one casting is being drilled, the hole in another casting, at the adjacent position, is countersunk.

Of conventional design, each drilling head incorporates a driving motor and a reduction gearbox, carried on a hydraulically-operated slide similar to those for the milling units. On the front face of the gearbox is mounted a multi-spindle adapter, designed to suit the operations to be performed. Provision is made on the side of the gearbox for adjustments to the feed rate, by means of flow-control valves, but spindle speeds cannot normally be changed except by dismantling the unit.

One more idle station follows, and at the next three positions, different castings are machined simultaneously by spindles in common heads at both sides of the track. The spindle head at the left is mounted at an angle, as seen at *K* in Fig. 4, and it

Fig. 5. Taken from a point about one third of the way along the transfer track, this view shows the unit head *M*, which has two drills for operations on castings at adjacent platen positions on the track

has three spindles equipped with drills of successively greater length and smaller diameter, for operations on the off-centre oil-transfer hole *L*, Fig. 1. This hole is drilled right through the casting to communicate with the central boss in the circular housing at the opposite side. At the first two positions, the drills are guided by bushes in brackets secured to the side of the machine bed.

The spindle head on the right-hand side of the track at this position has two spindles which operate on the circular housing. The first spindle is fitted with a cutter head having six inserted blades for facing and boring the large opening. For operations on the central boss of the casting at the adjacent position, the second spindle has a combination tool with sets of four, four, and two inserted blades, designed to face and step-bore the boss in one pass.

Three more idle stations allow space for setters to work on the machine, and are followed by three further positions at which operations are performed, as seen in Fig. 5. At the left there is a head *M* arranged at a compound angle, with two drilling spindles for machining the hole *N*, Fig. 1, which communicates with another hole drilled from the opposite side. This hole, it will be noted, is drilled in stages at adjacent positions. On the right-hand side of the track, the head is also at a compound angle to match the inclination of the rectangular face, and it is equipped with ten spindles which operate on this face. The drills

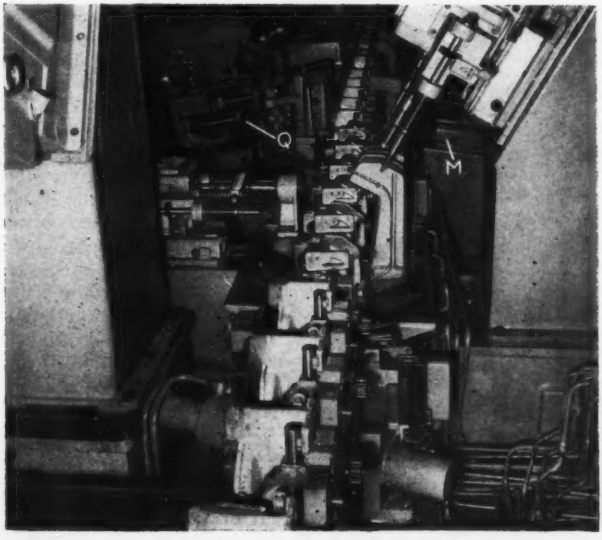


Fig. 6. After passing the station shown in the foreground in Fig. 5, the platens reach a turn-round station where they are swivelled through 90 deg. to enable operations to be performed on the side faces

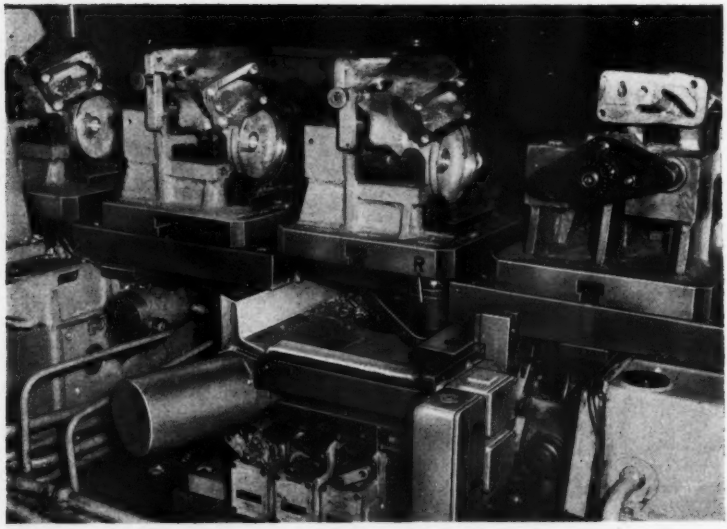


Fig. 7. Close-up view of the turn-round station. A central plunger, with a cross-bar carrying dowel-holders *R*, raises the platen clear of the transfer track and turns it through 90 deg.

carried by these spindles are supported in guide bushes in substantial holders *P*, Fig. 5, which are guided on pillars at each side and are spring-loaded towards the work.

As the head advances, the holders are carried forward almost into contact with the faces to be drilled, until bushed holes in the flanges engage locating dowels on heavy brackets secured to the side of the bed. The bush-holders are thus accurately positioned, relative to the work, before the drilling operations begin. Four of the drills in each group are employed to drill holes of about 0·375 in. diameter near the four corners of the rectangular face in one casting, and to chamfer the holes in the casting at the adjacent position. At the centre of each group there is a fifth drill which is applied to the interior of the rectangular housing, to machine the hole communicating with that indicated at *N* in Fig. 1. This drilling operation is completed in stages at adjacent work positions, and the movements of the heads are so timed that the drills do not interfere on breaking through.

At the far side of the head there is a bracket carrying four probes which are spring-loaded towards the casting at the next position along the line. This bracket is seen at *Q* in the view looking in the opposite direction along the transfer track seen in Fig. 6, and the four probes which it carries enter the holes which are drilled and chamfered at the previous stations. Should these probes be prevented from entering because a drill has broken or a hole has not been machined to depth, a limit switch is operated and the machine cycle is interrupted. A lamp is then lit to indicate the position at which adjustment or tool changing is required.

TURN-ROUND TABLE

After passing the proble unit, the platen moves through an idle station before reaching a position at which it is turned through 90 deg. about a vertical axis, in a clockwise direction, as viewed from above.

A close-up view of this unit, from the left-hand side of the track, after the completion of the turning cycle, is given in Fig. 7. At the turning station, the platen rests on a portion of the support track which is narrower than the remainder. Beneath the track there is a cast housing with a central vertical plunger carrying a cross-bar. At each end, this bar has a cylindrical projection *R* which houses a dowel of the same diameter as those employed for location purposes.

A hydraulically-operated mechanism within the housing is designed to raise and lower the central plunger, and when it is raised, the dowels enter the locating holes in the corners of the platen. Further upward movement then lifts the platen clear of the transfer track, and the plunger is next rotated through 90 deg. by a hydraulically-operated rack and pinion arrangement, to turn the platen to the position shown. The plunger is now lowered, to deposit the platen on the transfer track with the second T-slot engaged with the line tenon, and the dowels are withdrawn from the locating holes. Finally, the plunger is returned to its original angular position, ready for the next turning cycle.

Automatic turning, which is completed within the machining portion of the cycle, after the return of the transfer bar, is controlled by means of limit switches on the outside of the housing, whereby solenoid valves in the hydraulic circuit are operated. The limit switches are actuated by means of stops on slides which are connected to, and moved

by, the raising, lowering and turning mechanisms within the housing. Another idle station follows the turn-round position, as seen at the left in Fig. 7, and the platens are next advanced to the machining stations seen in the foreground in Fig. 6.

Castings at the next two operating stations are machined by heads at each side of the track, the head at the right in Fig. 6 (on the left facing in the direction of transfer), being provided with two spindles equipped for successive drilling and spot-facing operations. The head is mounted in a nearly vertical position, and operates on the hole *S*, Fig. 1, near one corner of the casting, to drill and spot-face diameters of approximately 0·56 and 1·56 in. diameter. At the near side of the head there is a probe which enters this hole when the casting is moved to the next station to check that it has been drilled to depth in readiness for the subsequent tapping operation.

The head at the left in Fig. 6 is employed to drill the boss *T*, Fig. 1, on the side of the circular housing, and it also carries a probe which enters this hole at the next station to check that it is clear for tapping. Following these three stations there is again an idle position before the platen reaches a second turn-round station, of similar design to that shown in Fig. 7. Here, the original orientation of the platen is restored, and it then proceeds through another idle position to the station in the immediate foreground in Fig. 6.

LATERAL TAPPING STATION

In this position, the platen is aligned with the lateral transfer ways seen at the left in Fig. 6, which lead to a tapping station located some 6 ft. from the main transfer track, as shown in Fig. 8. The arrangement of the tapping station remote from the remainder of machine has the advantages that a different lubricant for the taps can be employed. Moreover, the tapping heads can be grouped round the casting so that all the holes are threaded at a single operation. At the position on the main track from which the platen is moved to the tapping station, the main tenon is replaced by projections from a slide between the ways of the lateral track.

This slide is coupled, by means of two cylindrical bars, to another slide on ways to the right of the main track, as viewed in Fig. 6, in line with the lateral track. The second slide carries a rack with vertical teeth and there is a similar rack secured to the base member. Meshing with both these racks is a pinion, mounted on a vertical shaft on a smaller slide which is connected to the ram of a hydraulic cylinder between the ways. With this arrangement, the movement of the pinion is amplified so that both the stroke and the speed of movement of the ram are doubled.

The platen is pushed along the lateral ways to the tapping station, being guided by a tenon which engages the transverse T-slot in the under-side. At the tapping station, this slot is moved into engagement with T-headed clamping plungers which are pulled down to secure the platen in position, after the locating holes have been engaged by rising dowels, as on the main track. Each of the tapping heads seen in Fig. 8 operates on an automatic cycle which is initiated as soon as the clamps have been applied to the platen, and is advanced under lead-screw control. Holes tapped at this station include the four at the corners of the wider rectangular face, those in the central and side bosses of the circular housing, and that indicated at *S* in Fig. 1.

Fig. 8. With the platen moved out from the main transfer track along a lateral track, tapping in four directions is carried out simultaneously

L2

Fig. 9. After returning to the main track, the tapped casting enters this station at which it is raised into a sheet metal housing to be washed and vibrated for swarf removal before passing on to the return track seen in the foreground

At the end of the tapping movement, the spindle and leadscrew of each head are reversed by the action of a switch within the head, actuated by a stop disc geared to the spindle, and the head automatically withdraws. When the locating dowels have been retracted and the clamps released, the direction of the oil supply to the slide-actuating cylinder is reversed to move the platen back to its original position in the line. The complete cycle of movements of the platen to and from the tapping station, and the tapping operations, are carried out during the 1 min. cycle time of the machine. From the line position opposite the tapping station, the platen is passed through two idle stations before moving into the pick-up position for a chip-dumping unit at the left-hand side of the track, as seen in Fig. 9.

CHIP-DUMPING AND PLATEN-RETURN ARRANGEMENTS

At this position, the platen is moved into engagement with grooves at the lower ends of two inverted U-shaped arms which are connected by cross-bars to form a frame. The arms are carried on a shaft at the side of the track which can be turned by means of a rack and pinion, actuated by a hydraulic cylinder. When the shaft is thus turned, the platen is lifted in an arc into a sheet metal housing at the side of the track, where it is subjected to the washing action of sprays of coolant in the completed installation. In the raised position, the frame is turned through an angle of about 110 deg. and it rests against stops within the housing.

Beneath the position occupied by the frame there is a second hydraulic cylinder, the ram of which is connected to a bell-crank lever. This cylinder is so arranged that the ram can be reciprocated automatically, and the other end of the bell-crank lever is thus brought into contact with the frame. A series of rapid blows is thus imparted to the frame during a period of about 2 sec., and the swarf dislodged is then washed into the trough of the swarf conveyor, seen beneath the unit in Fig. 9, which discharges at this end of the machine. The platen is next returned to the transfer track and three successive indexing movements brings it on to the first portion of the return track, in the foreground in Fig. 9.

This return track has supporting surfaces of the same width as the platen, and raised strips at each side for guidance. Between the supporting tracks is the transfer mechanism which incorporates two rectangular-section bars spaced about 8 in. apart. These bars are held on slides which are similar to those for the transfer mechanism serving the tapping station, and each bar carries a number of spring-loaded pawls. The pawls are pushed down by the platens during the return movement of the transfer bars, and rise again on the opposite sides. When the bars are again moved forward, therefore, the platens are indexed along the conveyor tracks.

The transfer cylinder is continuously actuated until the platen reaches a position near the end of the return track, where it operates a limit switch. This position is shown in Fig. 10, and it will be observed that the first portion of the return track leads to a platform *V*. This platform is secured to the side of a large hydraulic cylinder *W*, which can be moved vertically on its fixed ram, and with the cylinder in the raised position, the platen is moved on to the platform at the next indexing movement of the return transfer mechanism. The platform has a slot in the under-side, and when it is subsequently lowered, the slot straddles a con-

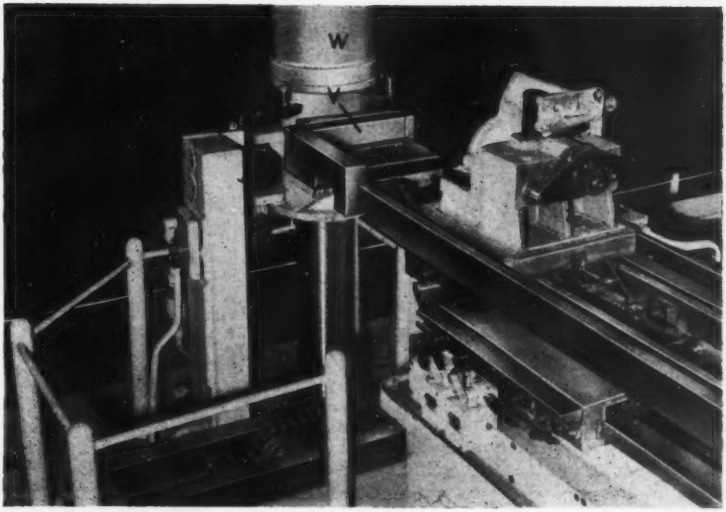


Fig. 10. At the end of the first leg of the return track, the platen is lowered by this hydraulic lift to a floor-level conveyor on which it returns to the loading station

tinuous roller chain extending along the portion of the return track which is parallel to the main transfer track of the machine, and at floor level.

The chain is driven intermittently by a motor at one end of the track, and it carries pawls which push the platen along until it eventually reaches a similar elevating platform near the loading end of the machine, as seen at the right in the heading illustration. This platform is so designed that the transfer bars of the end track, which is of similar design to that at the unloading end of the machine, can pass through slots to a position at which the transfer pawls can engage the platen and withdraw it. The platen is then indexed to the position where it is unloaded and re-loaded. Because of the difficulties of transport, the machine was demonstrated at Leipzig by re-cycling the castings continuously.

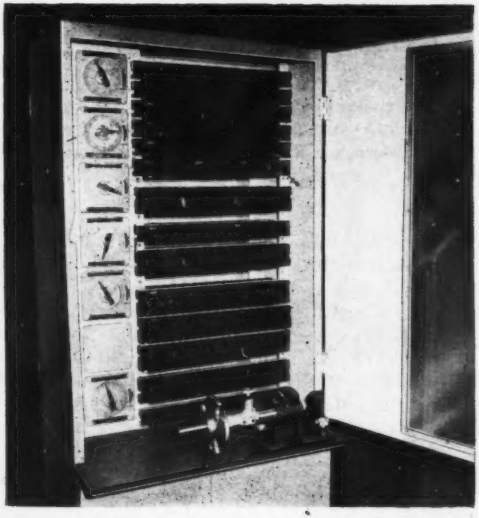


Fig. 11. Control of tool life for each station is obtained by means of dials in this cabinet, with pointers which are moved at each machine cycle. Provision is made for storing a spare set of tools, and for pre-setting them in their holders

Clamping and unclamping, and starting and stopping of the machine cycle are effected by means of push-buttons at the right of the loading station in Fig. 3, and the machine can also be manually controlled by means of a multi-position rotary selector switch on a separate panel, seen at the extreme left in the heading illustration. Behind this panel there is a cabinet containing the tool control equipment, with a glass-panelled door which is normally closed and locked. A view showing the equipment within this cabinet is given in Fig. 11, and it will be noted that there are six dials, each with two pointers.

Dials of two different types are provided, graduated in numbers from 0 to 2,400 and 0 to 10,000, to suit the particular operation to be recorded, and each dial relates to one of the machining stations of the transfer line. One of the pointers is set to the number of cycles which a set of tools will complete before it requires to be changed, this number varying according to the nature of the work performed. The other pointer is aligned with the fixed pointer when new tools are fitted, and at each machine cycle it is indexed towards the zero point. When zero is reached the machine stops automatically, and a lamp is illuminated to show that a tooling change is required.

To the right of each dial, there are wooden bars with holes to suit the shank diameters of the tools, to accommodate a complete spare set. A setting jig, as shown on the shelf beneath, is also provided, to enable the tools to be pre-set for length in their holders, before they are fitted to the machine spindles.

Use of Noral 28S Alloy for Lens Mounts

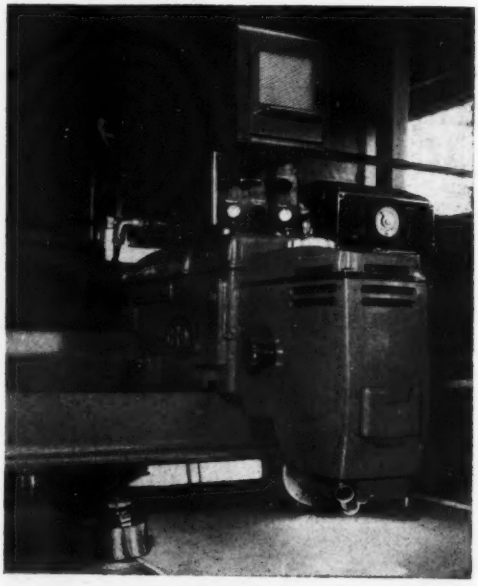
Various photographic and television lens mounting components, examples of which are shown in the figure, are now being produced by Taylor, Taylor & Hobson, Leicester, from Noral 28S aluminium alloy supplied by Alcan Industries, Ltd., Banbury. Machining properties of this alloy, it is stated, compare favourably with those of free-cutting brass. There is no build-up of metal on cutting edges, and long, continuous strands of swarf are not produced. In addition, the alloy has the advantages of being considerably lighter and cheaper than brass. It is normally supplied in the form of bar in sizes up to about 4 in. diameter, but is also available in the form of drawn wire, tubing, and simple extruded sections.

Noral 28S can be readily treated to produce a corrosion-resistant anodic film which will absorb dyes. For lens mounts, the film is dyed black prior to the application of matt black enamel on all internal surfaces. It is thus ensured that a bright metal surface is not exposed should the enamelled coating be damaged in service. External surfaces of the lens mounts are frequently coated with synthetic resin lacquer.

Examples of lens mounting components produced from Noral 28S aluminium alloy

B.O.C. Automatic Line Following Unit

British Oxygen Co., Ltd., Bridgewater House, St. James's, London, S.W.1, have introduced a new automatic line-following unit for profile flame cutting, which enables burner head movements to be controlled from a line drawing prepared in pencil or ink, for cutting shapes from steel plates. A B.O.C. Bison oxygen profiling machine fitted with the new unit, as shown in the illustration, was demonstrated on the company's stand at the recent Engineering, Marine, Welding and Nuclear Energy Exhibition.



The new B.O.C. automatic line-following unit is here shown mounted on a Bison profile cutting machine. Automatic compensation for kerf width is provided, and printed circuits and transistors are employed in the control system

Settings can be made with the aid of a dial to give automatic compensation for kerf width, and components can be cut from plates of any thickness within the capacity of the machine, from the same drawing. The unit incorporates an optical scanning head, which has a non-vibratory photo-transistor cell. Printed circuits and transistors are employed in the control system, which provides for comprehensive electronic interlocking.

Production of Components for Compressed Air Equipment

Some Interesting Set-ups at the Farnham Works of Martonair, Ltd. and Nuquip, Ltd.

By G. W. MASON, Associate Editor

AT THE FARNHAM WORKS of Martonair, Ltd., Richmond, and Nuquip, Ltd., machines built by the company have been installed for the quantity production of component parts for their range of air cylinders, and for performing operations on heads for lubricators which are incorporated in compressed air lines.

The machine shown in Fig. 1 is employed for drilling intersecting stepped-diameter holes in one end face and an edge of the end covers for a 2½-in. diameter air cylinder. Machined from hot brass pressings, the 2$\frac{15}{16}$-in. square end covers have an overall thickness of 1¼ in., and the holes, which are indicated at *A* and *B* in the sectional view, Fig. 2, serve to restrict the flow of air discharged from the cylinder during the final part of the working stroke, so that a cushioning action is obtained. In the final assembly, the tapped central portion of the hole *A* is fitted with a needle valve that is threaded 4 B.A., and enables the rate at which air is discharged from the cylinder during the final part of the piston travel to be varied. For most of the working stroke, air is discharged from the cylinder by way of the $\frac{3}{16}$-in. diameter hole *C*, but during the final part of the movement, an enlarged-diameter portion on the piston rod enters the 1$\frac{3}{16}$-in. diameter bore in the end cover. Air in the space between the opposing faces of the piston and the end cover is then admitted to the hole *C* by way of the holes *A* and *B*.

Referring again to Fig. 1, end covers are stacked, as indicated at *D*, between two pieces of angle iron which form a magazine at the right-hand end of the machine. At each working cycle, which occupies about 20 sec., the lowest component in the stack is moved to the left, on a pair of guide rails in the tunnel-shaped drilling fixture *E*, by a pusher bar operated by a horizontally-mounted air cylinder, and is thus brought to the first drilling position. At the same time, partly completed components in the fixture are advanced for a distance which corresponds to their width. In this way, alternate end covers are brought into line with the drilling spindles at each movement of the pusher bar.

End covers at the drilling stations are simultaneously located and clamped by cone-ended pins attached to steel plates, which are moved downwards (into engagement with tie-rod holes drilled in the components at a previous operation) by the action of four air cylinders, flange-mounted on top of the fixture. At the first three working stations, different operations are performed for drilling the stepped-diameter hole *A* in the edge of each end

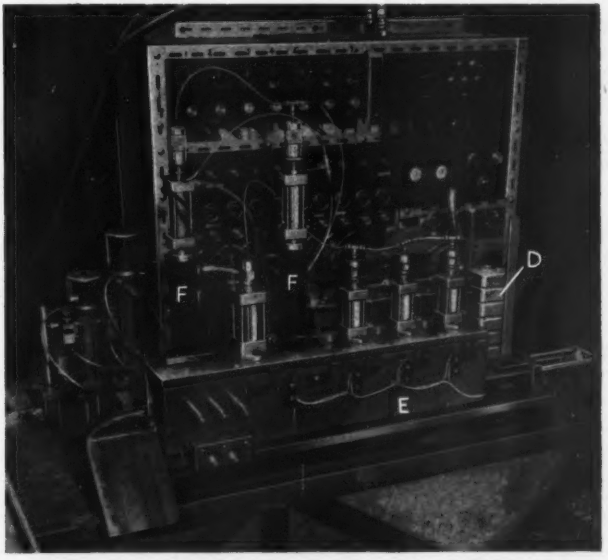


Fig. 1. This machine has been built by Martonair, Ltd., for drilling intersecting, stepped-diameter, holes in end covers for air cylinders, on a fully-automatic cycle

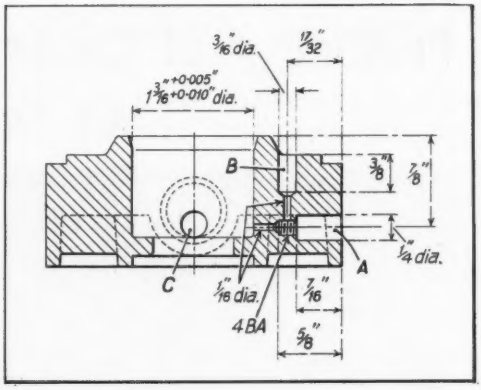


Fig. 2. Sectional view of an end cover for a Martonair air cylinder. The stepped-diameter holes indicated at *A* and *B* are drilled on the special-purpose machine shown in Fig. 1 in a cycle time of about 20 sec.

cover, by horizontal spindles at the rear of the fixture, which are driven by V-belts and pulleys from an electric motor. The stepped-diameter hole *B* is drilled in the end surface of the cover, at two operations, by the vertically mounted units *F*, the spindles of which are driven by Desoutter air motors. Feed and rapid traverse motions for all the drilling spindles are provided by air-hydraulic cylinders. When the drilling operations have been completed, the cover is pushed clear of the left-hand end of the fixture, and is discharged from the machine down an inclined chute, by the action of loading another component at the right-hand end.

The various motions of the machine are interlocked by a separate low-pressure air system. For this purpose, air at about 10 lb. per sq. in. pressure is delivered to units on top of the clamping cylinders, and through holes in metal plates which serve as stops for controlling, positively, the working strokes of the drilling spindles. When the workpieces have been clamped, all the inlet ports for the delivery of low-pressure air to the units are obstructed by extension pieces on the piston rods for the clamping cylinders, and the resulting build up of pressure in the system operates a diaphragm valve which initiates the drilling operation. At the end of the drilling stroke, seating plates on the spindles make contact with the stops, and, at the same time, obstruct the holes to prevent the escape of air. When all the holes have been closed in this way, pressure in the system again builds up to operate another valve incorporated in the circuit, which is arranged to initiate the return travel of the spindles.

Other machines of generally similar design are employed at the Farnham works for performing various drilling operations on end covers for different sizes of air cylinders.

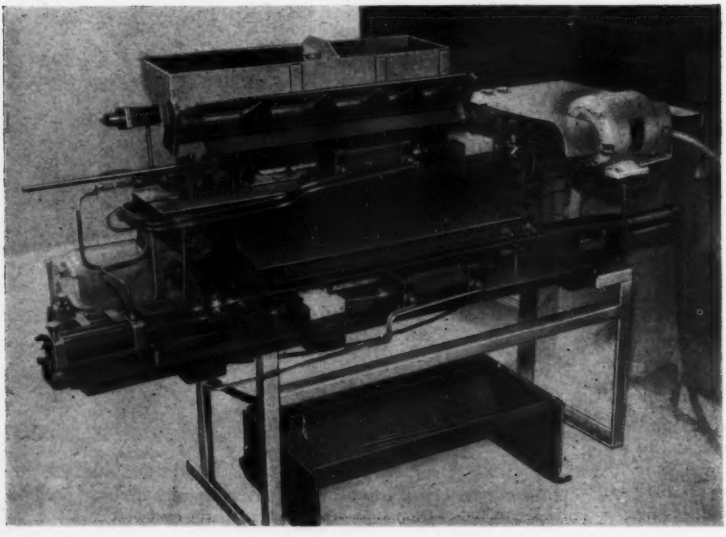


Fig. 3. Tie rods for air cylinders are chamfered at both ends, in preparation for threading, in a fully-automatic continuous cycle on this machine

CHAMFERING AND THREADING OPERATIONS ON TIE RODS

In Fig. 3 is shown a machine which has been built by the company for chamfering both ends of tie rods for air cylinders on a continuous fully-automatic cycle, and a close-up view is given in Fig. 4. Tie

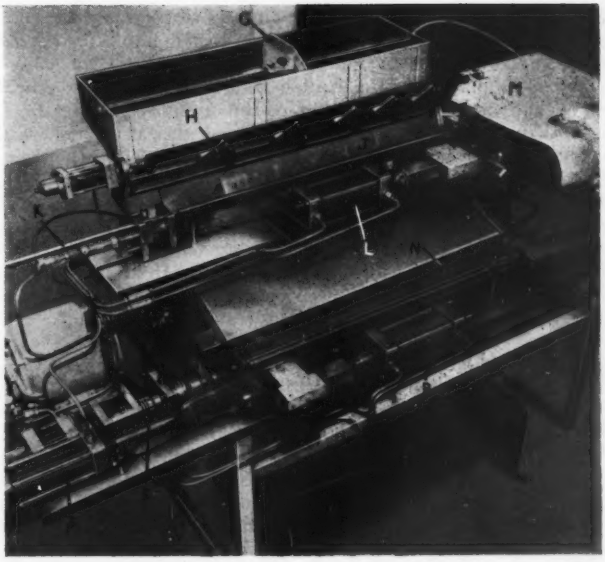


Fig. 4. Close-up view of the chamfering machine for tie rods shown in Fig. 3

rods to be chamfered, which may have diameters from ¼ to ⅜ in., and lengths from 4 to 22 in., are loaded into a hopper on top of the machine, at the right-hand side of the adjustable stop plate *G*. The rods then pass down a short chute at the bottom of the hopper, and are held at the lower end of this chute by projections at the right-hand ends of two or more of five swivel stops, one of which is indicated at *H*. These stops are connected to each other by a horizontal bar, and at each working cycle they are swivelled simultaneously by a short-stroke air cylinder at the left-hand end of the machine. As a result, the leading tie rod falls into the V-shaped trough *J*, but the remaining rods are held by projections at the left-hand end of the stops *H*. The stops are then returned to their original positions, and the projections prevent another tie rod from falling into the trough *J* during this movement.

A pusher bar, indicated at *K*, which can be adjusted in an axial direction to suit the length of the tie rods to be chamfered, is now traversed to the right by another air cylinder to move the rod in the trough into contact with a swing-type end stop. Next, the tie rod is held by gripper jaws, which are closed by means of a wedge, operated by the air cylinder *L*. At the same time, the stop is swung upwards clear of the work. A motor-driven spindle, fitted with a shell-type cutter, which is mounted beneath the cover plate *M*, is now advanced by a fourth air cylinder to perform the chamfering operation on the right-hand end of the tie rod. When the cutter spindle has been returned to its original position, and the gripper jaws have been opened, a plate which forms the bottom of the trough *J* is swung clear by an air cylinder at the rear of the machine, and the tie rod falls on to an inclined sheet metal guide, to be directed into a second

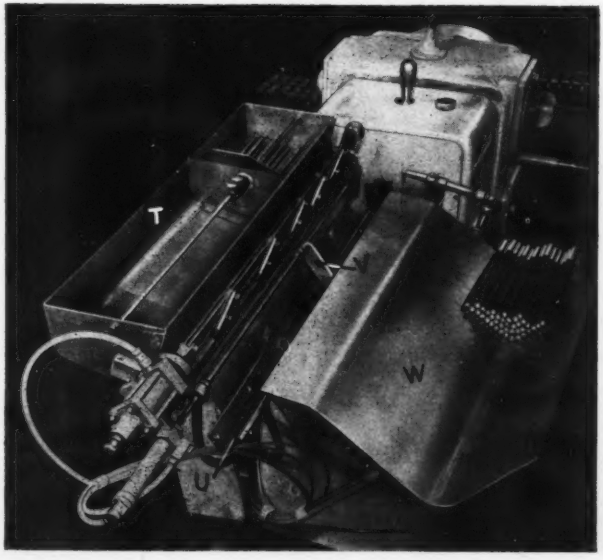


Fig. 5. When chamfering has been completed, threads are cut on both ends of the tie rods on this Edgwick machine, which has been fitted with work handling equipment and converted for fully-automatic operation by Martonair, Ltd.

trough indicated at *N*. Thereupon, the stops *H* are swivelled to allow another tie bar to fall into the trough *J*.

A pusher plate, which can slide on a cylindrical guide bar attached to the front of the trough *N*, is now moved to the left by means of the air cylinder *P*, to bring the non-chamfered end of the first tie bar into contact with a second swing stop. Next, the pusher plate is returned to its starting position by another air cylinder at the right-hand end of the machine. The pusher plate is attached to a steel cable, which extends in front of the machine, and passes round a pair of rollers at each end. The outer roller of each pair is mounted in a forked end piece attached to the piston rod of one of the air cylinders, and with this arrangement, the pusher plate can be traversed for the full length of the trough *N*, if required, by a fairly short movement of the piston.

As soon as the tie rod has been brought into contact with the swing stop, a second pair of gripper jaws is closed by the action of another wedge operated by the air cylinder *R*. Next, the motor-driven cutter spindle *S* is advanced, again by an air cylinder, to chamfer the left-hand end of the tie rod, and during the first part of its travel, a plate-type cam attached to a moving part of the spindle housing causes the swing stop to be brought clear. When the spindle *S* has been returned to its starting position, another plate, which forms the bottom of the trough *N*, is swung clear, and the chamfered tie rod falls into a container that rests on the shop floor beneath the machine.

Following chamfering, screw threads are cut on both ends of the tie rods at separate operations, on an Edgwick (Alfred Herbert, Ltd.) threading machine, which has been fitted with work-handling equipment, and converted by the company for operation on a fully-automatic cycle. A close-up view of this machine showing the work-handling equipment is given in Fig. 5. From the hopper *T*, tie rods are released into the trough *U*, one at a time, at each working cycle, by way of two or more of five swivel stops, which are of similar design to those seen at *H* in Fig. 4. When a tie rod has been loaded into the trough *U*, the pusher arm *V* is swung downwards to the position shown, and then advanced to pass the rod between the jaws of the work-holding vice. The cylindrical bar which carries the pusher arm is moved in an axial direction by an air cylinder, and the swivelling motion is obtained from a twisted, square-section end piece, which passes through a support bracket attached to the hopper at the end nearer to the die head on the machine.

As soon as the pusher arm has been brought to the end of its stroke, the vice jaws are closed by the action of another air cylinder, and the arm is then swung clear. The handwheel normally provided on the machine for traversing the slide for the vice on the bedways, has been removed, and the pinion shaft is now turned by a third air cylinder, through an arrangement of links, to feed the tie rod into the die head. When the vice jaws have been opened at the end of the return travel of the slide, following the screw-cutting operation, the trough *U*, which is carried on a pair of arms, is swung upwards by another air cylinder, and the tie bar is discharged on to the steel plate *W*.

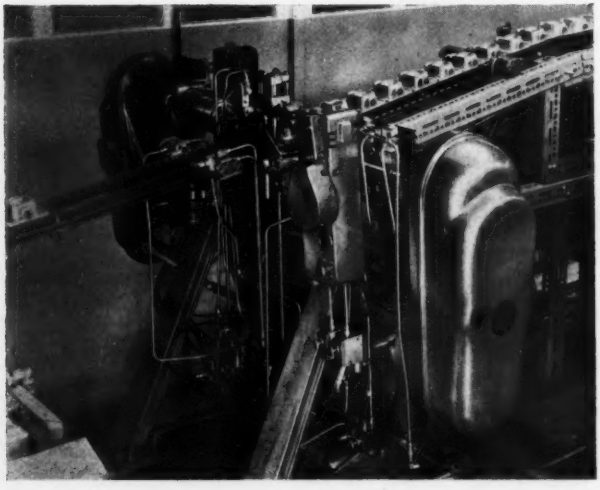


Fig. 6. A 2-spindle fully-automatic machine for tapping cored holes, to receive hose connectors, in pressure die cast heads for Nuquip lubricators

OPERATIONS ON LUBRICATOR HEADS

Heads for lubricators for compressed air lines, made by Nuquip, Ltd., are pressure die cast in brass, and at the first stage in the sequence of machining operations, co-axial cored holes at opposite sides of each component are tapped, to take connecting pieces for hoses, on the 2-spindle machine shown in Fig. 6. This operation is completed in a

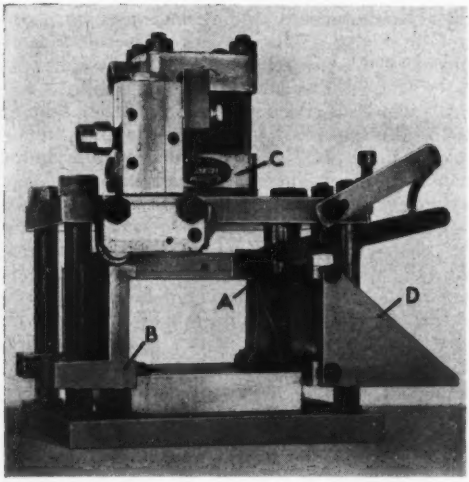


Fig. 7. One of the interchangeable fixtures employed on the machine shown in Fig. 6 for holding lubricator heads while tapping is in progress

cycle time of 25 sec., and the holes are not drilled prior to tapping.

The machine incorporates two Pacera (W. J. Meddings, Ltd.) drilling heads, fitted with Autal [Optical-Mechanical (Instruments), Ltd.] tapping chucks, which are mounted at the ends of a large-diameter horizontal bar carried by two A-shaped castings. Mounted on the bar between the castings there is a platform to take interchangeable work-holding fixtures for two sizes of die castings, in one of which holes are tapped ½ in. B.S.P., and in the other, ¼ in. B.S.P. Inclined chutes at both sides of the machine comprise angle iron side pieces fitted with closely-spaced ball bearings which ensure that the die castings can move easily when they are being loaded into and discharged from the fixture.

Die castings to be tapped are loaded on to the chute at the right-hand side of the machine, which is supported by a framework built up from slotted angle sections, and they are moved by gravity to bring the leading component into contact with a trigger stop incorporated in the fixture. Fig. 7 shows the fixture for tapping the larger die casting, and the trigger stop is indicated at *A*. The die casting is then supported at the sides by shoulders on the inverted channel-shaped member *B*, which can slide on vertical guide bars on the fixture, and is attached to the piston rod of the air cylinder *C*. The air cylinder is now brought into operation, for clamping the die casting between the top plate of the member *B* and another plate mounted on the base of the fixture. At the same time, two of four tie-rod holes cored in the die casting pass over pins in the lower plate, for locating the component for the tapping operation. During the clamping sequence, the die casting is brought clear of the trigger stop *A*, which is then moved sideways by spring action, riding on the top surface of the component, and the triangular

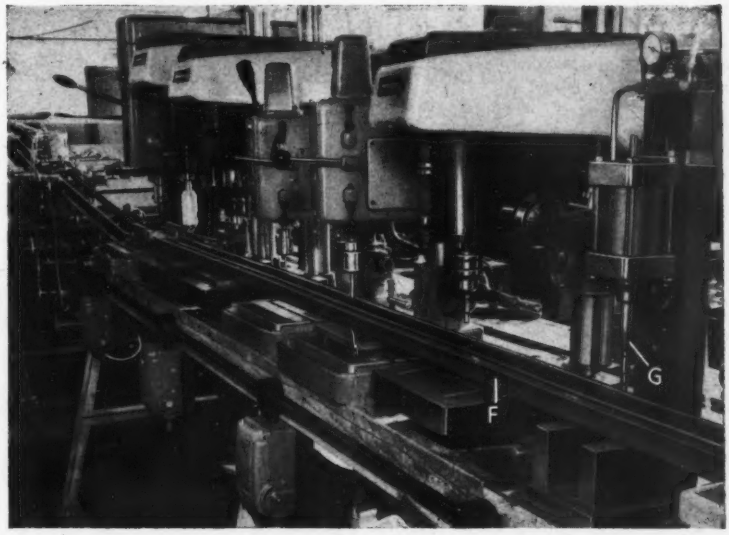


Fig. 8. When the holes for connecting pieces have been tapped, lubricator heads are passed to each of these bench-mounted drilling machines, in turn, by way of cylindrical guide bars in the channel-shaped support member *F*, for other operations

plate *D* operates a roller-type air valve to start the tapping cycle.

The tapping spindles are advanced towards the work by tne action of Martonair feed units mounted on the Pacera heads, one of which may be seen at *E* in Fig. 6. This unit comprises, essentially, a double-acting air cylinder with rack teeth cut in the piston rod, which mesh with a hollow pinion, the latter being mounted on the pinion shaft normally provided on the Pacera head. At the end of the tapping stroke, other roller-type valves are operated by stops on the spindle heads, to reverse the feed units for withdrawing the taps from the work. When the spindles have been brought to the ends of their return strokes, another pair of valves is operated to reverse the clamping cylinder on the fixture for releasing the component.

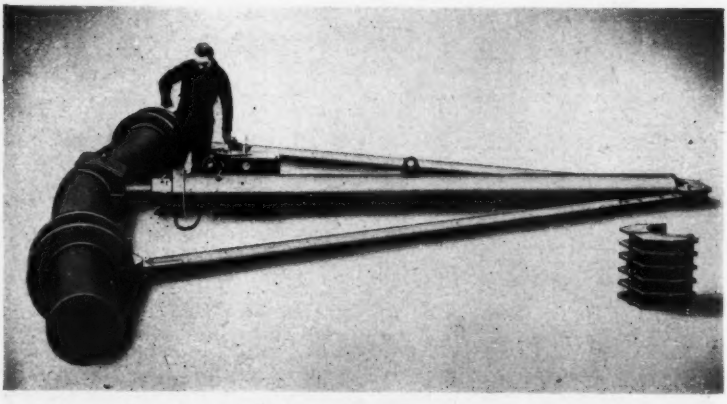
The tapped component now passes down the chute at the left-hand side of the fixture, and is loaded, by hand, into another fixture on the work-table of a bench-mounted, hand-operated machine, which is set up for tapping three cored holes ¼-in. B.S.F. in the top face, to take screws for fixing a cover plate. From this fixture, the component is passed on to a pair of cylindrical guide rails incorporated in a channel-shaped support member, which is mounted on the work-tables of other hand-operated drilling machines, as shown at *F* in Fig. 8. The die casting is subsequently moved from one machine to another by hand, and the operations that are carried out comprise drilling a 0·136-in. diameter hole; drilling, tapping, and spotfacing a 2 B.A. hole; and tapping another hole ⅛ in. B.S.P. The spindles of the drilling machines are staggered so that when the component is brought into contact with cylindrical locating pieces attached to the rear inner face of the channel *F*, the holes to be machined are aligned with the cutting tools. Since drilling and tapping is carried out on cored holes in the die casting, for the 2 B.A. and ⅛-in. B.S.P. sizes, the need for work-holding fixtures is avoided. For drilling the 0·136-in. diameter hole, the conical lower end of an attachment on the drilling spindle engages with a larger-diameter concentric bore in the die casting, to ensure accurate location.

When these operations have been completed, the die casting is brought into line with a tool attached to the piston rod of the air cylinder *G*, which forms a small V-shaped recess in the spot-faced end of the 2 B.A. hole. This hole takes a cheese-headed screw, and when the lubricator is in operation, oil is passed to the compressed air supply between the lower face of the screw head and the V-shaped recess in the seating.

Staffa 18-in. Pipe Bending Machine

Chamberlain Industries, Ltd., Argall Avenue, London, E.10, have recently added to their range the Staffa 18-in. transportable hydraulic pipe bending machine, which is intended primarily for use when pipe-laying is in progress, and has capacity for mild steel pipes up to 18 in. diameter, with wall thickness of ½ in. As an indication of the speed of operation, a pipe of this size can be bent through 10 deg. in less than 10 min.

To facilitate moving the machine from one location to another, it incorporates two arms in place of a forming head of the conventional type. These arms are pivoted at either side of the ram unit, at the rear end, and in operation their outer ends are clamped to the work, as seen in the illustration. A number of alternative pivot holes in the rear end of each arm enables the effective length to be adjusted, for altering the maximum bending radius obtainable. The hydraulic system incorporates a relief valve, to prevent overloading, and is supplied with pressure oil by an air/hydraulic pump.



Staffa 18-in. hydraulic pipe bending machine

The Staveley Group Research Department

By P. A. SIDDERS, Chief Associate Editor

CERTAIN OF THE EXHIBITS of James Archdale & Co., Ltd., and Geo. Richards & Co., Ltd., at the M.T.T.A. International Machine Tool Exhibition last year, incorporated features that had been developed by the Research Department of Staveley Industries, Ltd., of which these two companies are members. The research department was formed towards the end of 1956, at the instigation of Sir Ben Lockspeiser, K.C.B., F.R.S., who had earlier joined the board of the parent company. It was proposed that a centralized department should provide research facilities for the whole group comprising, amongst others, the two firms already mentioned, Cunliffe & Croom, Ltd., Cyril Adams, Ltd., Tilghman's, Ltd., J. H. Shand, Ltd., Bradley & Foster, Ltd., and W. H. Smith & Co. (Electrical Engineers), Ltd. The aim was to provide a closely-knit group for the development of machine tool control systems and automation, with the research department undertaking the basic investigations and development work, the machine tool companies constructing machines based on this work, and the firm of Smith supplying the necessary electronic equipment.

The present premises at Clapham, on the outskirts of Bedford, were taken over in 1957, and were occupied by the research department, under the direction of Dr. E. H. Frost-Smith, in April, 1958. This building was selected because it provided the space required initially, with room for expansion, and because it was conveniently situated between London and the Midlands. Some 10,000 sq. ft. is now occupied by laboratories, workshops and offices, and a new building is to be constructed which will have a floor area of approximately 2,500 sq. ft. This building will house the mechanical engineering laboratory, and will permit the expansion of the other departments within the main building.

Within the research department there are three main sections, concerned with mechanical engineering, control systems, and electronics, and it will be appreciated that the work of the latter two sections overlaps to a certain extent. There is also a design and drawing office, a machine shop and a standards room. Equipment in the latter includes a Hilger & Watts 24-in. line standard, which has been calibrated by the N.P.L., and is within $\pm 0{\cdot}00004$ in. at normal temperature. This standard is used as the fundamental reference by the research department in any work concerned with measurement.

Some 50 people are employed in the department, of whom about half are graduates. Two graduates at a time are recruited from outside and are sent to

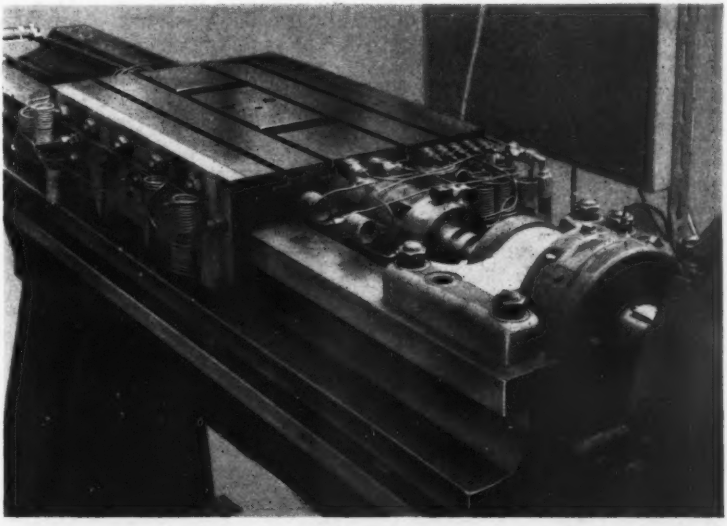


Fig. 1. Test rig for investigations concerned with a hydro-static nut and leadscrew system for traversing a machine tool slide. The screw has a hydrostatic thrust bearing, and is supported radially and laterally within the nut by high-pressure oil

Birmingham University, with all expenses paid by the Staveley Group, where they pursue a 2-year course of studies, under Professor Tobias, formerly of Cambridge University, in order to take their Ph.D. degrees.

The research department maintains contact with other research groups in the machine tool, automation and allied fields. In addition to Birmingham University, it has been in close touch with N.E.L., N.P.L., and the machine tool departments at Manchester University under Dr. Koenigsberger. It is hoped to collaborate with the new Machine Tool Industry Research Association, and it may be mentioned here that Dr. Frost-Smith serves on the committee of that Association.

FEED SYSTEMS OF IMPROVED RIGIDITY

Some examples of the work of the research department will now be considered. Early investigations connected with the numerical control of machine tools indicated that the conventional slide and feed screw arrangements were not satisfactory for precise operation. Hydro-static slideways were therefore investigated whereby the slide is supported on an oil-film of predetermined thickness, the oil being introduced between the slide and its mating slideway at a high pressure. In order to provide axial motion without play, yet without high frictional losses, recourse was had to ball nuts and screws. Two nuts were used with each screw, with a shim between the nuts which could be adjusted to give any desired degree of preloading. This arrangement eliminated play, without unduly reducing the freedom of movement, but preloading introduced other problems, notably deformation of the ball tracks.

It was considered that the hydro-static system that had been employed successfully to slideways could be advantageously applied to feed screws and nuts. An example of such an application is shown in Fig. 1. Series restrictors have been introduced into the system to maintain balanced pressure at the various points in a bearing, under conditions of varying load. Oil is delivered to the slide at a pressure of 20 lb. per sq. in., and to the nut at several hundred lb. per sq. in.

INVESTIGATING THE STIFFNESS OF HYDRO-STATIC SLIDES

Research has been undertaken in connection with the stiffness of hydro-static slides. For this purpose, an Archdale 20-in. horizontal milling machine has been fitted with an auxiliary slide, with a lengthwise projection at each side which is machined to form a hydro-statically supported slideway. Support is provided by oil films between the upper and lower faces of the projections and the guideways in a base, which is secured to the machine table.

For the tests, a workpiece has been mounted on a strain-gauge dynamometer, bolted to the slide, and cutting tests have been carried out by traversing the slide and workpiece. Cutters of various types have been used and both climb and conventional milling have been employed. Variations in the thicknesses of the oil films were checked with the aid of capacitance gauges at either end of the rig, which modulated the frequency of a signal obtained from an oscillator. At the same time, signals obtained from the strain gauge dynamometer were amplified and fed to an oscilloscope to give wave patterns for force and displacement, which were recorded with a ciné-camera.

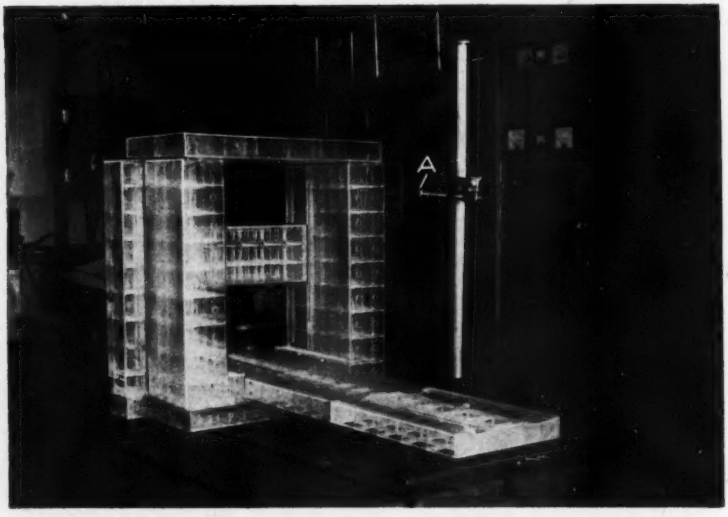


Fig. 2. This Perspex model is being used by the Staveley Group research department to investigate the behaviour of a machine tool structure under load

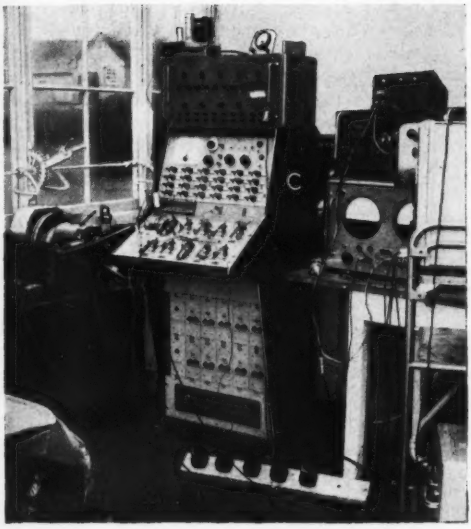


Fig. 3. A set-up for investigating the performance of a hydraulic motor for a machine-tool feed system. Operating conditions are simulated with the aid of the computer *C*

PERSPEX MODELS OF MACHINE STRUCTURES

The research department makes use of Perspex models of machine tools to predict the dynamic behaviour of a design before the actual machine is built. On this basis, the behaviour of an Archdale 20-in. horizontal milling machine has been investigated. The Perspex model of the Archdale machine was made in the workshops at Clapham, and the dynamic performance of the machine itself was checked at the research department. Comparison of the results obtained indicated that it was necessary to carry out investigations on a model of the complete machine, and not with individual elements, in order to obtain a reasonable true prediction of performance. It was found possible, moreover, to determine a relationship between the performances of the model and machine to a useful order of accuracy.

A scale model of a large planing machine is now being constructed at the research department for similar investigations, and is shown in Fig. 2. The model is being investigated by checking the deflection of the various elements under applied vibration. For this purpose, it is coupled to a Goodman's type V.47 vibrator, powered by an amplifier supplied by the same company. A piece of aluminium foil is attached to the element under investigation, by means of grease, and a ferroxcube E-core proximity pick-off unit *A* is applied at a series of positions, to detect deflection of the model. The pick-off unit forms part of a frequency modulated circuit, and is supported by an arm that is attached by a universal clamp to a vertical pillar fitted to an Eclipse permanent magnet base. When necessary, the frequency of the applied vibration can be checked with a Venner counter-timer unit, and the phase of the vibrations is determined with a Muirhead phase meter, against a known reference.

HYDRAULIC MOTORS

Interest in transmission systems and drives for machine tools has led the research department to investigate the possibilities of hydraulic drives for machine tool feed systems. The equipment seen in Fig. 3 is being used to determine the capabilities of a hydraulic motor *B*, for a machine tool servo-drive.

The equipment includes a Solartron Minispace

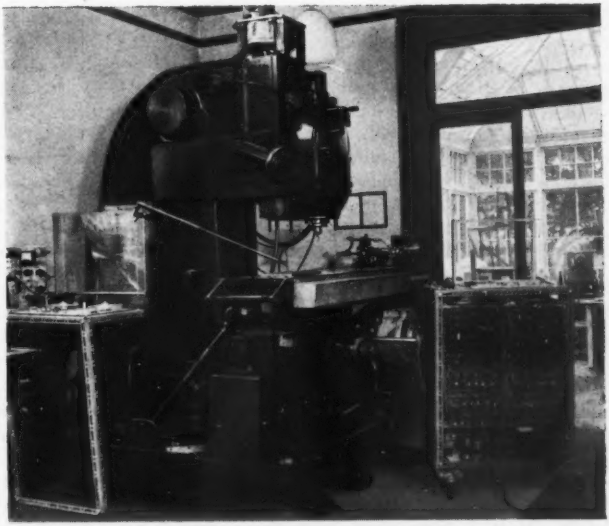


Fig. 4. This Archdale vertical milling machine has been arranged for programme control in three directions by the Staveley Group research department. Different drive systems are used for movements in each direction, so that their merits can be evaluated

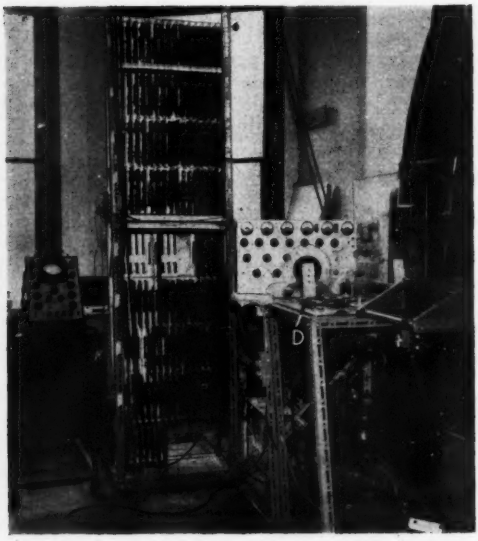


Fig. 5. The research department has built this computer for the production of tapes for the control of the milling machine seen in Fig. 4. Any contour composed of straight lines, circular arcs, or parabolic curves can be machined

computer *C*, which is being used to simulate the dynamic performance of the machine tool. A flywheel is fitted to the output shaft of the motor to simulate inertia mechanically, and drive can be taken from the flywheel to a d.c. generator to provide an electrical load. The motor is fitted with a pressure transducer head, and drives a tacho-generator to give indications of the pressure of the oil and the output speed.

TAPE-CONTROLLED CONTOUR-MILLING MACHINE

An Archdale 34-in. vertical milling machine has been converted for contour milling under tape control and is being used to evaluate different types of servo systems and drives. Control is provided in three directions (*x*, *y* and *z* axes), and motion in any two directions can be controlled simultaneously. A general view of the machine is given in Fig. 4, and the control equipment mounted in the trolley seen at the right incorporates the tape deck. Joy-stick type manual control is provided.

Signals to control the machine are recorded on ¼-in. wide magnetic tape. There are four tracks—one for each axis and one for a reference signal.

Each moving member of the machine is provided with a measuring system of Staveley type. This system has no moving parts and makes use of a reflection grating, with 100 lines per inch. The grating is scanned by four sections of grating, arranged in a "4-phase cursor," and light signals transmitted from the reflection grating through the cursor gratings are detected by four photo-cells, which are switched in and out by signals derived from the reference track of the control tape. The feed-back signal from the measuring system is compared with the signal from the tape, for each axis, by means of a phase comparator. An output signal is generated, the mean d.c. level of which is in proportion to the error of movement along that particular axis, and is used to adjust the position of the associated machine member. If the phase difference between the feed-back signal and the tape signal exceeds ±½ cycle (that is, ±0·005 in.), the machine is stopped.

COMPUTER FOR TAPE PREPARATION

The research department has built a computer for the preparation of tapes, and this equipment is installed at one side of the Archdale milling machine, as seen in Fig. 5. Signals for the machining of any shape composed of straight lines, circular arcs or parabolic curves can be derived from the computer and recorded on tape by means of the tape deck *D*. Information is fed to the computer by means of punched paper tape, prepared on a Friden Flexowriter, from data given on a planning sheet. The punched tape is read by a Creed unit, and the computer converts the information into phase signals that are correct to within 0·0001 in. Of compact design, the computer is fully transistorized, and could be housed in a standard cabinet measuring 6 by 2 by 1 ft.

"IMPROVER" FOR MOLY-VI-BOND MOLYBDENUM DISULPHIDE. K. S. Paul (Molybdenum Disulphide), Ltd., Angel Road, London, N.18, state that the resistance of their Moly-VI-Bond dry-film bonded coating of molybdenum disulphide to abrasion, oxidation, and attack by acids and alkalis, can be further increased by the addition of about 2 per cent of a special composite type resin. The additive also improves the elasticity of the film, and thus facilitates the subsequent processing of parts made from light alloys, tin-plate and steel.

The new "improver" is colourless, non-toxic, and odourless. In use, it is merely mixed with the Moly-VI-Bond, and the resulting compound has a minimum shelf life of four months. There is no change in the method of application of the bonded coating, except that hot curing is essential.

Assembling Domestic Radio Sets

Some Aspects of the Practice and Equipment at Corran Works, Ltd., Larne, Northern Ireland

By A. W. ASTROP, Associate Editor

A FACTORY FOR THE ASSEMBLY of a wide range of domestic radio sets was established at Larne, Northern Ireland, by Corran Works, Ltd. (a member company of the Pye Group) in 1948, and was among the first to be erected in connection with the post-war industrial development programme instituted by the Northern Ireland Government. Reference was made to this programme in an editorial published in MACHINERY, 98/579—15/3/61, and it is sufficient to recall here that one of the main objectives was to diversify the manufacturing activities of Ulster, which previously had depended very largely on the agricultural, textile, shipbuilding and aircraft industries. In seeking to attract new industries, the Northern Ireland Government was primarily concerned with the reduction of unemployment, and, in consequence, was anxious to attract types of manufacture in which labour represented a major factor. In this respect, the radio industry, particularly as regards assembly, has much to offer, and Corran Works, Ltd., began production in a new factory of 30,000 sq. ft., with plans to employ about 250 people.

The factory was erected by the Northern Ireland Ministry of Commerce, and two additional buildings were subsequently provided on the site, to give an additional 20,000 sq. ft. of covered space. With the additional facilities, the number employed had increased to 500 by 1954, and two years later the main building was enlarged by the construction of a 55,000-sq. ft. extension. Employment has continued to rise steadily, and work is now provided for 950 people, of whom approximately 80 per cent are women. At present, still another extension is being built which will provide 50,000 sq. ft. of extra covered space, and will be employed mainly for storage. Space will thus be released in the production area which is currently being used for storage purposes.

Twenty-four different types of sets were in production at the time of our visit, of which 15 are transistorized and 9 of the conventional valve-type. The sets are broadly classified as domestic, pocket, and cabinet models, and of the 24 types being assembled, 17 are specifically intended for export. At peak periods, as many as 34 different types of

Fig. 1. During certain stages of assembly, simple fixtures of the type here shown are used to hold the circuit boards. The fixture can be "rolled" to provide access to both sides and both edges of the board

sets have been in continuous production at one time. In addition to assembly, facilities are provided for the production of a limited range of components, including printed circuit boards, which are used extensively; tuning dials, of a wide range of designs and sizes; and coils. A general view in the main building, showing part of the coil winding section, is given in the heading illustration. The company is also concerned with the production and packaging of complete kits of radio parts, which require only to be assembled. A wide range of these kits is made, and this activity accounts for an important part of the output, particularly in connection with export trade.

The assembly methods employed are generally conventional, with lines of operators seated at benches arranged transversely in the main building. Each operator is responsible for inserting specific components before the chassis is passed down the line, and in this manner it is progressively built up to completion. A simple, but effective, fixture is employed for holding each chassis during certain stages of assembly, and a general view of such a fixture is given in Fig. 1. It will be seen that it incorporates two hoops, made from steel strip, which are welded, one at each end, to a simple fabricated frame. This frame incorporates a pair of thumb-screw type clamps, one of which may be seen at *A*, for securing the chassis in position.

The hoops rest on two parallel lengths of electrical conduit, which extend along the bench and are arranged at such a height that the bottoms of the hoops are held clear of the bench-top by about ¼ in. With this arrangement, the complete fixture can easily be turned about the longitudinal axis to afford access to both sides and both edges of the chassis, yet will remain steady in any position, so that the operator's hands are free for assembly or soldering, for example. Subsequently, the fixture and chassis are slid along the rails to the next operator, who is seated close by. Behind the fixture in Fig. 1 may be seen a simple rack, built-up from welded steel strip, which serves to hold a number of plastics containers for the components to be assembled at this station.

Fig. 2. One of a number of mobile test units which are employed for checking the radio sets at various stages during the course of assembly

Fig. 3. This box-type jig facilitates threading three wires through a thin strip of insulant, to form a small sub-assembly

MOBILE TEST STATIONS

Electrical testing, on a 100 per cent basis, is carried out at numerous stages during the assembly procedure, and the equipment for performing certain tests is of the mobile type. Designed and built by the company, each test station comprises a wood knee-hole type desk, as seen in Fig. 2, at the left-hand end of which there is an extension whereon the main test equipment is mounted. The major item is a multi-frequency generator, which may weigh as much as 1 cwt., and is mounted at an angle so that the controls are readily accessible to the inspector's left hand. A set to be tested, in this instance an almost completely-assembled portable radio, is placed on the desk top, and checked with the aid of the dial-type instrument seen at the rear. This instrument is carried in a simple frame which is mounted on a substantial pillar at one corner of the desk top.

As the desk is mounted on six rubber castors, it can easily be moved to any required position along the assembly lines, or to a maintenance bay. This mobility is of great assistance when the assembly lines are re-arranged to provide for the production of different types of sets, and the test stations are required to be located in fresh positions. Moreover, if fewer test stations are required for a given set than for the type that was previously being assembled, the redundant units can be wheeled away to a store, where they are less likely to be accidentally damaged.

MECHANICAL AID FOR PRODUCING A SMALL SUB-ASSEMBLY

A small sub-assembly, which is required in very large numbers, comprises a group of three wires threaded through a rectangular strip of transparent insulating material, as seen in the foreground in Fig. 3. These small assemblies, are produced very rapidly and easily with the aid of the simple box-type fixture. Projecting from a steel plate at the front of the box there are three small-bore tubes, the ends of which are machined at an angle of approximately 30 deg. Wires from three coils supported on a stand at the rear of the bench are passed through holes in the rear wall of the box, and thence through the tubes, so that a short length projects from each.

The strips of insulating material are pre-punched with three rows of three equally-spaced holes, and a stack of strips is loaded on to the projecting tubes, which pass through the uppermost holes. Initially, the projecting ends of the three wires are bent upwards, and over, away from the operator, so that three backward-facing hooks are formed. The operator now grips the lower end of the first insulating strip in the stack, and by curling it upwards, and away from her, threads the centre group of holes over the three tubes. Next, she pulls the end of the strip downwards, and forwards, so that the last group of holes engages with the hooked ends of the wires.

She then pulls the strip towards her, so that it slides off the tubes, and continues this movement until there is a free length of wire of about 4 in. extending beyond the trailing end of the insulating strip. The next operation is to swing the strip upwards, and backwards, to bend the wires at the points where they leave the tubes. Finally, the three wires are severed with scissors in such a way as to leave three backward facing ends, or hooks, in readiness for the next strip to be brought forward and threaded in a similar manner. This simple fixture ensures that the wires of each assembly are cut to the same length, and greatly facilitates the threading operation, which, on account of the thinness and lightness of the insulating material, would otherwise be a difficult and tedious procedure. Each sub-assembly is threaded and cut-off in about 4 sec.

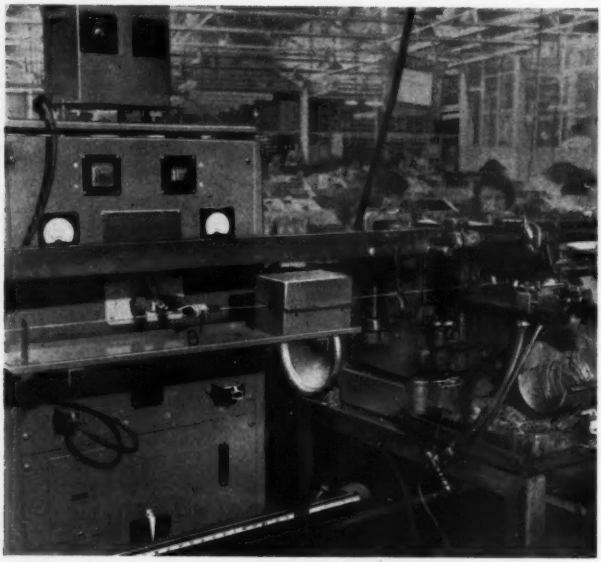


Fig. 4. This Radyne induction heating set is used in conjunction with the Artos wire cutting and stripping machine at the right, and obviates frayed wire-ends at the stripping stage

MODIFIED WIRE-STRIPPING MACHINE

Extensive use is made of wires which are pre-cut to specified lengths and stripped of insulation over a short length at each end. Automatic wire-cutting and stripping machines are employed, one of which can be seen at the right in Fig. 4. This machine was built by the Artos Engineering Co., Milwaukee, U.S.A. (Gaston E. Marbaix, Ltd.). Certain difficulties were experienced in connection with the stripping stage of the machine cycle, in that, although the insulation was removed cleanly, the wire strands were sometimes disturbed, and the ends were then slightly frayed. Wires with frayed ends, in turn, caused difficulties during assembly and soldering.

To overcome this trouble, the company operate the machine in conjunction with a Radyne induction heating unit, which was developed specifically for use in association with the Artos machine. This unit is seen at the extreme left in Fig. 4, and the heating coil is indicated at *B*. Wire is drawn from a reel to the left of the Radyne unit—and not shown in the figure—and the leading end is passed through the induction coil *B*, and thence to the Artos machine. The heating unit is switched on and off by limit switches, which have been fitted to the Artos machine, in synchronism with the operation of the latter, and with this arrangement the coil *B* is alternately energized and de-energized.

It is energized when the wire is momentarily stationary—during the stripping and cutting-off stages on the Artos machine—and the heat applied is just sufficient to "wet" the tinning on the wires without affecting the plastics insulation surrounding them. As a fresh length of wire is pulled through by the Artos machine, a limit switch is tripped to cut-off the heating current, which is restored only when the wire feed movement has been completed. It will be appreciated that with this arrangement there are short lengths of wire, at regularly spaced intervals, on which the tinning has been wetted sufficiently to bond the various strands together. Moreover, the strands are bonded at the points where the wire is to be cut and stripped, with the result that they are not disturbed or frayed by these operations.

The Radyne unit is mounted on steel rails, arranged parallel with the run of the wire, on which it can be adjusted to the required position relative to the Artos machine, according to the length of wire to be cut. This adjustment is carried out with reference to the scale and pointer seen in the left foreground of the illustration.

FLOW-SOLDERING FACILITIES

Flow-soldering of printed circuit boards is carried out with the aid of a continuous machine supplied by Fry's Metal Foundries, Ltd., and a close-up view of the working area of this equipment is given in Fig. 5. The molten solder is forced continuously over a weir, as at *C*, by means of a motor-driven impeller, and the circuit boards are held in simple jigs and are traversed over the weir by slowly-moving endless chains. These chains are housed within the channel-sections at *D*, and the links are engaged by pegs which project from the under-sides of the jigs.

The jigs are so designed that they are readily adjustable to accommodate a range of circuit boards of different widths, and the latter can be loaded and unloaded quickly without the need for manipulating screw clamps or clips. Of welded steel construction, each jig incorporates a pair of strips at each end, arranged transversely and with

a gap between them, one pair being indicated at *E*. The gap between each pair of strips serves to accommodate a bolt whereby the strip *F* is secured, and this strip is positioned and clamped to suit the width of the circuit board which is being handled.

Secured to the strip *F*, and projecting downwards, are two ½-in. diameter pillars, and close to the lower end of each pillar there is a V-shaped annular groove, of a width to suit the thickness of the circuit board. Another strip, *G*, is of similar design to the strip *F*, and has two identical pillars with annular grooves at the lower ends. The strip *G*, however, is arranged to slide on the members *E*, and is connected to the strip *F* by a tension spring at each end. To load a circuit board, it is necessary only to pull the strip *G* towards the front of the machine, against the tension springs, with the left hand. The circuit board is then loaded from the top, and the rear edge is engaged with the grooves in the pillars on the strip *F*. Next, the strip *G* is released slowly, whereupon the grooves in the pillars on this member engage the front edge of the circuit board, and the latter is gripped under spring pressure.

The strip *G* is prevented from rising or tilting, under the pull of the springs, by screws and washers which engage with the under-sides of the strips *E*. When the jig has passed over the solder bath, the strip *G* is pulled towards the operator once more, to release the circuit board which can then be lifted out. It may be mentioned that for purposes of illustration a sheet of white paper was inserted beneath each jig seen in Fig. 5, in order to show the construction in more detail.

In a second article on Corran Works, Ltd., to be published shortly, reference will be made to a stores system whereby control is maintained over more than 4,500 different types of bought-out components used in the company's radio sets.

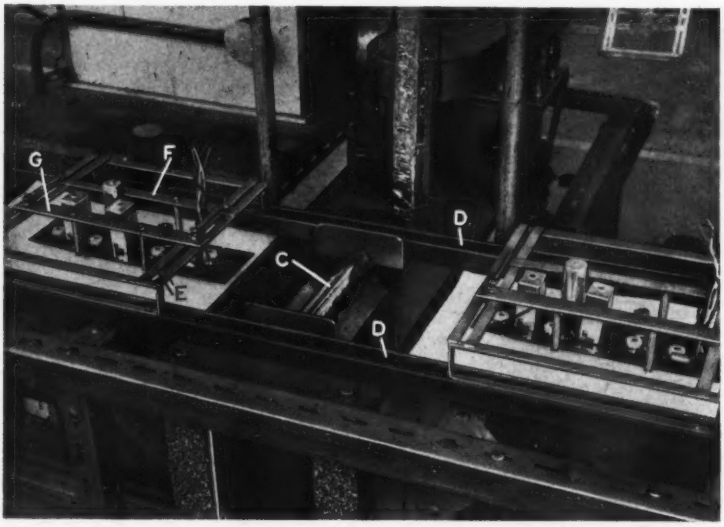


Fig. 5. The jigs used in conjunction with this Fry's continuous flow-soldering machine will accommodate a wide range of circuit boards, and provide for rapid loading and unloading

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CALOR P4 FLAME CUTTER. An oxy-propane flame cutter, known as the Calor P4, for which some important advantages are claimed, has been introduced by Calor-Midgley, Ltd., the Sheffield subsidiary of Calor Gas (Distributing) Co., Ltd., Poland House, 116 Oxford Street, London, W.1. This cutter, developed by Mr. A. Foster, a technical representative of the company, is said to be capable of cutting steel up to 5 ft. thick, using a straight mixture of Calor propane and oxygen.

A slab of 42-in. thick carbon steel, cut at the rate of 10 ft. per hr., was among the company's exhibits at the recent Engineering, Marine, Welding and Nuclear Energy Exhibition. The cutter has also been used to advantage for "parting" the tops and bottoms of very large, hollow ingots, between 55 and 58 in. diameter. Previously, parting by machining, involving annealing and cooling, occupied as much as 240 hours, whereas with the P4 cutter, the time required is only 80 min., and there is a substantial saving in fuel costs. It is stated that the success of the P4 cutter depends on the fact that the propane gas and oxygen are mixed in the cutting nozzle, and not in the barrel. Low oxygen pressures—25 lb. per sq. in. for heating, and 30 lb. per sq. in. for cutting—are also of importance, since at these pressures greater effective depth of penetration is achieved.

Machine Tool Industry Research Association

A REVIEW OF THE PROGRESS that has been made in the establishment of the Machine Tool Industry Research Association has recently been published*. The director, Mr. A. E. De Barr, B.Sc., F.Inst.P., took up his duties on April 1, and the Council has appointed Mr. J. A. Mozley as secretary. Mr. Mozley has had experience of research association work, and took up his appointment on June 5.

Pending the finding of suitable office accommodation in the South Manchester district, temporary offices have been rented in the centre of Manchester. The headquarters of the Association were transferred to the latter premises on June 5, and, until further notice, all correspondence should be addressed to:—The Director of Research, The Machine Tool Industry Research Association, 28 Deansgate, Manchester, 3 (telephone Blackfriars 3851, extension 110).

The chairman of the Association, Mr. J. C. Snow, and the director have visited the National Physical Laboratory, Teddington, to discuss the work of the laboratory in relation to machine tool problems. The director has also visited the following establishments to discuss machine tool research in progress:—National Engineering Laboratory, East Kilbride; Department of Mechanical Engineering, Manchester College of Science and Technology; Department of Mechanical Engineering, Birmingham University; Production Engineering Research Association, Melton Mowbray; and College of Aeronautics, Cranfield. He has also visited the factories and laboratories of several member firms to discuss their work and problems.

Earlier this year, application was made to the Department of Scientific and Industrial Research for a grant-in-aid. The terms of the grant subsequently offered are particularly generous, and the chairman has expressed the hope that the industry will respond wholeheartedly to the offer and show faith in itself and its future by enabling the Association to qualify for the maximum amount. The grant is for a period of five years, starting January 1, 1961, and follows the established pattern of D.S.I.R. grants, which require re-application to be made every fifth year. Briefly, the terms provide that if the Association in the first three years of the 5-year period raises an annual income (approved as grant-earning) of £40,000, then D.S.I.R. will make an annual block grant of £40,000. For each complete £100 by which the grant-earning income exceeds £40,000, D.S.I.R. will make an additional grant of £80, up to a maximum additional grant of £28,000 per year. For each of the last two years of the 5-year period, provided that the Association raises an annual grant-earning income of £80,000, D.S.I.R. will make an annual block grant of £60,000, and for every complete £100 of additional income, an additional grant of £80 will be made, up to a maximum additional grant of £20,000 per year. As examples of the income that the Association could derive, it may be mentioned that, in the years 1961-63, if members' subscriptions (that is the grant-earning income) amount to £40,000, the total income will be £80,000; if subscriptions are £75,000, total income will be £143,000. For the years 1964 and 1965, subscriptions of £80,000 will result in a total income of £140,000; and subscriptions of £110,000, a total income of £190,000. If the machine tool industry responds fully to the offer, D.S.I.R. will pay almost 50 per cent of the cost of research carried out by the M.T.I.R.A. (as compared with an average of about 30 per cent for other industrial research associations).

An outline research programme was included in the Association's application for the grant, and it is envisaged that work will be carried out under the following main classifications:—performance of machine tools; design features; small tools and accessories; measuring techniques and methods of control; production processes and new methods; field studies and productivity studies. It is planned to provide a technical information service to meet the needs of the machine tool industry, and a technical advisory service to assist members, particularly in the application of the results of research and development work.

* M.T.I.R.A. News Letter, No. 1, May, 1961, available to nominated representatives of member firms.

A DUSTLESS DRILLING HAMMER, for use on concrete, rock, stone, or brick, has been introduced by Thor Tools, Ltd., Tynemouth, Northumberland. This hammer is pneumatically operated, and is so designed that a high velocity reverse-flow of air draws chips and dust through the drill-bit and rod and delivers them into filter tanks. Both the bore and the surrounding atmosphere are thus kept clear of dust, and it is claimed that the tool offers particular advantages for drilling inside buildings.

NEWS OF THE INDUSTRY

Tyneside

NOBLE & LUND, LTD., Felling-on-Tyne, report an increasing call for all the machine tools in their range, and particularly for special purpose and cold sawing machines, many of which are to be supplied with automatic feeding arrangements. Machines which have recently been ordered include a number of 6-in. spindle horizontal borers; a 63-in. centre lathe; a 30-in. centre lathe; a 60-in. high-speed cold sawing machine for export to Germany; and a 68-in. centre lathe for Brazil.

We are informed that the recently introduced Millahead planer/miller conversion unit and the horizontal Millahead machine, which we hope to describe fully in a future issue, have been well received.

A large amount of development work is at present being carried out, and we noted that the prototypes of an automatic measuring device and a new 4-ft. capacity plano-milling machine are at present in hand. We hope to publish full details of these developments at a later date.

Machines seen in progress in the works included a large number of vertical and horizontal type hydraulically operated, cold sawing machines of various sizes; a 30-in. centre lathe which is to be equipped with electronic tracing equipment for copy turning; a column and base type horizontal Millahead machine, with a horizontal traverse of 17 ft. and a vertical traverse of 8 ft.; and a 60-in. table-type cold sawing machine for cutting aluminium slabs. The table of the latter machine is of the power-driven roller type, and two cutting speeds of 1,500 and 3,000 ft. per min. are available.

Among the machines recently despatched from the works may be mentioned a lathe with a centre height of 20 in. and a capacity of 32 ft. between centres, for which the main drive is provided by a 75-h.p. motor, and a 38-in. horizontal table type, Fluifeed cold sawing machine which was specially designed for cutting slabs of 99·1 per cent pure aluminium. We are informed that test pieces were cut on this machine at a rate of 420 sq. in. per min.

Other activities of the company include gear cutting, gear grinding, and spline hobbing and grinding for the trade. The foundry is maintaining an output of approximately 40 tons of castings per week, some of which are for outside customers. There is provision for handling castings with individual weights up to 20 tons.

CLARKE, CHAPMAN & CO., LTD., Gateshead-on-Tyne, report that the works are busy on a variety of products. A lively demand is being experienced for their range of single-direction turbines for driving tank-purging fans on board tankers, and orders are in hand from both the home and export markets for reversing steam turbines for marine applications. There is considerable activity in ships' deck machinery, including electric, steam, and hydraulic winches, capstans, and windlasses, and it may be noted that an order has recently been received for trawl winches for installation on four factory trawlers for Russia, which are being built on the Continent.

BUMA ENGINEERING CO., LTD., Robson Street, Newcastle-on-Tyne, inform us that a steady flow of orders is being received for their Cent-Ro-Mac portable fine boring machine from the shipbuilding and heavy engineering industries, and that production in the fabrication and the contract machining departments is being well maintained.

This company also builds prototype machinery and special purpose machines and equipment, which can be designed to suit customers' requirements, or made to drawings and specifications supplied. The services of the shot-blasting and metal spraying department are in good demand from various branches of industry, and we are informed that a number of mobile shot-blasting and metal spraying units has been formed to enable work to be carried out on site.

New machine tools recently installed in the shops have included a Jones-Shipman type 1400 surface grinder, a Newall jig boring machine, and a Berthiez planing machine of 3 ft. square by 13 ft. capacity.

LUMSDEN MACHINE CO., LTD., Hawks Road, Gateshead-on-Tyne, report that a satisfactory volume of orders is in hand for the various machine tools in their range, and that an increasing number

of enquiries is being received from both the home and export markets. Orders on the books indicate a steady call for standard types and a substantial increase in the demand for special-purpose and large-capacity machines. Among those recently ordered may be noted three 100-in. vertical spindle, rotary-table, grinding machines; a number of continuous grinders for the motor vehicle industry, of the rotary table type, and fitted with single, twin, or multiple grinding heads for completing components at one pass; a 16-ft. reciprocating table type grinder for a customer in Belfast; a number of rotary, retracting table type machines; a reciprocating table grinder for France; three rotary, retracting table type, die grinders for India; a 60-in. machine equipped with a rotary table mounted on a traversing table, and a grinding head carried on a cross-rail, which has been modified to swing 84 in. diameter, and is to be used for rotary, reciprocating, and internal grinding; and a reciprocating machine for France with a 20-ft. long by 4-ft. wide table, and a work height capacity of 3 ft.

To enable the works to keep pace with the increasing demand and to assist in overcoming the shortage of skilled labour, a certain amount of plant replacement is being carried out. Machines and equipment recently installed have included a Herbert Pre-optive turret lathe, and sand blasting plant, and a large Richards boring machine is on order for delivery in the near future.

LERCHE MACHINE TOOLS, LTD., Oakwellgate, Gateshead-on-Tyne, who are sole distributors of a wide variety of British and Continental machine tools and equipment, inform us that the demand from all branches of the engineering industry is maintained at a high level.

Machines and equipment displayed in the showrooms include capstan and centre lathes, tool grinders, welding plant and machine vices. We are informed that the company have recently been appointed Northern Area agents for Melbro electro-magnetic clamping type portable drill posts, which are available in a range of three sizes, up to 2¼-in. diameter drilling capacity.

CHURCHILL GEAR MACHINES, LTD., Blaydon, Co. Durham, report a continued growth in the demand for their machine tools and equipment.

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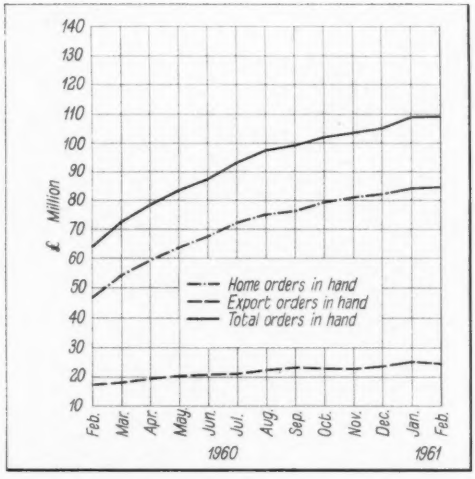
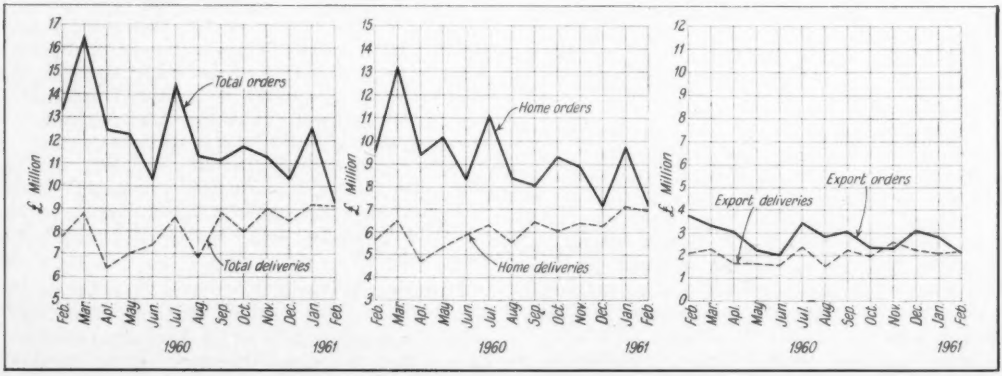

£ Million
Home orders in hand
Export orders in hand
Total orders in hand
Feb. Mar. Apr. May Jun. Jul. Aug. Sep. Oct. Nov. Dec. Jan. Feb.
1960
1961

❖ ❖ ❖

The accompanying graphs show the values of machine tool orders and deliveries during the past twelve months also the values of orders in hand



Orders are in hand at present for gear hobbing, shaving, hard honing, chamfering and rounding, forming (rolling), washing, and checking machines, also for gear sound testers, and Conomatic automatics, the latter being built under contract for The Cone Automatic Machine Co., Ltd.

It was noted that a large amount of automatic loading and transfer equipment is at present on order for use with the company's machines, and we are informed that the demand for this type of equipment is increasing. Orders recently received have included one for the supply of 37 automatic gear hobbing machines and 14 automatic gear shaving machines, to an automatic gearbox manufacturer.

All types of machines were in progress in shops including a battery of the recently introduced hard gear honing machines. Production in the cutter department is being maintained at a high level, and customers are making increasing use of the cutter re-grinding service operated by the company. Products to be shown at the forthcoming Brussels exhibition will include a fully automatic Mk.4. production gear hobber, a shaving machine, and a gear honing machine.

New plant which has been installed in the works since our last visit includes a Scharmann type F.B.125.C. horizontal boring and milling machine, a Futurmill planer/miller conversion unit, and a Delapena honing machine.

R. SUTCLIFFE.

The South

STARTRITE ENGINEERING CO., LTD., Gillingham, Kent, are still very busy with the production of machines for bandsawing, bandfiling, drilling, and abrasive band polishing operations. To enable output of such machines to be increased, the shops have again been extended.

HYTHE ENGINEERING CO., LTD., Hythe, Kent, are well occupied with a variety of products including structural steelwork, metal balustrades and stairways, pressure vessels, and pile driving equipment. Several dosage units, for use in connection with water purification, have recently been completed for export. The existing premises are too small for the company's anticipated future requirements, and to provide improved facilities, a new factory is to be built on a neighbouring site. Initially, a number of bays with a combined area of 3,600 sq. ft. will be erected and a 10-ton overhead travelling crane installed. Eventually it is hoped to quadruple the area in several stages.

INDUSTRIAL TECHNICS (SOUTHAMPTON), LTD., Empress Road, Southampton, who, as already announced, are now a subsidiary of Dowding & Doll, Ltd., London, W.14, are building machine tools and injection moulding machines and producing a variety of parts under sub-contract. Atlantic co-ordinate tables are in production, equipped with positioning control equipment. One such table was incorporated in a closed frame boring machine built by the company for installation in the works of William Asquith, Ltd. Weighing more than 13 tons, this machine has a base with overall dimensions of 12 ft. 9 in. by 8 ft. 6 in. The Atlantic table is so arranged that the directions of traverse are at 45 deg. to the bridge, and in this way it has been possible to provide for a greater range of table movements for a given column spacing than could normally be obtained.

At present the shops cover an area of approximately 16,000 sq. ft. and are working at full capacity. Recent additions to the plant include a Richards No. 2 boring machine and a Ward No. 7 Prelector turret lathe. Delivery of a Butler 4A planing machine of 10 ft. stroke is expected shortly.

MURAD DEVELOPMENTS, LTD., Whiteway, Queenborough, Isle of Sheppey, Kent, formerly at Stocklake, Aylesbury, Bucks., are experiencing a satisfactory demand for capstan lathes and the EG 8 pedestal-type off-hand grinding machine, which is provided with wheel hoods of special design that are stated to be effective in preventing the spread of dust produced during grinding. The Bormilathe, introduced to meet the demand for a machine which can be employed for boring, milling, and turning operations, has proved of interest both to industrial and experimental establishments, and one of the latter has placed repeat orders as a result of the advantages gained from the machine originally installed. Quantity production of the Bormilathe will begin as soon as the arrangements for providing the necessary machining facilities have been completed.

F. W. HERRIDGE.

Advice for the Small Firm

Sources of advice for the smaller firm was the subject of a recent 1-day conference held by the Central London Productivity Association, which is affiliated to the British Productivity Council, 21 Tothill Street, London, S.W.1.

Presented by Mr. A. Thorogood, of the Department of Scientific and Industrial Research, the first paper was entitled "D.S.I.R. Technical Services for the Smaller Firm," and drew attention to the activities of the 51 grant-aided industrial research organizations from which advice was readily available. With the aid of coloured slides, the speaker gave details of various advisory services, and he

explained that, in certain instances, D.S.I.R. might be able to put small firms in touch with field officers who would assist them in solving their problems. Quick advice on technical matters could be obtained by telephoning the D.S.I.R. technical information division (telephone No. Hunter 1212, extension 727).

Dr. Margaret Wray, of the Federation of British Industries, spoke on the economic data that were available in various statistical publications, and she explained how F.B.I. economic surveys were conducted. Typical experiences of an advisory organization were described by Mr. F. M. Algar, of the Rural Industries Bureau.

Mr. D. W. W. Roberts, of the National Provincial Bank, dealt with the various courses which could be adopted by firms wishing to export their products for the first time. He pointed out that firms could freely consult the Export Services Branch of the Board of Trade for general guidance and for more detailed advice. Moreover, advice could be obtained from the overseas department of a firm's own bank. Mr. Roberts explained in some detail the many methods of payment which could be used, and he emphasized the advisability of taking out credit insurance.

Finally, Mr. J. B. Darner, of the National Union of Manufacturers, gave details of his organization, and he drew attention to the facilities afforded by the Union's Industrial Advisory Service at Thames Chambers, 12 York Buildings, Adelphi, London, W.C.2. This body offers specialist consultant service in a wide range of management problems, and this service is not confined to member firms, although membership of the N.U.M. affords concessions in respect of fees.

Applications of Electrostatic Forces

(*Continued from page* 1275)

fluid which ensures that no air is present between the contact faces.

Electrostatic charges of opposite polarity are then generated on the contact surfaces of the chuck and the workpieces, to produce the required holding force, by means of a compact power unit. Any electrically conducting material can be held, including, for example, brass, aluminium alloys, and non-magnetic stainless steels. It is also possible to grip parts made from ceramics or plastics if the contact surfaces are previously coated with a thin metal film.

It will be evident, therefore, that electrostatic forces can be usefully applied in a variety of ways, and as further experience is gained in this field it is probable that these forces will be utilized for the solution of other problems.

Industrial Notes

JOHNSON, MATTHEY & CO., LTD., 73-83 Hatton Garden, London, E.C.1, can now supply zone-refined germanium, normally in ingots of 1 kg. nominal weight. A large scrap-recovery plant has been installed, and the company now wishes to purchase large or small quantities of germanium scrap.

E.M.I. ELECTRONICS, LTD., Hayes, Middlesex, inform us that they have received an order from Société Genevoise d'Instruments de Physique, Geneva, for six E.M.I. rotary control systems to be applied to Rotoptic rotary positioning tables. It is stated that this order, which is valued at approximately £20,000, has been placed following extensive tests with prototype equipment.

RESETTLEMENT OF THE DISABLED IN A CHANGING SOCIETY will be the subject of a 3-day course and conference to be held at The University of Liverpool on July 18 to 20. The event is being organized by the British Council for Rehabilitation of the Disabled, Tavistock House (South), Tavistock Square, London, W.C.1, from whom full particulars can be obtained.

RENOLD CHAINS CONTINENTAL, LTD.—The Belgian branch of this organization has moved to new premises at 1 Allee Verte, Brussels. The building, which comprises three floors and a sub-basement, provides an area of more than 20,000 sq. ft. Large stocks of chains and wheels and power transmission accessories are carried, and there are facilities for the production of special wheels.

MOON BROTHERS, LTD., Beaufort Road, Birkenhead, Cheshire, have introduced the CD hand-operated machine for cutting off the tops of steel drums of almost any size. Gauging rollers hold the machine in position, and the cut is made just below the end seam. Hardened steel cutters are employed and drive is transmitted through reduction gearing. A clean cut is obtained, and the edge can subsequently be curled or flanged, if required.

THE BRITISH OXYGEN CO., LTD., Spencer House, St. James's Place, London, S.W.1, have issued the first number of a house journal entitled *Arc* which replaces Quasi-Arc *Welding News*. This change has been made as a result of the arrangement whereby the sales activities of Quasi-Arc, Ltd., are being carried on in the name of the Electric Welding Department of British Oxygen. Under the new title, the style and presentation of the journal have been revised, and the scope has been broadened to embrace Argonarc welding and allied processes. This first number, which is very well presented, includes, for example, articles on Argonarc and its applications, low cost lightweight welding sets, a high-lift boom for streamlined production, flux materials, and hard facts on hard facing.

ELECTRO-CHEMICAL ENGINEERING CO., LTD., Sheerwater, Woking, Surrey, recently opened a new depot at Moor Lane, Witton, Birmingham, 6, which has been provided at a cost of £50,000. This depot has been built on a site of 2 acres which provides space for future expansion, and in addition to offices and stores, a laboratory will shortly be in operation to provide services for testing and

analysis. The main stores are housed in a building with dimensions of 115 ft. by 47 ft., and effective utilization of space has been ensured by the provision of interchangeable steel racks, fork-lift trucks, and self-propelled hoists. In addition to Efco-Udylite plating plant and processes, the company can supply automatic degreasing and metal cleaning equipment by arrangement with Technochemie A.G., Zurich, and Solventol Chemical Products Inc., Detroit, also automatic polishing machinery with the co-operation of Acme Manufacturing Co., Detroit.

ORDERS AND OUTPUT IN THE ENGINEERING INDUSTRIES.—The volume of net orders received in March by the industries producing engineering and electrical goods (Order VI of the Standard Industrial Classification), locomotives and railway track equipment, railway carriages and wagons, heavy commercial vehicles, and wheeled tractors, was 17 per cent more than in March, 1960, and for the first quarter of the year, the increase was 6 per cent. Export orders rose in March, but for the quarter they were 3 per cent less than in the corresponding period of 1960. On the other hand, home market demand for plant and machinery in particular has shown a marked expansion in the early months of this year.

It is estimated that the volume of output in the engineering and electrical goods industries in March was 2 per cent higher than in March, 1960, and that for the quarter the rise was 3 per cent. Exports of goods (volume) made by these industries in the first quarter were 15 per cent more than in the corresponding period of 1960.

New Appointments

The following new appointments have been announced:—

MR. ERIC TURNER as chairman of the Birmingham Small Arms Co., Ltd., in succession to MR. JOHN Y. SANGSTER who continues to be a director.

MR. S. H. IRELAND as assistant managing director, MR. L. S. BRIGHT as financial director, and MR. A. O. MILLER as director of Consolidated Pneumatic Tool Co., Ltd., 232 Dawes Road, London, S.W.6.

MR. J. J. MCCORMICK and MR. F. W. WESTCOMBE, joint sales managers, and MR. IAN A. F. CRAIG, overseas manager, as local directors of The British Wagon Co., Ltd., 13 Grosvenor Crescent, London, S.W.1.

MR. S. G. DEAVES, a director of B.T.R. Industries, Ltd., as chairman for 1961-62 of the British Moulded Rubber Hose Manufacturers' Association, 19-20 Berners Street, London, W.1.

MR. T. H. GALLIE (overseas) and MR. J. R. H. CRANE (copper products), as directors of the Metals Division of Imperial Chemical Industries, Ltd., Millbank, London, S.W.1.

MR. F. B. G. SAMMONS, A.M.I.Prod.E., as sales manager, MR. G. SEARLE, as technical sales representative for Yorkshire and the North Eastern counties, and MR. J. BRADY as technical sales representative for Lancashire, Cheshire, and the North Western counties, of the Moore Manufacturing Co., Ltd., Blanche Street, Laisterdyke, Bradford.

MACHINERY'S ENQUIRY BUREAU

For many years MACHINERY has provided an enquiry service not only for subscribers and advertisers but for all engineers in need of such information as the names of makers—or their agents—of machines or equipment for performing particular operations, suppliers of various classes of material, firms with facilities for undertaking certain types of work, owners of trade names, and agents for foreign machine builders. If you have such a problem write (MACHINERY, Enquiry Bureau, Clifton House, 83-117 Euston Road, London, N.W.1) or telephone (Euston 8441, 2 lines). This service is, of course, entirely free.

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Wakefield Memorial Lecture

The third Wakefield Memorial Lecture was recently delivered to a meeting of the College of Aeronautical and Automobile Engineering, Kings Road, Chelsea, London, S.W.3, by Mr. Alick Dick, managing director, Standard-Triumph International, Ltd.

Speaking on the subject of education, Mr. Dick pointed out that, although the country wanted large numbers of highly-trained technicians, there was also a demand for skilled administrators with a sound knowledge of the purpose and economics of industry, of finance, and of human relations. It was necessary to teach these basic principles of management rather than to expect people to acquire them, but, at present, there was no specific degree course covering management studies, in any university in the U.K. In the United States, however, the majority of universities had faculties specializing in business studies and management.

In Great Britain, the intake of staff into industry was largely confined to technically-trained people, but it was Mr. Dick's view that more students of the arts should be selected to strengthen the commercial side of business. The training which was received by arts students, he considered, was ideal for potential management staff. Such students learned to work out problems for themselves and to draw the appropriate conclusions, and this training was invaluable in making decisions in any field.

Trade Publications

CHAPHONE ENGINEERING DEVELOPMENTS, LTD., Sutton Coldfield, Warwickshire. Illustrated brochure describing the company's type CV2 and CV3 multi-purpose vertical hydraulic honing machines. Attention is drawn to the various features of the design, and specifications are included. In addition, particulars are given of Chaphone rigid hydraulic honing units.

MISAL S.a.S. LETO, Via Vittor Pisani, 14, Milan, 508, Italy. Catalogue covering the company's manufacturing programme for 1961 which comprises numerous centre lathes; turret lathes; universal and vertical milling machines; shapers; surface, universal, and tool cutter grinders; slotters ; hacksawing machines ; and radial drills. The various machines are illustrated and specifications are included.

ASSOCIATED ELECTRICAL INDUSTRIES, LTD., Electronic Apparatus Division, New Parks, Leicester. Publication 4103-1 describes the Numeritrol system for continuous numerical control of machine tools in two or three dimensions, from ¼-in. wide magnetic tape. Sections are devoted to basic principles; features of the system; the planning sheet; equipment associated with the machine tool; and tape service.

W. & T. AVERY, LTD., Soho Foundry, Birmingham, 40, have introduced a new publication entitled "Survey." In the first issue, which is noteworthy for the high standard of presentation and illustration, there are articles concerned with various applications of the company's weighing equipment at the works of Petters, Ltd., Fairey Aviation, Enfield Rolling Mills, Ltd., Victoria Flour Co., Ltd., and Hamilton Brush Co. (London), Ltd.

JOSEPH RHODES & SONS, LTD., Wakefield. Catalogue describing in detail, with numerous illustrations, the company's range of patented fluid drive shears which covers capacities from 14-gauge by 6 ft. to 1 in. by 16 ft. Sections are devoted, for example, to maintenance, controls, productivity, 2-speed drive, precision, hold-down, gauging equipment, blades, and bevel edge cutting. Another publication is concerned with the Rhodes stagger-feed press for producing stampings from sheets at speeds up to 180 strokes per min. It is stated that the average time required for changing over to a stamping of a different size is 35 min.

Scrap Metals

†LONDON.—‡Prices per ton for non-ferrous scrap metals free from iron are as follows:—Clean copper wire, untinned and free from lead and solder, £210; clean heavy copper, untinned and free from lead and solder, £205; copper wire No. 2, £201; clean light copper, £197; braziery copper, £176; gunmetal, £184; brass, mixed, £136; lead, net, £52; zinc, £43; cast aluminium, £93; old rolled aluminium, £96; battery lead, £27; unsweated brass radiators, £110; hollow pewter, £555; black pewter, £435.

MIDLANDS.—Fluctuations in market prices of copper have resulted in the present value of non-ferrous scrap being slightly lower, merchants viewing the future with a certain amount of caution. Although trading in general remains steady, there may be a doubt existing that the upward trend of recent weeks will be maintained. Metal is changing hands freely with keen price competition for all parcels which are offered.

Tin continues strong, concern over supplies resulting in firm demand. Solder and pewter scrap are finding ready outlets at higher prices.

General indications of metals affected by market conditions are as follows:—

Copper.—Prices show little change, with all grades readily accepted by users. Large and small quantities are moved quickly to take advantage of the existing high tone of the market.

Brass.—Mixed brass remains firmly in demand, brass rod swarf commanding no better price at present.

Gunmetal.—The tone of this metal and allied grades continues good, with prices £1 to £2 per ton higher.

Lead.—A weak market, which provides little hope of future improvement. Prices have dropped by £2 to £3 per ton, mainly due to production exceeding demand. Outlets are available, but prices do not cause much enthusiasm, since they allow only a very small margin of profit.

Aluminium.—No change in prices, and hopes of better trading are still slow to materialize. Old rolled and cast scrap are of almost equal value. Prices offered for aluminium swarf are not too attractive.

Zinc.—Slightly less interest, prices easing by £1 to £2 per ton. Zinc die casting scrap is favoured by most buyers.

† George Cohen, Sons & Co., Ltd., 600 Wood Lane, London, W.12.
‡ Subject to market fluctuations.

Machine Tool Share Market

Dullness and irregularity in price movements, with a generally lower trend, characterised most sections of the stock markets during the period under review. The gilt-edged section was depressed, and, for the most part, British Government stocks displayed a sagging tendency. At the same time, home corporation and dominion loans lost ground, but some improvement was shown towards the close.

Unsettled conditions prevailed in the commercial and industrial sections, which were affected by persistent small selling and a slackening of demand, also by several unfavourable items of company news. An easier tendency developed, and prices for the most part finished at the lowest, although scattered good features have been in evidence.

Among machine tool issues Edgar Allen lost 1s. 3d. at 44s. 6d.; Asquith Machine Tool 9d. at 11s. 6d.; Birmingham Small Arms 3s. at 31s.; British Oxygen 2s. at 23s. 6d.; Broom & Wade 3s. at 24s. 9d.; Chas Churchill 1½d. at 9s. 7½d.; Clarkson Engineers 2s. 6d. at 42s. 6d.; Coventry Gauge & Tool 1½d. at 33s. 7½d.; Craven Bros. (Manchester) 7½d. at 10s. 7½d.; John Harper 3d. at 8s. 6d.; Alfred Herbert 1s. at 77s. 6d.; Ambrose Shardlow 7½d. at 69s. 4½d.; Stedall & Co. 3d. at 8s. 7½d.; and Tap & Die Corporation 3d. at 19s. On the other hand A. A. Jones & Shipman advanced 9d. to 30s.; and W. E. Norton (Holdings) 1s. 9d. to 11s. 3d.

BROOKE TOOL MANUFACTURING CO., LTD. Interim dividend of 5 per cent.

BIRMINGHAM SMALL ARMS CO., LTD. Interim dividend of 4 per cent.

SANDERSON KAYSER, LTD. Final dividend of 12½ per cent, making, with the interim, a total distribution of 17½ per cent. for 1960.

New Companies Registered*

HERTFORD PRECISION ENGINEERS, LTD., 1 Stadium Buildings, Rye House, Hoddesdon, Herts. Registered April 4, 1961. Nom. cap.: £10,000 in £1 shares. Directors: W. A. G. Hill and G. V. Hill.

FUTURMILL-DENFORD LTD., 7 St. George's Square, Huddersfield. Registered May 17, 1961. To carry on business by arrangement with and to the requirements of Futurmill (Conversion) Ltd., as designers, manufacturers of and dealers in machinery, tools, etc. Nom. cap.: £1,000 in £1 shares. Directors: H. S. F. Denford and G. H. R. Denford.

* From the lists compiled by Jordan & Sons, Ltd., Company Registration Agents, 116-118 Chancery Lane, London, W.C.2.

COMPANY		Denom.	Middle Price
Abwood Machine Tools, Ltd.	Ord.	1/-	2/6
Allen (Edgar) & Co., Ltd.	Ord.	£1	44/6
" "	5% Prf.	£1	13/6*
Arnott & Harrison, Ltd.	Ord.	4/-	16/-
Asquith Machine Tool Corp., Ltd.	Ord.	5/-	11/6
" " "	6% Cum. Prf.	£1	16/6xd
Birmingham Small Arms Co., Ltd.	Ord.	10/-	31/-xd
" " "	5% Cum. "A" Prf.	£1	14/6
" " "	6% Cum. "B" Prf.	£1	17/-
" " "	4% 1st Mort. Deb.	Stk.	90½xd
British Oxygen Co., Ltd.	Ord.	5/-	23/6
" " "	6% Cum. Prf.	£1	20/6
Brooke Tool Manufacturing Co., Ltd.	Ord.	5/-	10/3
Broom & Wade, Ltd.	Ord.	5/-	24/9
" "	6% Cum. Prf.	£1	16/6
Brown (David) Corporation, Ltd.	5¼% Cum. Prf.	£1	16/-xd
Buck & Hickman, Ltd.	6% Cum. Prf.	£1	17/-
Butler Machine Tool Co., Ltd.	Ord.	5/-	16/3
" " "	5% Cum. Prf.	£1	14/3xd
Churchill (Charles) & Co., Ltd.	Ord.	2/-	9/7½
" " "	6% Cum. Prf.	£1	25/4½‡
Clarkson (Engrs.), Ltd.	Ord.	5/-	42/6
Cohen (George), 600 Group, Ltd.	Ord.	5/-	14/6
" " "	4½% Cum. Prf.	£1	12/6
Coventry Gauge & Tool Co., Ltd.	Ord.	10/-	33/7½
" " "	5% Cum. Red. Prf.	£1	16/3
Craven Bros. (Manchester), Ltd.	Ord.	5/-	10/7½
Elliott (B.) & Co., Ltd.	Ord.	1/-	3/7½
" "	4½% Red. Cum. Prf.	£1	12/-xd
Firth Brown Tools, Ltd.	4% Cum. Prf.	£1	11/-
Greenwood & Batley, Ltd.	Ord.	10/-	27/-
Harper (John) & Co., Ltd.	Ord.	5/-	8/6
" " "	4½% Red. Cum. Prf.	£1	11/9
Herbert (Alfred), Ltd.	Ord.	£1	77/6
Holroyd (John) & Co., Ltd.	"A" Ord.	5/-	22/6xd
" "	"B" Ord.	5/-	20/6xd
Jones (A. A.) & Shipman, Ltd.	Ord.	5/-	30/-
" "	7% Cum. Prf.	5/-	4/9xd
Kearney & Trecker-C.V.A., Ltd.	5½% Red. Cum. Prf.	£1	11/-
"	Prefd. Ord.	£1	13/9
Kearns (H. W.) & Co., Ltd.	Ord.	5/-	25/-
Kerry's (Gt. Britain), Ltd.	Ord.	5/-	10/7½xd ex rights
Macready's Metal Co., Ltd.	Ord.	5/-	17/-xd
Martin Bros. (Machinery), Ltd.	Ord.	2/-	2/6
Massey (B. & S.), Ltd.	Ord.	5/-	12/-
Newall Engineering Co., Ltd.	Ord.	2/-	11/9
Newman Industries, Ltd.	Ord.	2/-	6/3
" "	6% Prf. Ord.	5/-	5/-
Noble & Lund, Ltd.	Ord.	2/-	6/-
Norton, W. E. (Holdings), Ltd.	Ord.	2/-	11/3
Osborn (Samuel) & Co., Ltd.	Ord.	5/-	58/-
" "	5½% Cum. Prf.	£1	23/-
Pratt (F.) & Co., Ltd.	Ord.	5/-	18/9xd
Sanderson Kayser, Ltd.	Ord.	10/-	40/-
" "	6½% Cum. Prf.	£1	17/-
Scottish Machine Tool Corporation, Ltd.	Ord.	4/-	12/3
Shardlow (Ambrose) & Co., Ltd.	Ord.	£1	69/4½
Shaw (John) & Sons, Wolverhampton, Ltd.	Ord.	5/-	20/-
Sheffield Twist Drill & Steel Co., Ltd.	Ord.	4/-	20/-xd
" " "	5% Cum. Prf.	£1	14/3
Stedall & Co., Ltd.	Ord.	5/-	8/7½
Sykes (W. E.), Ltd.	"B" non-voting Ord.	10/-	32/6
Tap & Die Corporation, Ltd.	Ord.	5/-	19/-
" " "	4½% Deb. 1961-1977	Stk.	82½xd
Wadkin, Ltd.	Ord.	10/-	26/-xd
Ward (Thos. W.), Ltd.	Ord.	£1	83/6
" "	5% Cum. 1st Pref.	£1	14/-
" "	5% Cum. 2nd Pref.	£1	22/6
Willson Lathes, Ltd.	Ord.	1/-	3/4½

The Middle Prices given in the list are in several cases nominal prices only and not actual dealing prices. Every effort is made to ensure accuracy, but no liability can be accepted for any error. * Sheffield price. ‡ Birmingham price.

BRITISH MACHINE TOOL

Exports of New Machine Tools

Countries	Bar and Chucking Automatics		Vertical Boring Machines		Other Boring Machines		Drilling Machines		Gear-cutting Machines		Grinding, Lapping and Honing Machines		Capstan and Turret Lathes		Other Lathes	
	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £
Commonwealth																
South Africa	—	—	183 (1)	6,352	—	—	220 (66)	4,646	—	—	161 (14)	5,185	162 (4)	6,895	515 (26)	20,679
India	—	—	1,089 (1)	60,754	735 (2)	13,644	1,710 (21)	57,018	—	—	1,055 (39)	48,715	1,008 (22)	44,324	251 (19)	9,407
Pakistan	—	—	293 (2)	8,104	—	—	81 (1)	3,115	—	—	12 (1)	224	29 (2)	1,387	—	—
Australia	405 (3)	28,856	—	—	136 (3)	8,499	489 (15)	15,956	—	—	1,012 (36)	45,789	687 (26)	28,462	1,897 (64)	65,960
New Zealand	31 (1)	5,419	—	—	—	—	55 (7)	1,536	—	—	161 (30)	7,826	177 (4)	7,279	624 (41)	19,676
Canada	—	—	338 (1)	10,350	6 (1)	959	3 (1)	95	—	—	541 (15)	21,158	35 (2)	2,519	237 (9)	9,522
Miscellaneous	—	—	—	—	7 (2)	593	188 (40)	5,771	—	—	204 (15)	8,320	—	—	325 (22)	9,712
Foreign																
Soviet Union	—	—	101 (1)	10,722	—	—	—	—	54 (2)	4,331	226 (3)	20,151	—	—	171 (2)	5,865
Sweden	—	—	—	—	—	—	1 (1)	109	—	—	166 (3)	7,438	883 (18)	41,798	323 (26)	15,898
Norway	—	—	—	—	—	—	5 (5)	155	—	—	44 (2)	1,975	11 (1)	835	32 (7)	1,255
Denmark	—	—	—	—	—	—	186 (2)	3,843	—	—	16 (2)	743	47 (2)	3,020	31 (9)	1,608
Western Germany	39 (1)	2,000	—	—	90 (1)	1,834	116 (29)	2,024	—	—	105 (4)	5,798	164 (5)	4,175	692 (43)	29,594
Netherlands	—	—	—	—	—	—	346 (16)	9,262	—	—	78 (9)	3,207	272 (6)	7,021	—	—
Belgium	—	—	100 (1)	3,230	42 (1)	3,213	22 (21)	815	—	—	329 (5)	8,731	305 (6)	10,492	45 (9)	1,579
France	—	—	—	—	—	—	1 (1)	90	27 (1)	3,048	181 (5)	6,603	81 (1)	4,540	18 (1)	1,669
Switzerland	—	—	—	—	—	—	96 (6)	4,721	—	—	116 (7)	6,235	171 (5)	13,325	248 (77)	13,000
Spain	—	—	—	—	—	—	639 (4)	16,320	—	—	160 (6)	13,847	—	—	33 (1)	2,325
Italy	470 (2)	31,559	—	—	63 (1)	3,828	28 (1)	3,130	—	—	326 (12)	23,760	242 (2)	16,844	20 (12)	804
U.S. America	157 (1)	7,727	—	—	—	—	81 (5)	1,995	—	—	1,013 (14)	34,604	63 (2)	1,633	691 (36)	28,118
Miscellaneous	356 (2)	22,253	130 (1)	4,812	249 (4)	20,362	1,602 (57)	34,912	616 (10)	41,437	1,211 (44)	74,863	475 (15)	23,026	882 (56)	45,683
Total	1,458 (10)	97,814	2,224 (8)	104,324	1,328 (15)	52,932	5,869 (299)	165,513	697 (13)	48,816	7,117 (266)	345,172	4,812 (123)	217,575	7,035 (460)	282,354

Total exports of reconditioned machine tools:—Quantity: No., 86; Weight, 4,239 cwt.; Value, £39,347.
Total exports of imported machine tools:—Quantity: Weight, 1,438 cwt.; Value, £45,904.

Imports of New Machine Tools

Country of Origin	Bar and Chucking Automatics		Vertical Boring Machines		Other Boring Machines		Drilling Machines		Gear-cutting Machines		Grinding, Lapping and Honing Machines		Capstan and Turret Lathes		Other Lathes	
	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £
Sweden	—	—	—	—	—	—	118 (7)	2,721	55 (1)	4,106	861 (12)	49,317	—	—	47 (1)	1,668
Western Germany	155 (4)	7,768	9 (3)	289	1,194 (3)	37,586	70 (20)	4,714	199 (4)	17,797	1,887 (55)	97,116	856 (26)	59,102	1,535 (19)	49,936
France	260 (2)	8,715	16 (1)	3,733	—	—	8 (4)	201	—	—	—	—	12 (1)	591	251 (7)	10,454
Switzerland	211 (18)	31,141	26 (1)	3,627	44 (2)	4,560	13 (2)	752	4 (1)	729	237 (13)	23,318	123 (2)	10,782	687 (22)	43,315
U.S. America	433 (2)	23,517	14 (2)	1,300	—	—	8 (1)	1,210	4,945 (25)	345,333	1,880 (35)	218,199	142 (2)	9,396	827 (11)	52,525
Miscellaneous	20 (2)	682	41 (1)	2,828	282 (4)	10,828	282 (29)	10,801	250 (2)	5,258	412 (28)	14,453	—	—	846 (74)	28,525
Total	1,079 (28)	71,823	106 (8)	11,777	1,520 (9)	52,974	499 (63)	20,399	5,453 (33)	373,223	5,277 (143)	402,403	1,133 (31)	79,871	4,193 (134)	186,423

Total imports of reconditioned machine tools:—Quantity: No., 36; Weight, 3,220 cwt.; Value, £67,284.

IMPORTS AND EXPORTS (Classified)

and Parts during February, 1961

Milling Machines		Presses		Sheet-metal Working Machines		Sawing Machines		Screwing and Threading Machines		Planing, Shaping and Slotting Machines		Unit Transfer Machines and Heads		Other Machines		Machine Tool Parts*		Total	
Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt.	Value £	Quantity. Cwt. and No.	Value £
52 (2)	3,138	867 (12)	14,541	354 (8)	5,471	61 (24)	1,275	79 (3)	3,817	122 (4)	3,499	—	—	131 (15)	3,835	578	21,168	3,485 (179)	100,501
62 (4)	2,982	124 (20)	6,133	2 (1)	98	—	—	315 (3)	22,181	854 (1)	19,629	—	—	1,237 (21)	57,014	846	33,737	9,288 (154)	375,636
—	—	—	—	—	—	—	—	—	—	—	—	—	—	20 (2)	793	73	1,496	498 (8)	15,119
739 (18)	37,156	353 (10)	10,640	623 (11)	15,626	173 (5)	4,453	213 (6)	14,345	394 (12)	14,976	—	—	829 (21)	42,258	2,205	113,677	10,175 (230)	446,653
111 (4)	4,491	229 (11)	3,729	72 (5)	1,921	63 (14)	1,712	—	—	173 (11)	6,115	—	—	16 (1)	705	65	4,377	1,777 (129)	64,786
618 (10)	32,082	11 (1)	160	322 (3)	6,018	8 (2)	176	—	—	66 (2)	3,150	—	—	142 (1)	1,999	2,100	32,387	4,427 (48)	120,575
21 (1)	1,223	224 (7)	11,514	155 (12)	3,109	122 (28)	3,713	28 (3)	1,471	55 (5)	1,541	—	—	112 (14)	3,448	781	35,799	2,222 (149)	86,214
—	—	—	—	114 (2)	10,550	—	—	—	—	—	—	—	—	—	—	6	3,726	672 (10)	55,345
45 (1)	1,459	—	—	—	—	4 (1)	247	—	—	—	—	—	—	228 (6)	14,592	87	9,328	1,737 (56)	90,869
—	—	—	—	58 (1)	1,147	—	—	—	—	—	—	—	—	— (1)	97	39	3,003	189 (17)	8,467
—	—	—	—	—	—	22 (1)	434	21 (1)	1,582	—	—	—	—	3 (1)	48	44	4,879	370 (18)	16,157
832 (14)	26,386	7 (1)	693	117 (3)	9,173	7 (1)	902	252 (8)	18,444	18 (2)	1,498	—	—	50 (2)	10,274	70	7,583	2,559 (114)	120,378
40 (2)	1,442	247 (8)	12,957	10 (1)	81	—	—	193 (3)	10,568	7 (1)	177	—	—	35 (1)	1,194	241	13,409	1,469 (47)	59,318
184 (2)	10,928	39 (5)	2,083	19 (1)	749	11 (1)	248	—	—	—	—	—	—	16 (3)	640	557	8,660	1,669 (55)	51,368
—	—	206 (19)	7,181	46 (1)	2,368	—	—	20 (1)	1,582	20 (2)	492	—	—	4 (2)	518	189	16,107	793 (34)	44,198
114 (3)	5,521	459 (1)	8,408	—	—	—	—	20 (1)	1,772	—	—	12 (1)	793	41 (1)	3,085	41	3,491	1,318 (102)	60,351
—	—	—	—	—	—	—	—	—	—	—	—	—	—	44 (2)	4,425	32	2,000	908 (13)	38,917
710 (3)	35,696	1,781 (3)	30,715	—	—	—	—	—	—	—	—	—	—	24 (1)	3,183	72	6,282	3,736 (37)	155,801
—	—	40 (1)	1,001	38 (5)	4,127	4 (1)	162	—	—	62 (1)	2,242	—	—	536 (10)	18,354	245	13,995	2,930 (76)	113,958
703 (12)	37,931	530 (18)	16,963	772 (12)	30,733	17 (4)	353	233 (4)	22,600	593 (16)	19,064	—	—	4,837 (99)	162,828	487	32,943	13,693 (354)	590,763
4,251 (76)	200,435	5,117 (117)	126,718	2,702 (66)	91,171	492 (82)	13,675	1,374 (33)	98,362	2,364 (57)	72,383	12 (1)	793	8,305 (204)	329,290	8,758	368,047	63,915 (1,830)	2,615,374

Figures in parentheses denote number of machines. * Not including machine tool cutting parts.

and Parts during February, 1961

Milling Machines		Presses		Sheet-metal Working Machines		Sawing Machines		Screwing and Threading Machines		Planing, Shaping and Slotting Machines		Unit Transfer Machines and Heads		Other Machines		Machine Tool Parts*		Total	
Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt. and No.	Value £	Quantity. Cwt.	Value £	Quantity. Cwt. and No.	Value £
24 (1)	1,264	—	—	71 (2)	2,374	—	—	5 (1)	353	17 (13)	1,122	—	—	—	—	95	10,640	1,293 (38)	73,565
1,621 (28)	79,098	1,248 (17)	33,409	206 (27)	5,762	479 (38)	16,940	229 (26)	10,898	84 (5)	3,404	1,342 (2)	60,745	3,147 (75)	112,187	297	32,304	14,558 (352)	629,055
899 (19)	42,226	272 (11)	15,591	33 (4)	10,573	4 (1)	274	279 (4)	14,933	—	—	—	—	51 (35)	6,106	152	9,496	2,237 (89)	122,893
435 (13)	31,966	410 (2)	11,999	114 (3)	3,274	—	—	102 (8)	11,562	9 (1)	715	—	—	682 (131)	22,182	207	35,956	3,304 (219)	235,878
975 (9)	83,210	697 (8)	24,400	449 (5)	34,272	30 (1)	1,245	—	—	—	—	—	—	925 (22)	84,339	1,830	174,932	13,155 (123)	1,053,878
779 (20)	24,902	1,451 (28)	37,822	278 (36)	16,050	55 (17)	2,673	11 (1)	1,420	499 (3)	9,347	6 (1)	1,829	744 (20)	41,593	173	13,629	6,129 (266)	222,640
4,733 (90)	262,666	4,078 (66)	123,221	1,151 (77)	72,305	568 (57)	21,132	626 (40)	39,166	609 (22)	14,588	1,348 (3)	62,574	5,549 (283)	266,407	2,754	276,957	40,676 (1,087)	2,337,909

Figures in parentheses denote number of machines. * Not including machine tool cutting parts.

PRICES OF MATERIALS

All prices per ton except where otherwise stated.

Pig Iron

Foundry and Forge No. 3, Class 2

Middlesbrough (10 tons or over)	£21 17 0
Birmingham (10 tons or over)	£21 9 3

Phos. Over 0·1 up to 0·4%

Birmingham (6 ton lots)	£23 5 0
Grangemouth (6 ton lots)	£23 10 0

Hæmatite

English No. 1 (10 tons or over)

N.E. Coast (made in N.E.)	£23 19 0
Scotland	£24 5 6
Sheffield	£25 9 0
Birmingham	£25 13 0

Welsh 10 tons or over £23 19 0

Steel Products

Medium plates (50 tons and over)	£43 16 6
Mild steel plates, ordinary (50 tons and over)	£40 7 0
Boiler plates (50 tons and over)	£42 17 0
Flat bars, 5 in. wide and under (50 tons or over)	£39 1 0
Round bars, under 3 in. (50 tons or over)	£39 1 0
Billets, rolling quality, soft U.T. (100 tons or over)	£31 15 6

Phosphor Bronze

Ingots (2B8) (A.I.D.) d/d	£322 0 0

Copper

Cash (mean)	£244 12 6
Cold rolled and hot rolled sheets 4 ft. by 2 ft. by 10 SWG	£320 5 0
Rods, $\frac{7}{16}$ in. to $\frac{1}{2}$ in. diam.	£338 10 0
Tubes, $1\frac{1}{2}$ in. bore by 10 SWG, ton lots, per lb.	3s. 3½d.
Wire rod, black, hot-rolled ($\frac{1}{4}$–$\frac{9}{16}$ in.), English	£261 2 6

Zinc

Refined, minimum 98 per cent purity, current month (mean)	£81 16 3

Brass

Tubes, solid drawn, basic per lb.	1s. 11½d.
Strip 63/37, 6in. by 10 SWG coils, ton lots	£267 15 0—£270 15 0
Rods, $\frac{1}{2}$–3 in. diam. (59 per cent copper)	2s. 1½d.

Yellow Metal

Condenser plates, per ton	£197 0 0
Rods, per lb.	2s. 2½d.

Aluminium

Ingots, min. 99·5 per cent Canadian d/d	£186 0 0

Tinplates

*U.K. Home trade: Cold reduced, f.o.r. makers works (15-50 tons)	£3 6 8
U.K. Export: Hot rolled basis, f.o.r. works port	73s. 6d.—76s. 0d.
Cold reduced basis, f.o.r. works port	73s. 6d.—76s. 0d.

Gunmetal

Ingots, B.S. 1400 L.G.2, delivered	£232 0 0

* Official maximum price, after allowing for adjustments for increase in price of tin.

MAKERS' PRICES

Hexagon Steel Bars[1]

Sizes in inches from 1 in. up to 2·21 and 2·41 a/f ex works, 2 tons basis	£42 17 0
Free cutting black	£47 6 6

Reeled Steel Bars[1]

Single-reeled, 1½ in. upwards, f.o.t. works (+ usual extra for sizes)	£43 9 6
Free cutting	£47 19 0

Precision-ground Mild Steel[2]

1-in. diam. ± 0·00025-in. 4-ton lots, per cwt.	124s. 6d.

Bright Ground Stainless Steel Bars[3]

EN56AM (martensitic, free cutting)	£304 10 0
EN58AM (austenitic free cutting)	£377 10 0

Prices are basic, subject to extras.

High-speed Steel

Black random length bar. All prices basic, per lb., subject to extras:

Molybdenum "66"	6s. 5d.
Molybdenum "46"	6s. 3d.
14 per cent tungsten	6s. 11d.
16 per cent tungsten	7s. 4d.
18 per cent tungsten	7s. 9d.
22 per cent tungsten	9s. 2d.
5 per cent cobalt	10s. 10d.
4·75/5·25 molybdenum + 6·0/6·75 tungsten + 1·75/2·05 vanadium per cent (5-6-2)	6s. 7d.

Precision-ground, High-speed Free-turning Brass Rod[2]

½-in. diam. ±0·00025-in., 2 ton lots, per lb.	2s. 7½d.

Grey Iron Rod

Die Cast[4] in random lengths 18 in. to 26 in. rough machined $\frac{1}{16}$-in. above listed size. Extra for definite lengths. Discounts for orders over £150.

	Per cwt. net. Mark I	Mark III
¾ or ⅞ in.	260s. 3d.	338s. 3d.
1 or 1¼in.	208s. 4d.	267s. 3d.
1½ to 1¾ in.	146s. 3d.	181s. 7d.
1⅞ to 2 in.	112s. 7d.	133s. 6d.
2¼ to 3¼ in.	97s. 1d.	112s. 9d.
3½ to 12 in.	91s. 9d.	105s. 3d.

Continuous Cast

10-ft. lengths, centreless machined 1 to 3-in. diam. + 0·010 to 0·020 in., prices as quoted for die cast bar[4]

centreless ground 1 or 1⅛ in. +0·010 in. Extra		208s. 4d.
for hardenable alloy iron[5]	1⅛ to 1½ in.	146s. 3d.
	1⅝in. to 2 in.	112s. 7d.
Per cwt. net	2¼ to 3¼ in.	97s. 1d.

Stellite[6]

Welding Rods, plain

¼ in. diam., per lb.	30s. 0d.

Toolbits

¼ in. sq. × 4 in., each	22s. 3d.

[1] Colvilles, Ltd., Glasgow, and 17 Grosvenor Street, London, W.1. [2] Pratt, Levick & Co., Ltd., Chester. [3] Spartan Steel & Alloys, Ltd., St. Stephens Street, Birmingham, 6. [4] Sheepbridge Alloy Castings, Ltd., Sutton-in-Ashfield. [5] "Flocast," Harold Andrews Sheepbridge, Ltd., Halesowen. [6] Deloro Stellite, Ltd., Highlands Road, Shirley, Solihull.

BASIC PRICES FROM LONDON STOCK[6]

Free Cutting Steel

Bright cold drawn: (Usaspead) over 1 to 2 in.	£59 4 6
Lead bearing (Usaled)	£63 11 0
Precision ground, 1¾ in.	£84 14 6

Bright Drawn

M.S. bars (M.M.C.) over 1½ to 2 in.	£56 10 0
Square edge flats (Usaflat)	£73 6 6
M.S. angles (Usaspead)	£100 6 6
Case hardening (EN) (Usacase over 1½ to 2 in.	£62 10 0
M.S. bars (EN3B) (Usamild) over 1½ to 2 in.	£58 16 6
Carbon manganese semi-free cutting case hardening (EN202) (Usaspead 202) over 1½ to 2 in.	£71 5 0
35/45 ton tensile (EN6) (Usen) over 1 to 1½ in.	£67 3 0
0·4 carbon normalized (Usaspead "40") over 1½ to 2 in.	£69 5 0
0·45 carbon normalized EN9 (Usaspead 55)	£69 15 0
Carbon manganese steel to Specification EN16T (Usaspead 5565), per ton	£126 17 0

Ground Flat Stock

18-, 24-, and 36-in. lengths (Usaspeed). List prices plus 10 per cent, less 5 per cent.

Oil Hardening Cast Steel

Non-shrink (Usaspead N.S.O.H.), ¾ in. to 2½ in., per lb.	1s. 11d.
Non-distorting heavy duty (Usaspead H.C.H.C.), ¾ in. to 2¾ in., per lb.	4s. 2d.

Silver Steel

(0·194-in. to 1½-in.)

Genuine Stubs quality, per lb.	4s. 10d. less 27½%
M.M.C. quality, per lb.	2s. 8d. + 6½%
Boxes of 16 assorted sizes, $\frac{1}{16}$ in. to ¾ in. diam.	7s. 6d.

Stainless Steel

KE40AM (free cutting), per lb.	3s. 8d.

Glacier Machined Bronze Bars

Phosphor bronze (2B8) / Lead bronze	Prices on application

High-speed Steel

18 per cent tungsten. Prices on application.

Toolholder bits:

Usaspead "Super" / "Supreme" / Cobalt 10	List price

Shimstock

Steel assorted, per tin	3s. 6d.
Brass " "	7s. 3d.

[6] Macready's Metal Co., Ltd., Pentonville Road, N.1. Subject to confirmation by London Office. Delivered free by van in London area.

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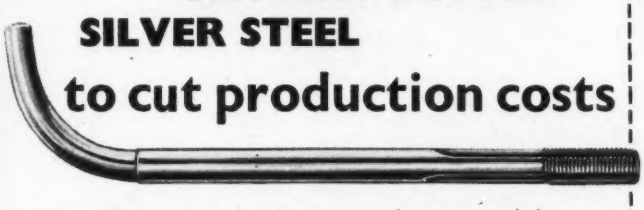
GENUINE P.S. STUBS SILVER STEEL to cut production costs



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3 Circular split die
4 Reamer
5 Plug Gauge
6 Guess what?

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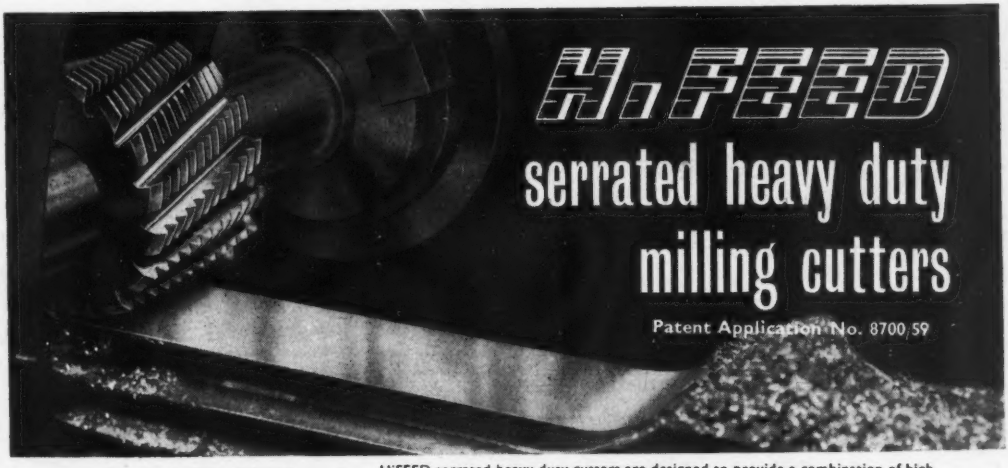

HiFEED serrated heavy duty milling cutters

Patent Application No. 8700/59

BRAYSHAW TOOLS LIMITED
BELLE VUE WORKS, MANCHESTER 12.
Phone: EASt 1046 (3 Lines)
Grams: Hardening M/C.

HiFEED serrated heavy duty cutters are designed to provide a combination of high rate of stock removal and good surface finish.

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INCREASED PRODUCTION, particularly on work hardening and high tensile materials.
EFFICIENT HEAT DISSIPATION resulting from the break up of the cutting edges enables **HIGHER FEEDS AND SPEEDS** to be employed.

Primarily designed for heavy stock removal HiFEED cutters produce a surface finish acceptable for most applications. An alternative design, offering similar advantages plus superior surface finish when required, is also available.
HiFEED cutters INCREASE production REDUCE costs.
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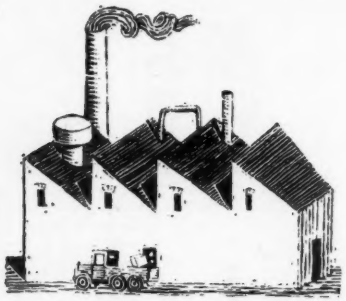

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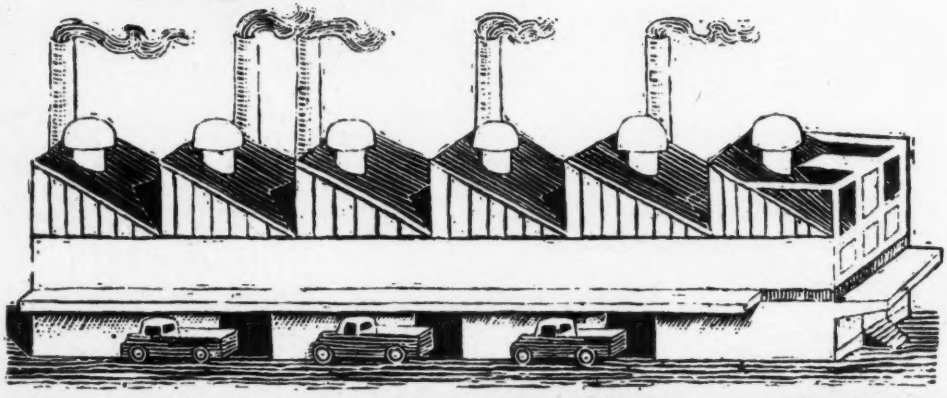

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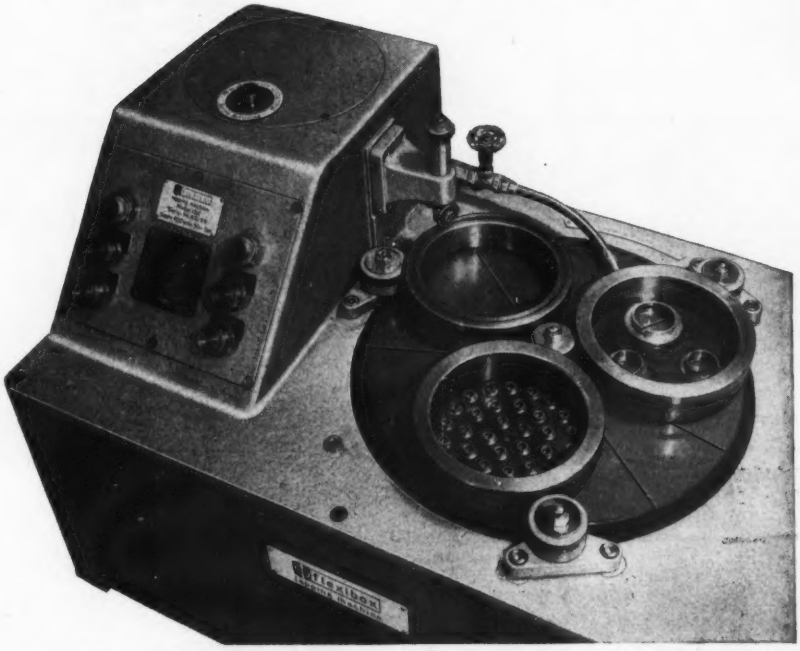

the flexibox range

Model	Max. diameter of work
Model 15A bench lapper	5½ inches
Model IV	7½ inches
Model VA	10½ inches

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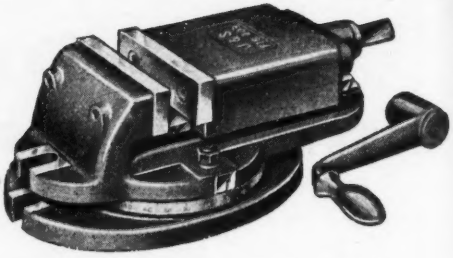

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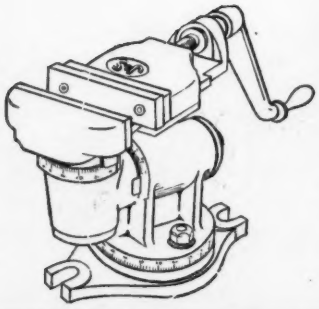

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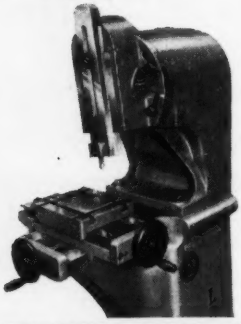

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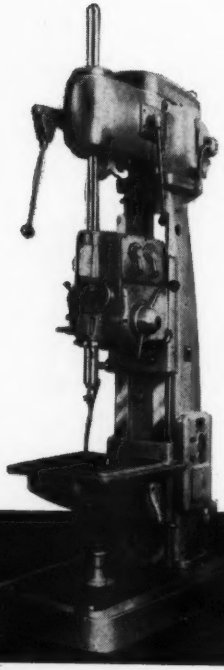

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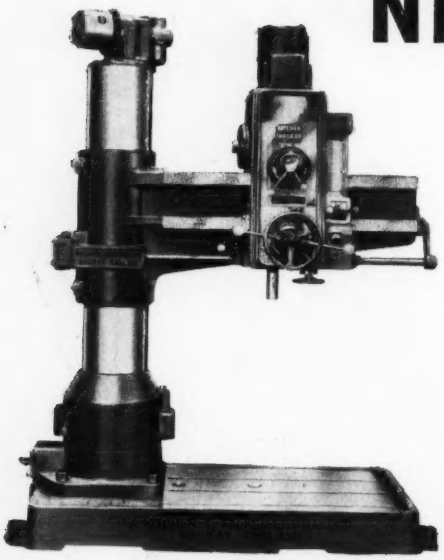

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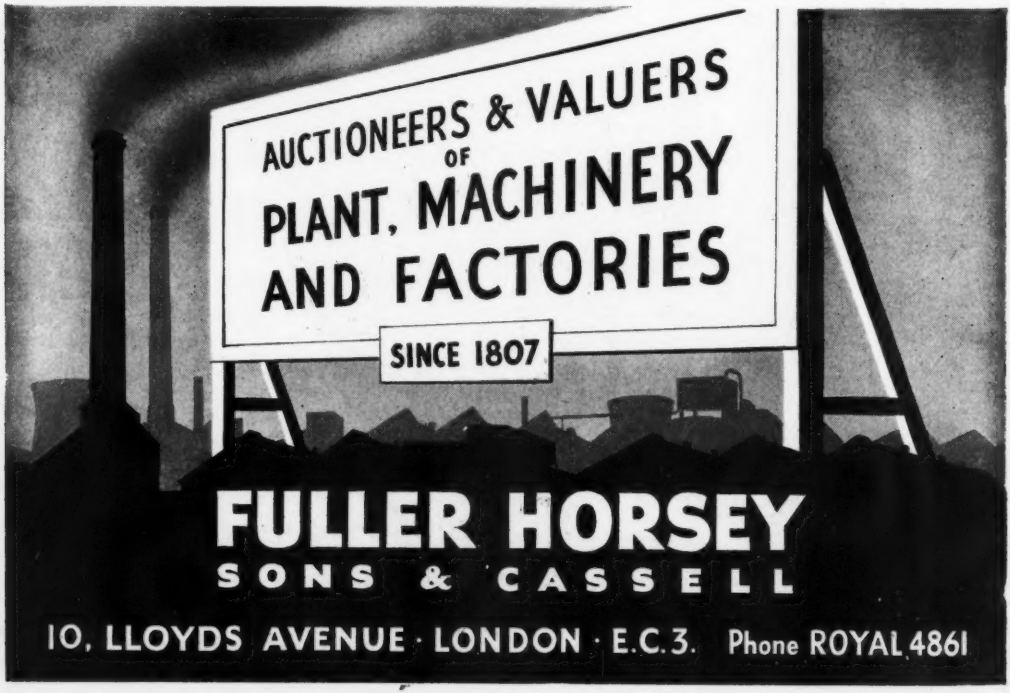

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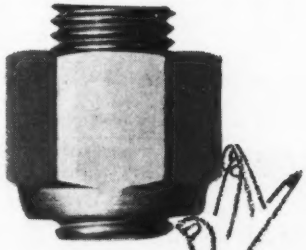

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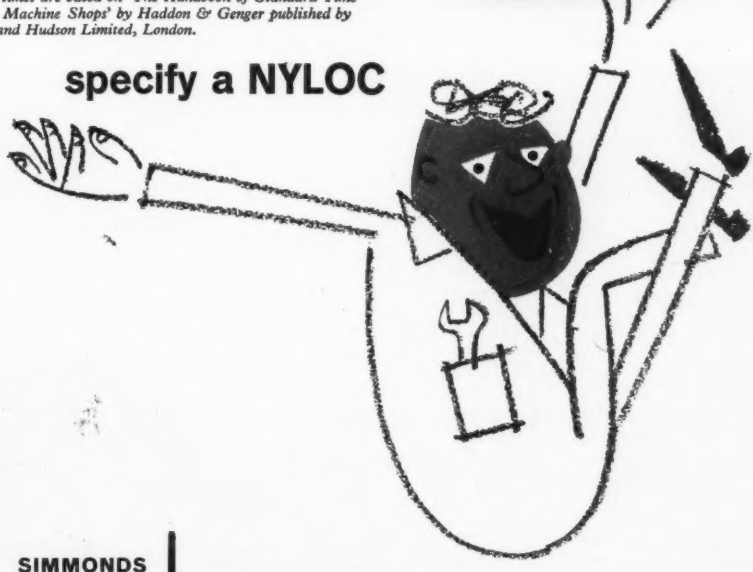

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4	28in. by 8in.	19in.
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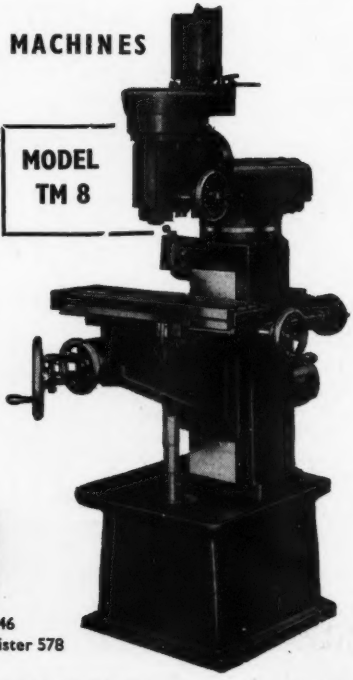

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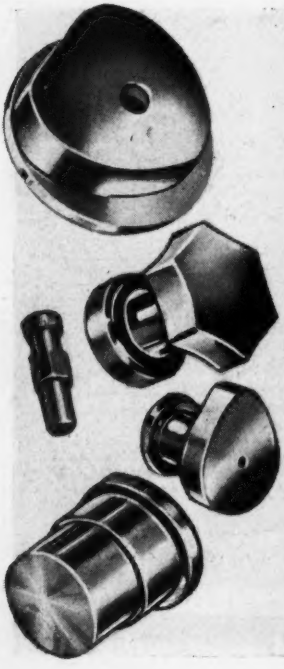

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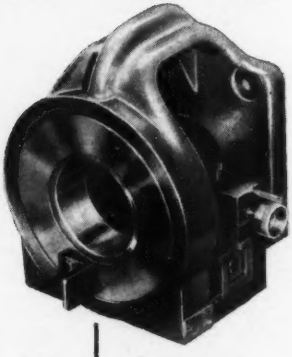

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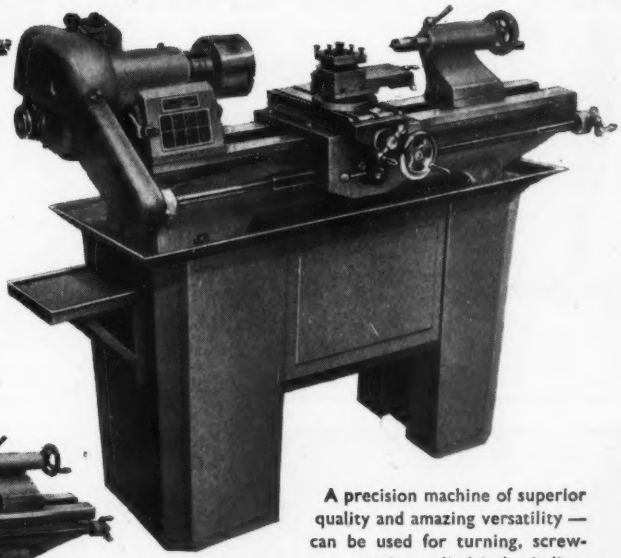

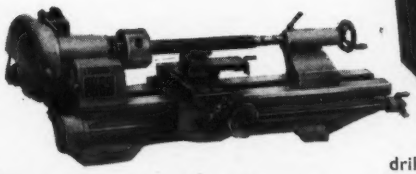

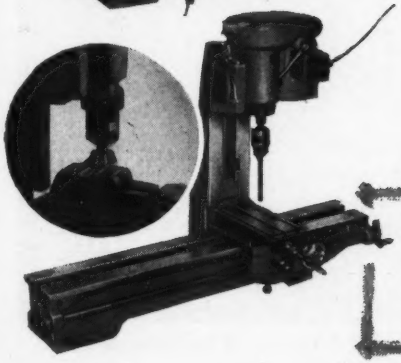

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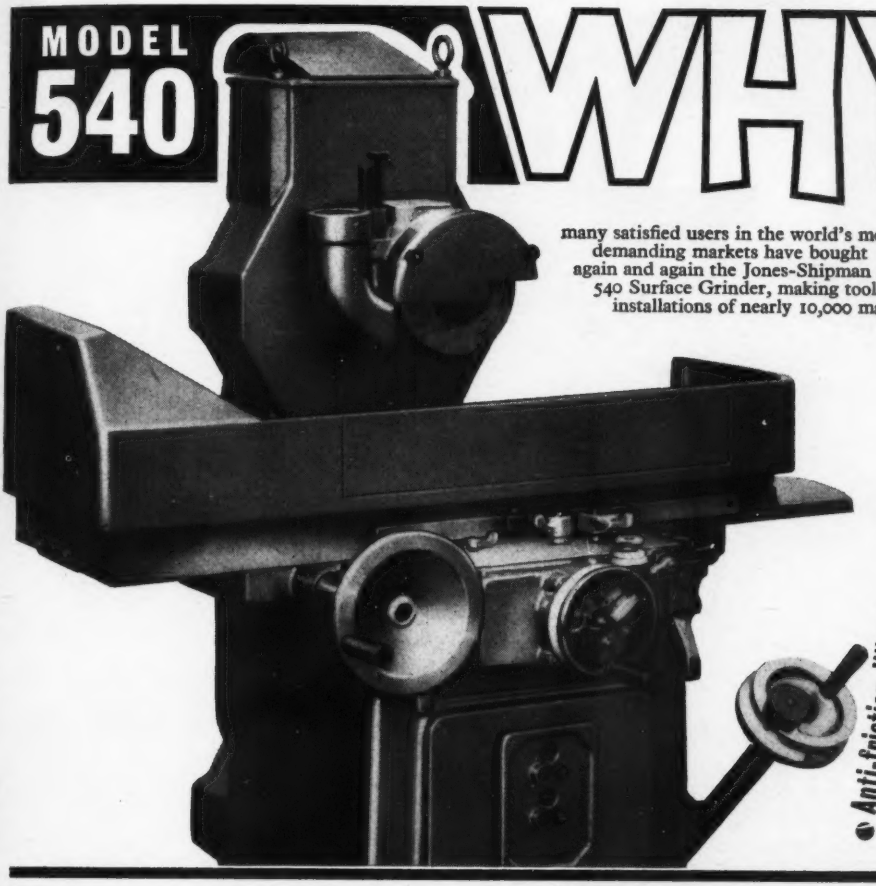

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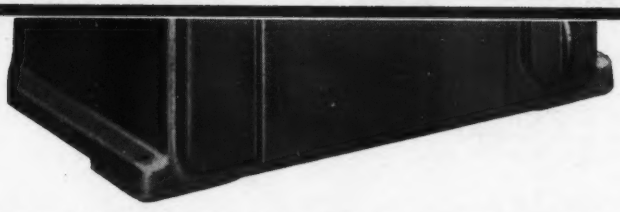

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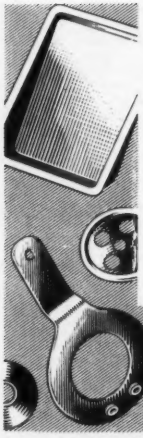

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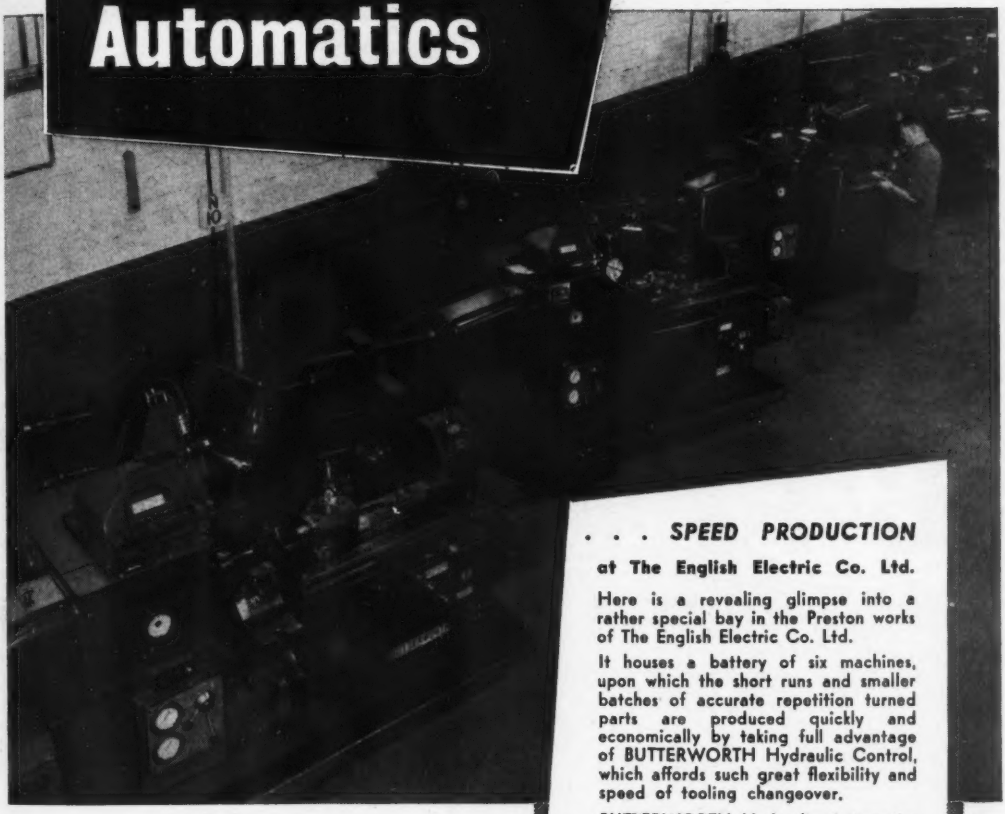

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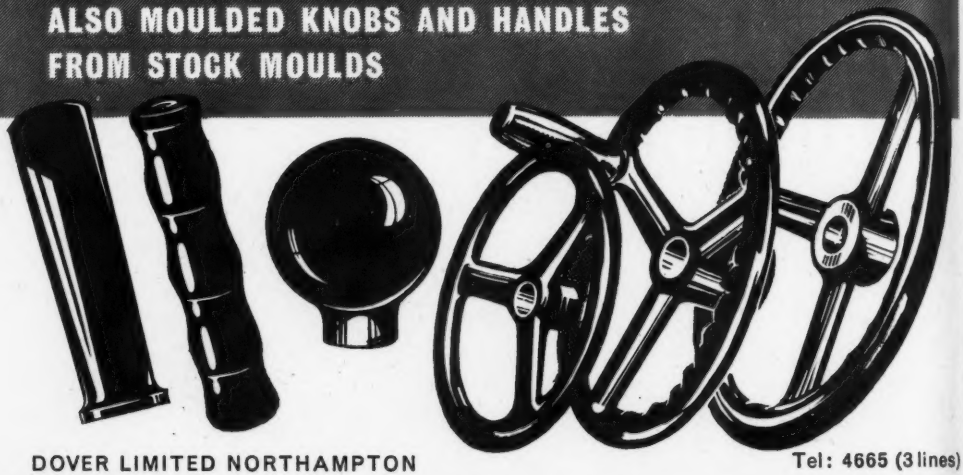

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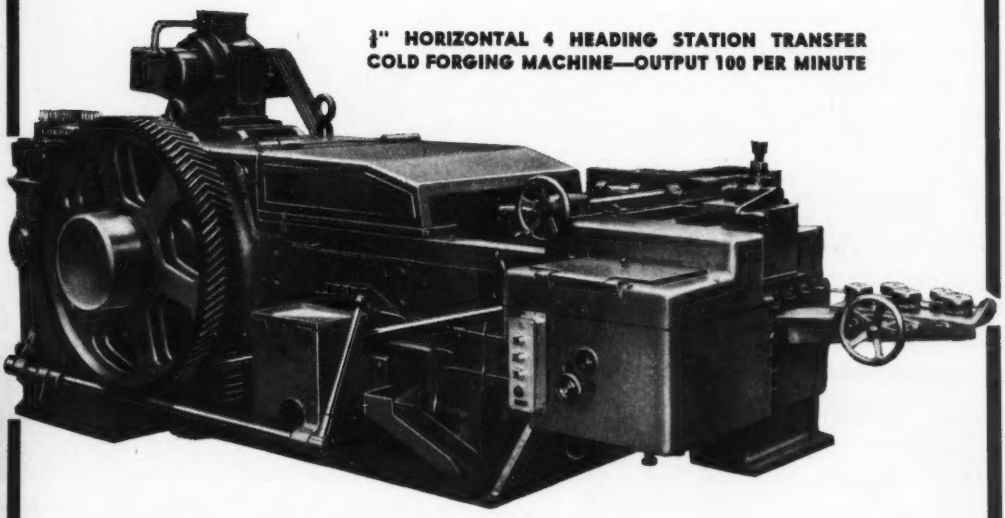

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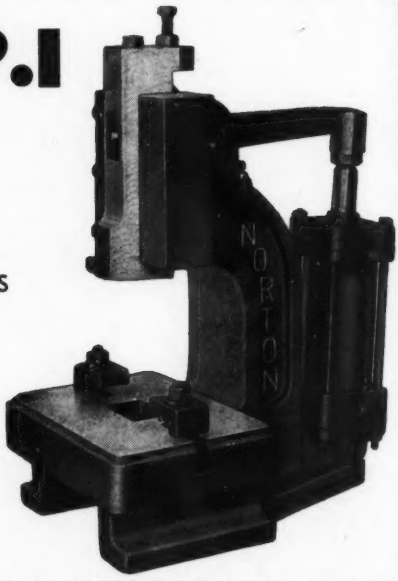

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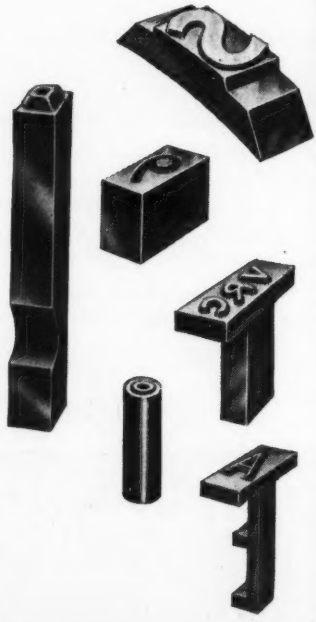

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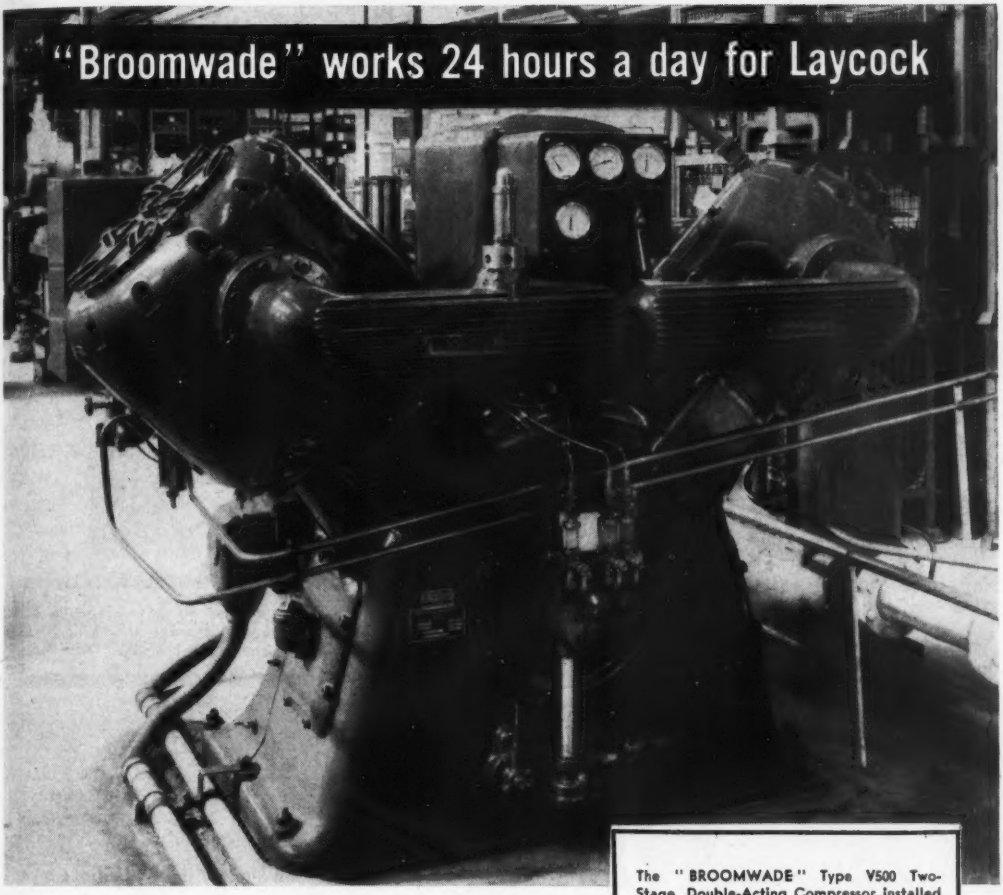

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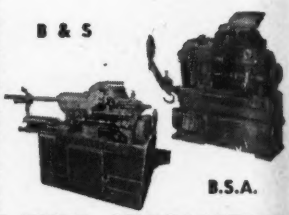

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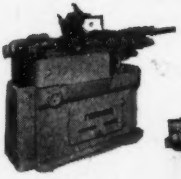
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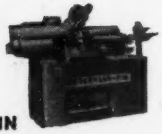
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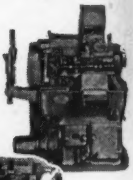
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★ May we visit your works and quote for reconditioning your machine?

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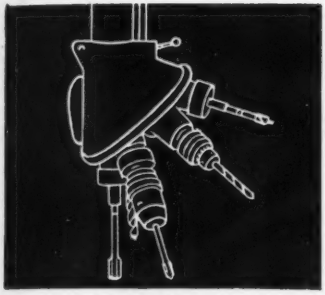

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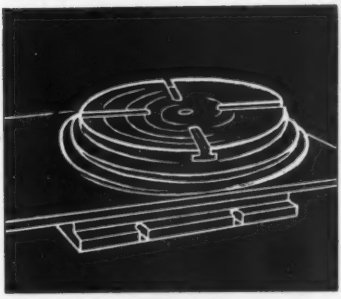

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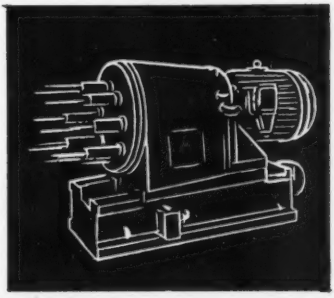

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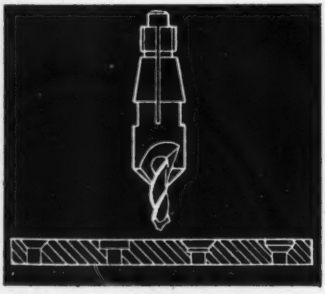

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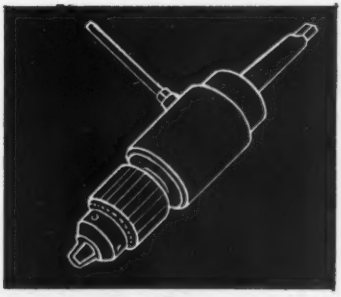

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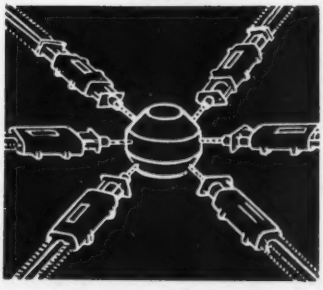
do two operations in the time of one. Combined drilling and countersinking, counterboring deburring or trepanning, with ordinary twist drills.



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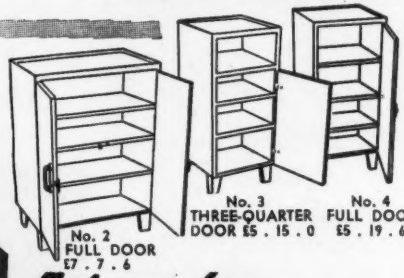

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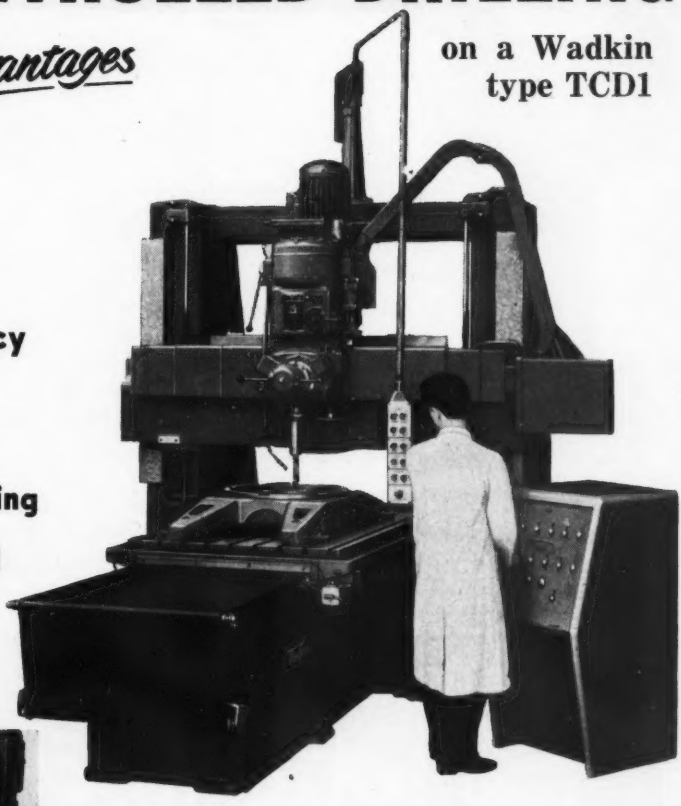

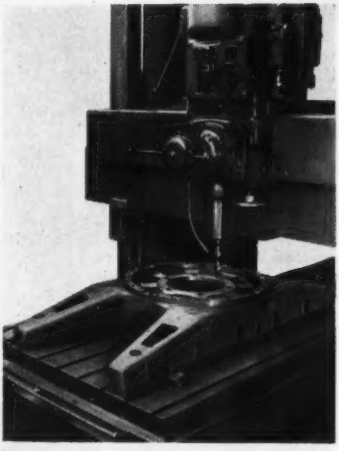

Wadkin Tape Controlled Drilling Machine drilling a cast-iron rotating slideway.

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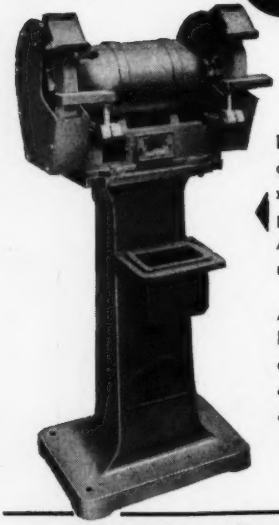

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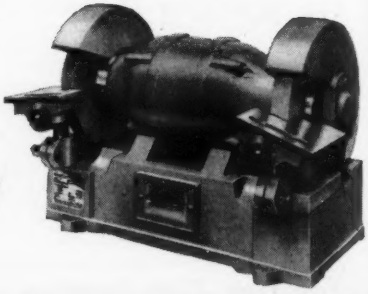

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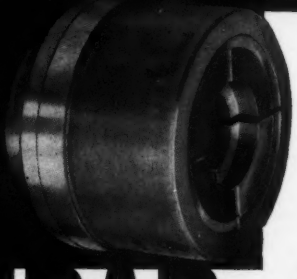

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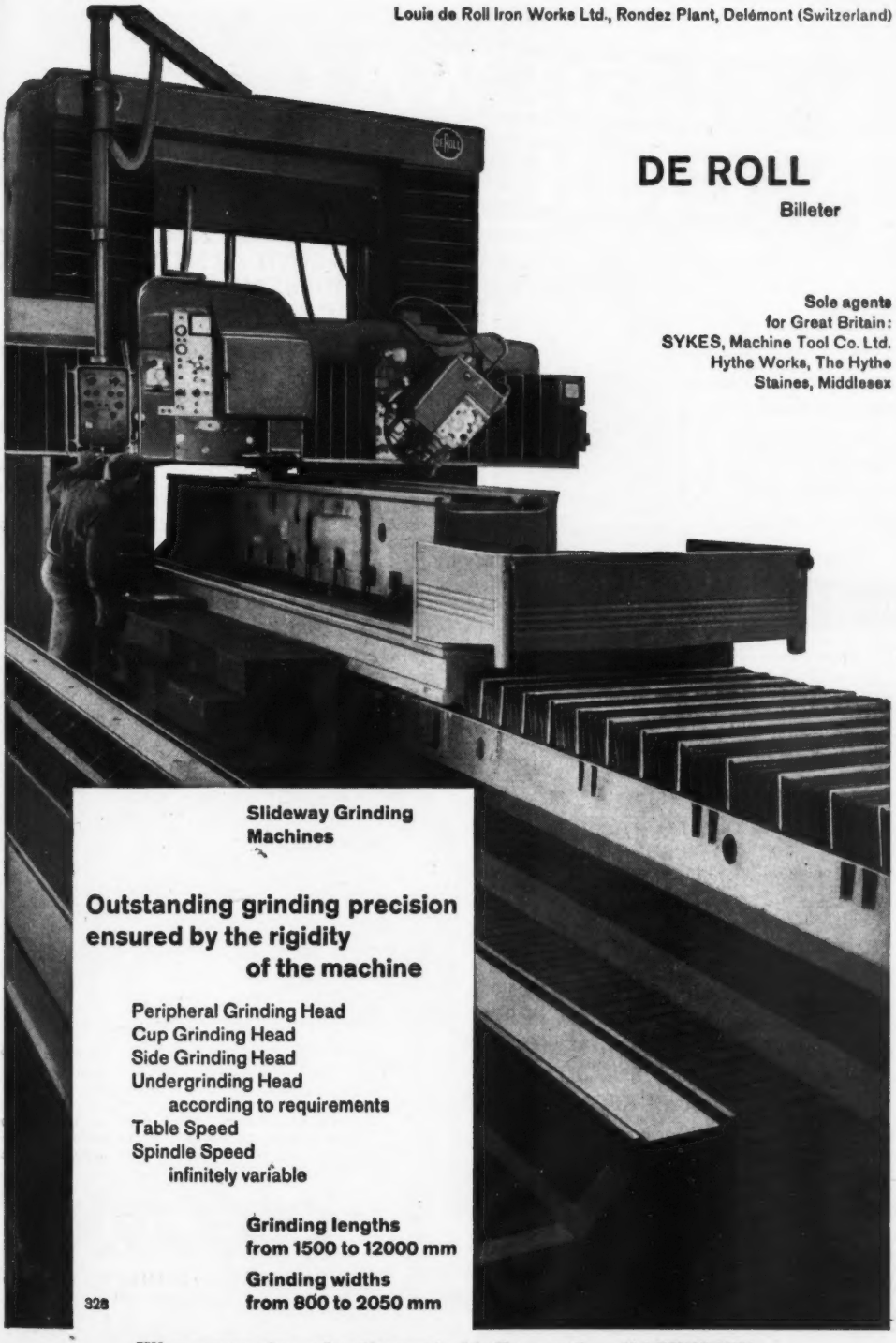

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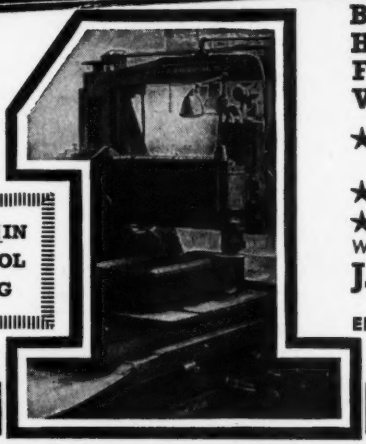

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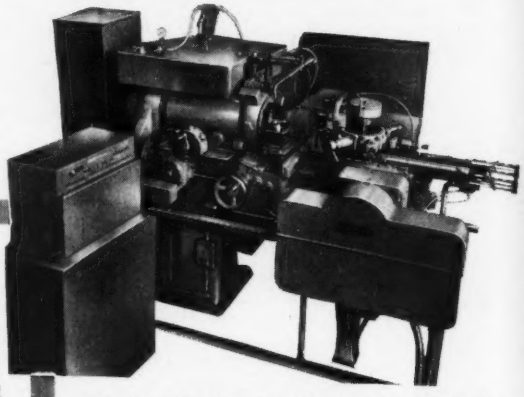

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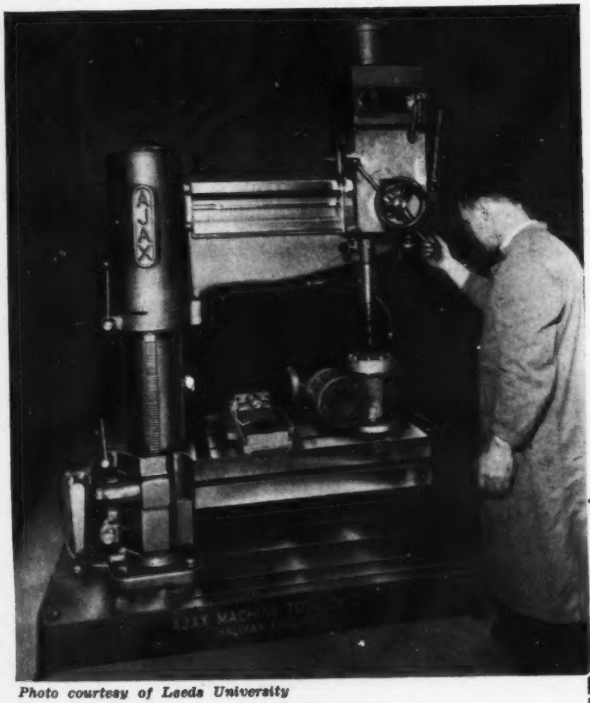

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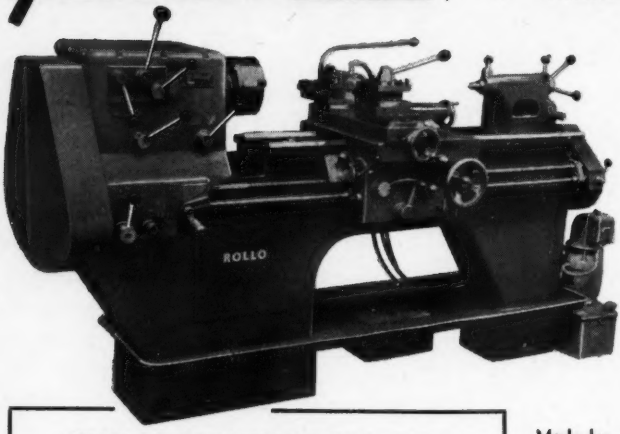

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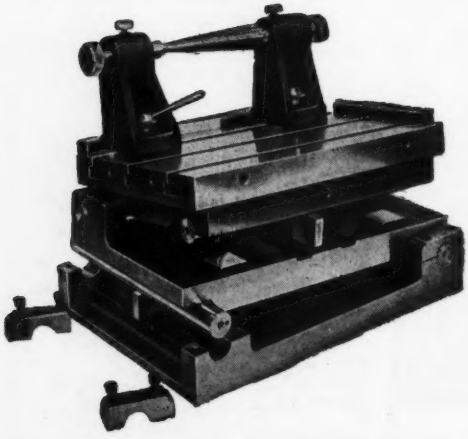

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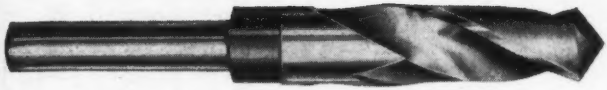

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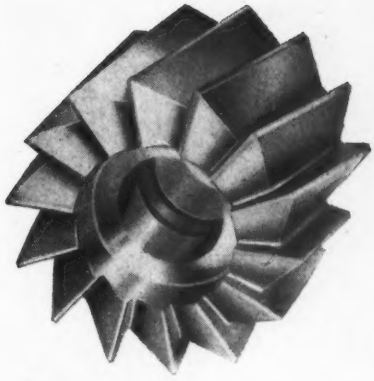

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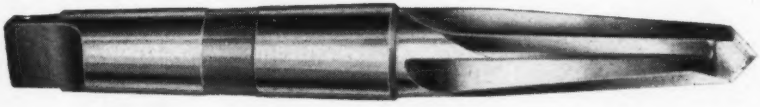

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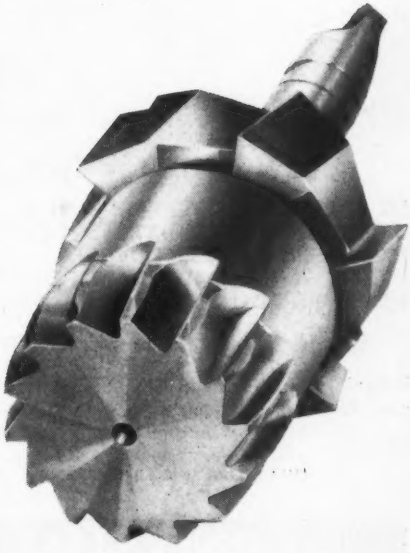

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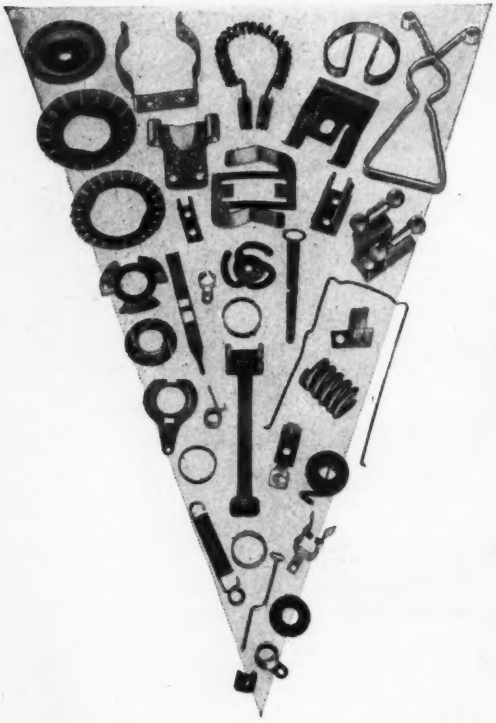

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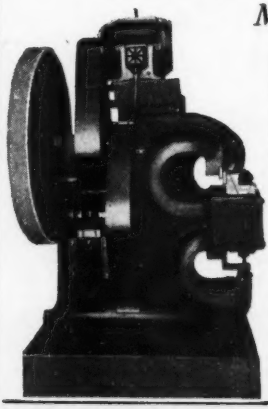

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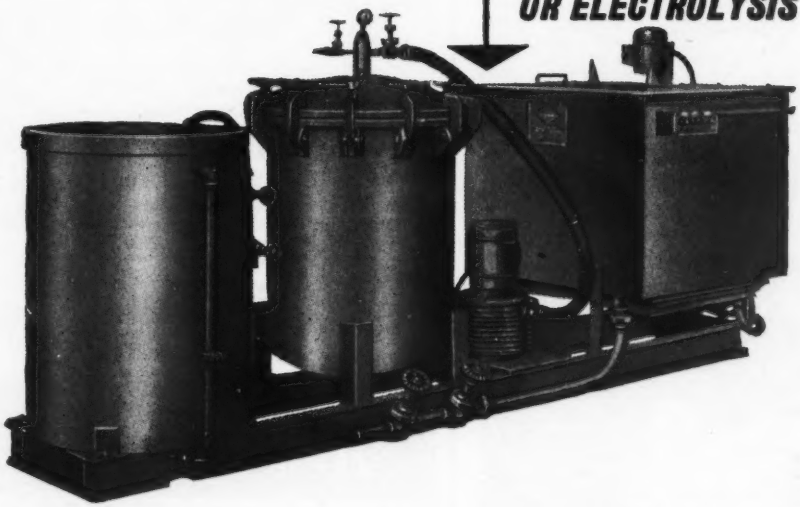

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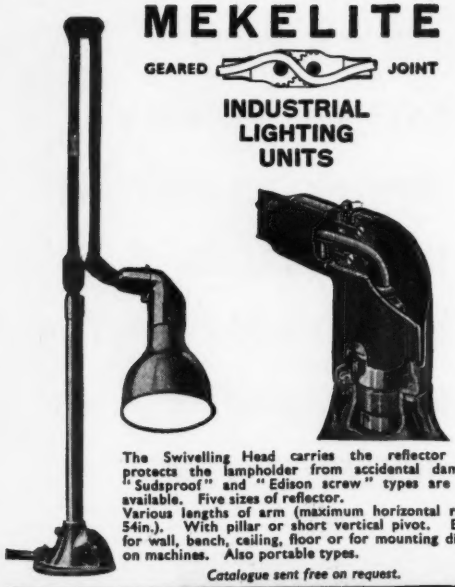

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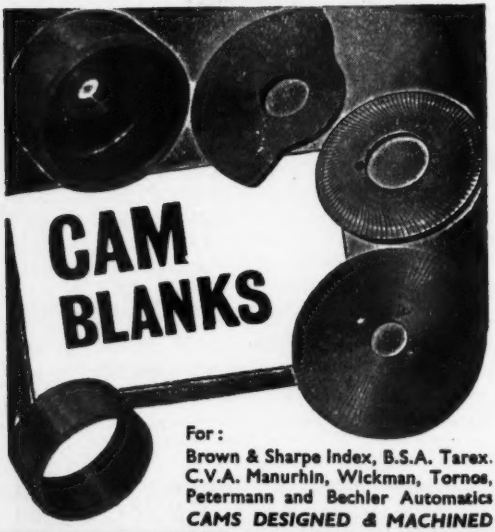

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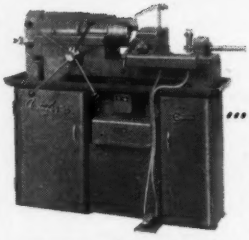

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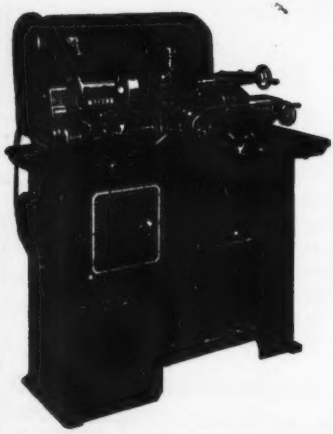

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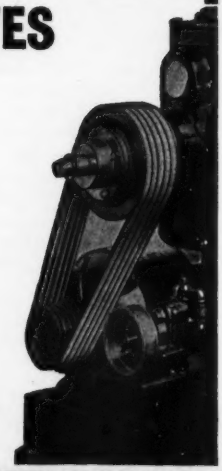

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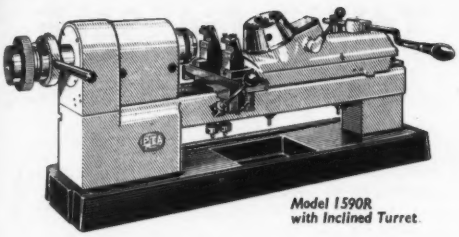

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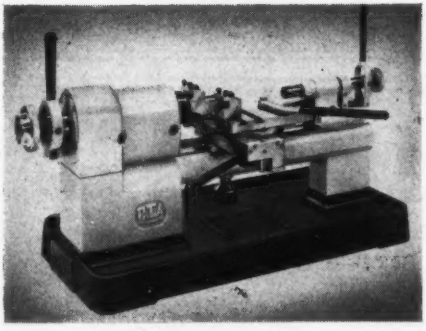

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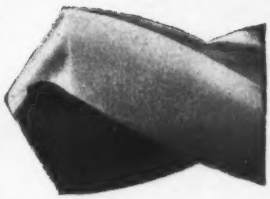

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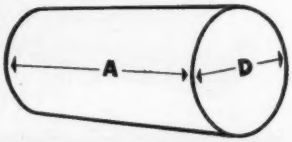

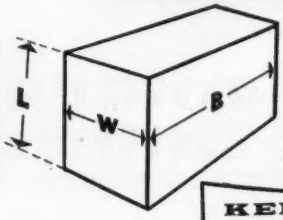

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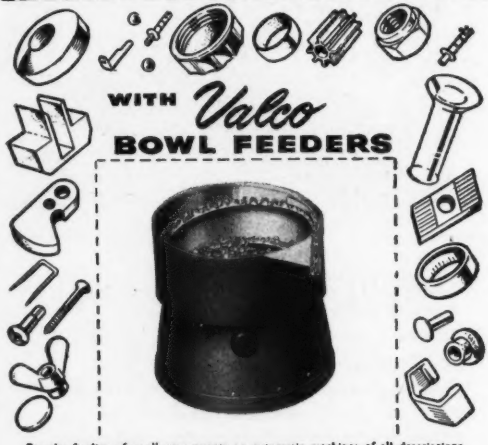

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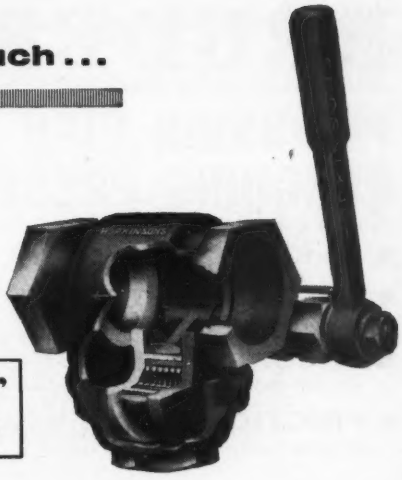

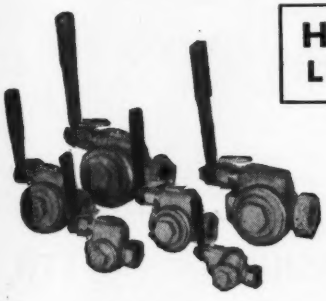

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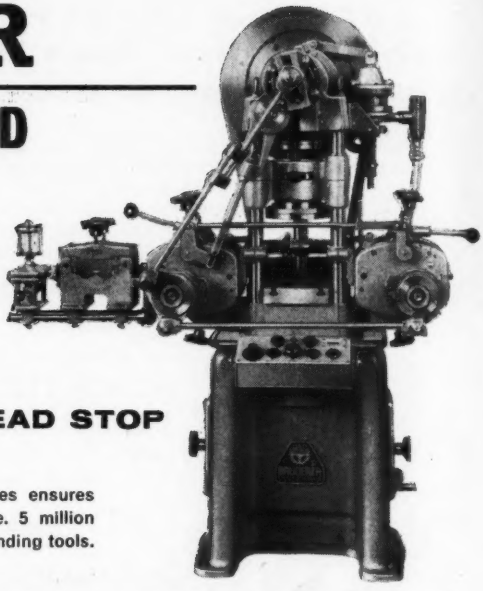

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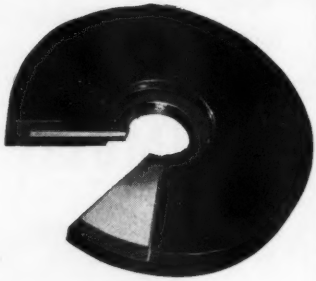

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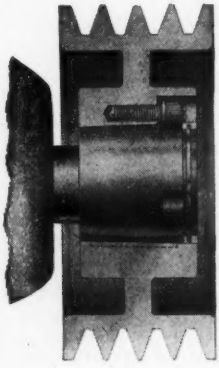

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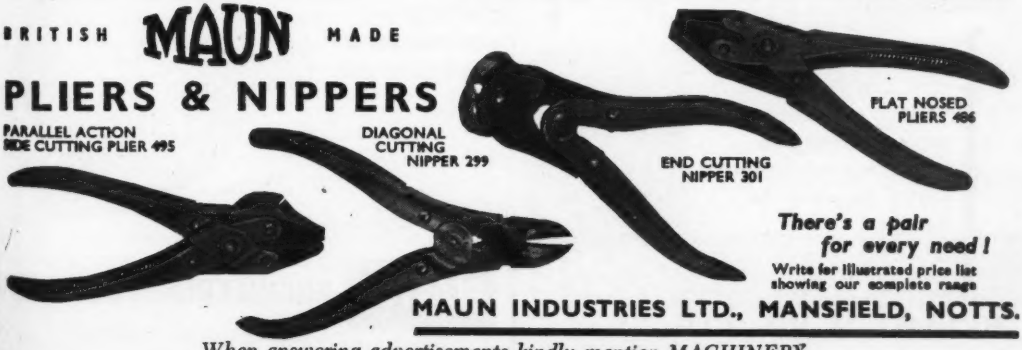

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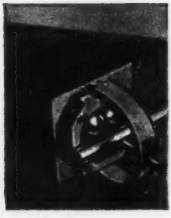

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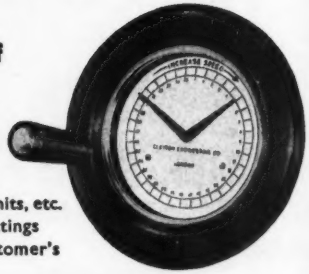

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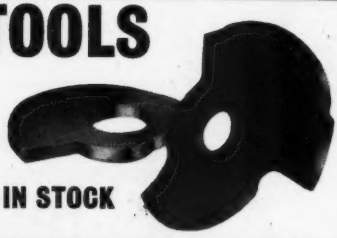

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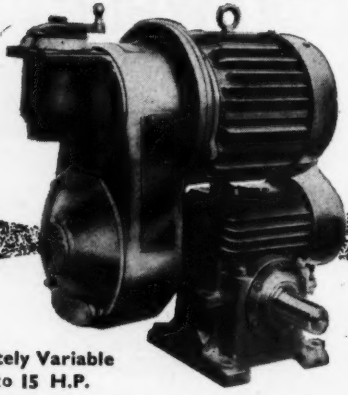

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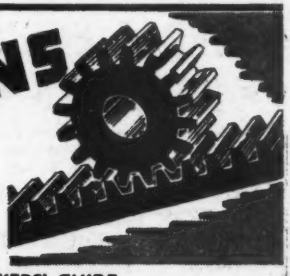
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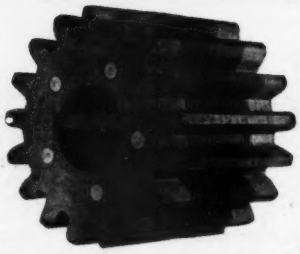

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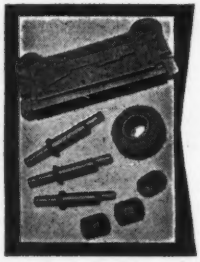

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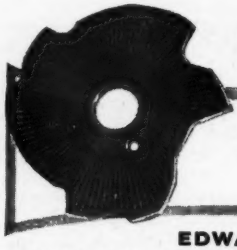

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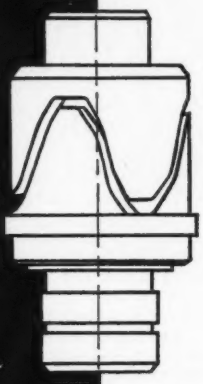

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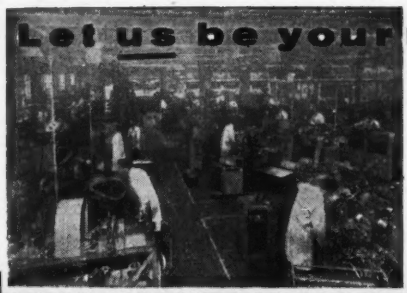

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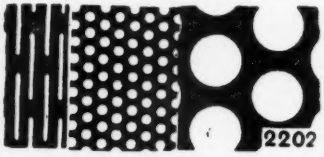

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COLCHESTER "Triumph," 7in. × 48in. Gap S.S. & S.C.
LE BLOND 15RP S. & S., 15in. × 24in.
CARDIFF S.S. & S.C. 8¼in. × 48in. "Senior." 1952 M/c.
CRAVEN 36in. Swing × 12ft. Between S.S. & S.C.
SMART & BROWN 4in. × 18in. S.S. & S.C.
LANG 36in. Surfacing and Boring.
ACME No. 5W Capstan, chuck machine.
RYDERMATIC No. 12 Multi-Tool.
D.S.G. 13Z Minor S.S. & S.C.
WILLSON 6½in. × 36in. Gap Bed S.S. & S.C.

CAPSTANS AND AUTOS

WARD No. 7 Capstan, chucker.
HERBERT 4B D/L chuck and bar feed.
HERBERT 2S air-operated chucker.
TAYLOR No. 1263 Capstan, ¼in. cap.

DRILLS

FOSDICK 4 BM. 3 spin. H/Sp.
CORONA 3M Pillar, 1½in. cap.
KITCHEN & WADE 2ft. 6in. Radial, 2in. capacity.
CORONA Model 9FX Super High Speed Bench.
CORONA Model 12AX Bench, ⅞in. cap.
BRISDON Model 52 Pillar, ¾in. cap.

GRINDERS

KEIGHLEY KN Internal.
GRAND RAPIDS No. 36 Hyd. Hor. Spin. Surface.
HERBERT JUNIOR Surface, 10in. × 6in. × 9in.
BROWN & SHARPE No. 5 Surface.
BROWN & SHARPE No. 23 Plain, cap. 10in. × 48in.
BROWN & SHARPE No. 2 Surface, cap. 6in. × 18in.
SMART & BROWN Internal, 1½in. cap.
BROWN & SHARPE No. 5, 3in. × 18in. Plain.
BALLINGER 10/24 "Versatile" Abrasive Cutting-off Machine.
NEWALL Model L.U. 10in. × 36in. Hyd. Universal.
B.S.A. LANDIS Type C 6in. × 18in. Hyd. Plain.
SNOW Mod. O.S.72 Surface, cap. 15in. × 72in.
CHURCHILL Mod. H.C.B. Internal Auto Size.
HAHN & KOLB Hyd. Disc Lapping M/c.
JACKMAN No. 22 Disc, 18in. dia.
LUMSDEN Mod. 12M. Tool, 14in. × 2 wheel.

MILLERS—Vertical

REED PRENTICE Mod. 3VG, table 38in. × 10½in.
CINCINNATI Model O8 Production.
KENDALL & GENT Duplex Profile, table 18in. × 15in.

MILLERS—Horizontal

CINCINNATI Mod. O8 Plain Automatic.
BROWN & SHARPE No. 000 Plain Auto Miller.
BROWN & SHARPE No. 2 Universal, light type.
RICHMOND 2HS Plain, table 35in. × 9in.
ARCHDALE 20in., table 40in. × 10in.
ASQUITH H.K.1 Duplex Keyway, table 43in. × 10in.
CINCINNATI Mod. O.K. Prod., table 34in. × 12in.
ARCHDALE 14in. Plain, table 27in. × 8in.
ARCHDALE 28in. Plain, table 49in. × 13in.

BORING MACHINE

KEARNS Mod. O.C. Horizontal, 3in. dia. spindle.

SAWING MACHINES

EHJ No. 13 Filing and Sawing.

SHAPERS

TOWN 14in.
HERBERT N.D. 20in.
ORMEROD 14in.

GEAR CUTTER

MAXICUT Gear Shaper, Mod. No. 2.

MISCELLANEOUS

T.T. & H. Javelin Etchers, Multi-heads (3 m/cs.).
HEAP 2in. Screwing Machine.

Classified Advertisements (*PLANT FOR SALE, contd.*)

Newman

AUTOMATICS

BULLARD Multi-Au-Matic 7in. 8 spindle.
BULLARD Multi-Au-Matic 12in. 6 spindle.

BORING MACHINES

KEARNS No. 2 Horizontal Boring and Facing Machine, 3in. dia. travelling spindle.
KEARNS Model OC Horizontal Boring Machine, 3in. dia. travelling spindle.
KEARNS No. 4 Horizontal Boring and Facing Machine, 4in. diameter travelling spindle.
WEBSTER & BENNETT Vertical Boring Machine, table 50in. diameter.
RICHARDS Type PRT Horizontal Floor Boring Machine, 3½in. travelling spindle, 28in. diameter facing head.
GIDDINGS & LEWIS No. 45 Horizontal Boring Machine, 5in. diameter travelling spindle.

CAPSTAN AND CENTRE LATHES

CHURCHILL-REDMAN Model 13NM Heavy-Duty S.S. & S.C. Gap Bed Centre Lathe, 15in. centre height × 72in. between centres. Swing in gap 50in.
MITCHELL Model DM10 S.S. & S.C. Gap Bed Centre Lathe, 10½in. centre height × 7ft. 5in. between centres. (NEW.)
OLDFIELD & SCHOFIELD Surfacing and Boring Lathe, 10½in. centre height.
WARD 7B Combination Turret Lathe.
NILES Heavy Duty Centre Lathe, S.S. & S.C. 17in. centre height × 28ft. between centres.
U.L.R.O. Heavy Duty Centre Lathe, 16in. centre height × 30ft. between centres.

DRILLING MACHINES

HETTNER Radial Drilling Machine, 10ft. elevating arm.

GEAR MACHINES

ORCUTT Model HM24 Hydraulic Interna Gear Grinder.
GLEASON 3in. Straight Bevel Gear Generator

GRINDING MACHINES

CHURCHILL Plain Cylindrical Grinding Machine, 26in. swing × 84in. between centres (1951).
LANDIS Type C Plain Hydraulic Cylindrical Grinding Machine, 6in. swing × 18in. between centres.
LANDIS Plain Hydraulic Cylindrical Grinding Machine, 18in. swing × 72in. between centres.
ORCUTT Model HM24 Internal Spur Gear Grinding Machines.
CHURCHILL Plain Hydraulic Cylindrical Grinding Machine, 20in. swing × 72in. between centres.
BROWN & SHARPE Plain Cylindrical Grinding Machine, 10in. swing × 36in. between centres

MILLING MACHINES

CINCINNATI No. 3 High Speed Dial Type Vertical Milling Machine (1950).
CINCINNATI Model 5/72 Plain Hydromatic Milling Machine, table 91in. × 22in. (1952).
CINCINNATI No. 2L Plain Horizontal Milling Machine, table 52in. × 10in.
CINCINNATI No. 1M Vertical Milling Machine.
CINCINNATI No. 4 Dial Type Horizontal Milling Machine.
GRAFFENSTADEN Model F1101 Plain Horizontal Milling Machine, table 52in. × 10in.
PRATT & WHITNEY Model BL3620 3-spindle "Keller" Die Sinking Machine.
CENTEC Model 3R Automatic Production Milling Machine, table 25in. × 16in.

MISCELLANEOUS

LANGE & GAILEN 28in. stroke Double Headed Hydraulic Shaping Machine.
TAYLOR & CHALLEN Double Sided 50-ton Geared Power Press, 10in. stroke.

NEWMAN INDUSTRIES LIMITED,

Machite Tool Division: YATE, BRISTOL

Tel.: Chipping Sodbury 3311. Telex. 44121. Cables: "Dynamo Yate."

London Office: Terminal House, Grosvenor Gardens, S.W.1. Tel.: Sloane 8206. Telex. 23289.

One Secondhand Scrivener No. 1

Centreless Grinding Machine, maximum capacity 1¼in. diameter with Plunge Feed. Hand Operated. Motorised 400-440/3/50.

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75-ton Daniels Downstroke Hydraulic Press.

Ram 8in. dia., 12in. stroke. Max. daylight 24in. Platens 17½in. × 14½in. Two 2½in. pushback rams. Motorised pump unit.—LEE & HUNT, LTD., Crocus Street, Nottingham. Tel.: 84246.

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BENNIE 4ft. by ¼in. Bending Rolls.
BROADBENT Lathe 12½in. by 6ft. 6in.
WILSON Lathe 8in. by 3ft. 0in.
RHODES 6ft. by ¼in. Guillotine.
FACEPLATE Lathe 80in. swing.
RICHARDS No. 1, 2 and 4 Horiz. Borers.
RICHARDS 5ft. Double Column Vert. Borer.

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SYLVESTER GARDENS,
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Cincinnati No. 3 Vertical Milling

Machine. Speed Range 18-1,300 r.p.m. Dial Type.

Further details from:—
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Alba 24in. Shaper. Ormerod

18in. Shaper.—C. DUGARD, LTD. Denmark Villas, Hove 32471

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Used **PRECIMAX** Type UPJ12/72 Hydraulic Universal Cylindrical Grinding Machine with variable speed workhead and electrics to suit 400/3/50.
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HERBERT No. 12 Heavy Duty Combination Turret Lathe. Full chucking equipment. 400/3/50.
TOWN 28in. Vertical Spindle Drilling Machine. Compound table. 400/3/50.
K. & W. 33in. Sensitive Radial Drilling Machine. Swing-aside table, swing-aside arm. 400/3/50.
JONES & SHIPMAN 20in. Vertical Drilling Machine. No. 4 Morse Taper. Power feed. 400/3/50.
KEARNS No. 2 Standard Horizontal Boring Machine with facing head and sliding spindle. 400/3/50.
SNOW T20 Table Surface Grinding Machine.
ARCHDALE 28in. Horizontal Manufacturing Milling Machine, with power and rapid feeds. Table size 49in. × 30in. 400/3/50.
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GRINDERS

JONES & SHIPMAN 540 Surface Grinder.
ROBOT 6in. × 18in. Surface Grinder.
NEWMAN 10in. × 24in. Universal Grinder.
BROWN & SHARPE No. 2 Surface Grinder.
HORTSMAN Thread Grinder, capacity 5in. dia. × 9in. b.c.
BROWN & SHARPE No. 5 Cylindrical Grinder.
FRITZ WERNER Model 270A Cylindrical Grinders, 3½in. × 7in. b.c.
BROWN & SHARPE No. 13 Universal Grinder.
BRYANT No. 5 Heavy Duty Internal Grinder.
BENTLEY Form Cutter Grinder.

LATHES, CAPSTANS

D.S.G. 8½in. × 48in. Gap Bed, 19-418 r.p.m.
D.S.G. 8½in. × 30in., 11-490 r.p.m.
HOLBROOK 8in. × 36in., 11-400 r.p.m.
COLCHESTER MASTER 6½in. × 36in. Ainjest Screwing Attachment.
LE BLOND "Regal" 7in. × 40in., 25-500 r.p.m.
EMPIRE 6½in. × 40in. Lathe.
SOUTHBEND 5in. × 24in. Bench Lathe.
BOYES & EMMS S.S. & S.C. Lathe, centre height 16in. × 7ft. 6in.
ROLLO 6½in. Centre Lathe.
HENDY 13in. × 30in. S.C. Lathe.
RIVET 4in. × 18in. b.c. Precision Lathe.
LE BLOND 14in. × 24in. S.C. Lathe.
WARNER & SWASEY No. 3 Capstan.

MILLERS

CINCINNATI 8in. × 18in. Tool and Die Miller.
EDGWICK No. 2 Universal, 46in. × 11in. table, 24-405 r.p.m. Vertical Attachment Dividing Head.
TRIDENT Vertical, table 30in. × 8in., 75-750 r.p.m.
CINCINNATI 1-18 Production Miller.
KENDALL & GENT Vertical Miller, table 69in. × 10in., speeds 20-300, rapid traverses.
SCHIESS DEFRIES Vertical Keyseater.
MAMMUT 10in. × 23in. Table Horizontal Mill, hand lever operated.
FRITZ WERNER 10in. × 34in. Horizontal Mill.
BROWN & SHARPE No. 2 11in. × 49in. Horizontal Mill, speeds 15-376. Feeds 3/10-15 I.P.M.

PRESSES, SHAPERS, PLANERS AND HOBBERS

BUTLER 14in. Production Slotter.
INVICTA 5m. Shaper.
ORMEROD 8in. Toolroom Slotter.
CHURCHILL-REDMAN 32in. Stroke Heavy Duty Shaper. Excellent condition.
ESSEX No. 32 Punch Shaper.
30-ton **RASKIN** Double Sided Double Geared Drawing Press. Area 20in. × 23in. Draw 4¾in.
New **POREBA** Model HDA.80 Planer, capacity 10ft. × 32in. × 30in. table, drive by Heid gearbox.
DOWDING V8 Gear Hobber.

DRILLS

POLLARD 4-spindle Pedestal Drill, 2-2MT 2-3MT.
POLLARD 3-spindle Pedestal Drill, 3MT, 110-1,455 r.p.m. Power Feed.
POLLARD 13 AX Pedestal Drill.
PROGRESS 4E Pillar Drill.
TAUCO ½in. Bench Drill.
BOLEY Multi Drill VB 10in.
CORONA 13in. 2AP Sensitive Pedestal Drill.
CORONA 20in. Pedestal Drill.
15HEF 4 Spindle Drill.

MISCELLANEOUS

CANNING Double Ended and Centreless Polishing Machines.

Classified Advertisements (*PLANT FOR SALE, contd.*)

K·E·N·T

AUTOMATICS

C.V.A. No. 26. 1960 Machine.
C.V.A. No. 12. 1960 Machine.
C.V.A. No. 8. 1950.
B.S.A. ⅜in.

LATHES

Broadbent 14in. × 7ft., unused.
Sicmatic 14in. × 27in. Hyd. Lathe. 1960.
D.S. & G. 18in. × 12ft. S. & S.
Betts Bridgeford 15in. × 18ft.
Lang 6½in. × 3ft. S.S. & S.C.
Holbrook 6½in. × 4ft. Gap bed.

MILLING MACHINES

Sant Andrea U.F.O.3 Hor.
57in. × 14in., as new.
Archdale 20in. Hor. Rapid.
Reinecker Vert. 52in. × 24in. with built in cir. table, 30in.
Jason Vert. 48in. × 12in. Sw. and Sl.
Herbert 15s Vert. 48in. × 12in.
Adams No. 5 Thread Mill.

CAPSTANS AND TURRETS

Minganti 1a Turret, 2½in. Bar.
Gisholt No. 3 Capstan.
Warner & Swasey No. 3 Capstan.
Ward No. 2a Capstan Lathe.
Herbert 1S Capstan Lathe.
Murad 3Q Capstan Lathe.

MISCELLANEOUS

Churchill NB 18in. × 6in. Surface Grinder
B. & S. No. 2 Surface Grinder.
Excel No. 1 Surface Grinder.
C.V.A. 10 Die Press.
Maiden Bar-ending Machine.
Raboma 4ft. 6in. Radial Drill.
K. & W. 2in. Pillar Drill.
Granor 26in. H.D. Shaper.
Hutto Vert. Honer.
3 Ton Hi-ton Press.
S. Platt 3in. × 14g. Tube Roller.
Edwards 4ft. × ¼in. Power Guillotine.

Many other machines in stock.

All motorised 440/3/50.

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Holroyd Rivet Punching Machine for sale. Motorised, toggle action, with power lift to table. Capacity ½in. diameter rivets. Gap, 5in. Table 13½in. × 8in. Electrics for 350-440/3/50.—Photo. etc., from F. J. EDWARDS LIMITED, 359, Euston Road, London, N.W.1, or 41, Water Street, Birmingham, 3.

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Our stock includes Myford MG12 Grinders, Eagle Surface Grinders, Myford Lathes, Boxford AUD 4½in. Lathes, Willson 6½in. Lathes, Pacera Drilling Machines from ½in. to 1½in. capacity, Startrite Bandsaws, Kennedy, Rapidor and Q. & S. Hacksaw Machines, Centec Milling Machines, 18in. Alba Shapers, Vices and Rotary Tables of all types.

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RYDER Verticalauto, capacity 16in. swing × 8in., 6 spindles.

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RICHARDS 36in. Vertical Boring Mill, complete with side head.

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BULLARD 26in. Vertical Boring Mill.

KITCHEN & WADE Vertical Fine Boring Machine. 14in. stroke. Compound table.

SCHIESS Vertical Boring Mill, 39in. dia. of table. Maximum swing 48in. S.C.M.D. 35 h.p., 400/3/50.

DRILLING MACHINE

ARCHDALE 8-Spindle Hydraulic Vertical Drilling Machine.

GRINDING MACHINES

HEALD No. 172 Gap Bed Internal Grinding Machine, maximum diameter of component 36in.

BILLETER Hydraulic Open-side Slideway Grinding Machine, capacity 47in. × 12in.

LATHES

NOBLE & LUND Heavy Duty Centre Lathe, 22in. centre height × 29ft. between centres Max. swing over saddle 33in. dia.

HARVEY Heavy Duty Centre Lathe, 42½in. centre height × 52ft. between centres. Max. swing over saddles 65in. dia.

MILLING MACHINE

COLLET & ENGLEHARDT Keller Type Die Sinking Machine. Model FKf80, capacity 60in. × 30in.

PLANING MACHINES

CLEVELAND Openside Planing Machine, capacity 10ft. × 2ft. 6in.

CINCINNATI Planing Machine, capacity 8ft. × 2ft. 6in.

MISCELLANEOUS MACHINES

CLIFTON & BAIRD Horizontal Cold Sawing Machine, 30in. dia. Saw. Maximum capacity 22in. × 7in R.S.J.

Hydraulic Vertical Internal Honing Machine (manufactured by **PETER WOLTERS**), Capacity 0.2in. to 2in.

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Further details from

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BRANDON ROAD WORKS, BRANDON ROAD, COVENTRY.

'Phone:

WALSGRAVE-ON-SOWE 2253 (6 lines).

AUTOS

CONOMATIC 1¼in. 8 spindle. Type W.W.
WICKMAN 1¼in. 5 spindle. 1941 machine.
WICKMAN 1¼in. 5 spindle. 1941 machine.
WICKMAN 6in. 5 spindle Chucker.

DRILLING

ASQUITH 4ft. 6in. O.D.1 Radial Drill.
ASQUITH 4ft. O.D.1 Radial Drill.
PROGRESS 5E. Round table.

GEAR SHAPING

Model 61 **FELLOWS** Gear Shaper. Straight spur. 35in. dia. × 5in. face width.

LATHES

WARNER & SWASEY No. 2A Long Bed.
SOUTHBEND 16in.
EDGWICK 7in.
DEAN, SMITH & GRACE. Height of centres 7in.
MONARCH 22M S.S. Taper Turning Lathe.
WARD 10 Combination Turret Lathe.

MILLING

20in. **ARCHDALE** Plain Mill. Rapid.
28in. **ARCHDALE** Rapid All Ways.
18in. **EDGWICK** Production Mill.
CINCINNATI No. 5 High Power Plain Hor. 1942 machine.
KENDALL & GENT C.V.M.40.
KENDALL & GENT C.V.M.25 Vertical Mill.

SHAPING GUILLOTINES

EDWARDS 6ft. × ⅛in. Overcrank.
EDWARDS 8ft. × ¼in. Overcrank.

FOLDERS

MORGAN 6ft. × 14g. Universal.
EDWARDS 6ft. × ¼in. Swing beam, hand geared.
EDWARDS 6ft. × 14g. Open ended.
EDWARDS 6ft. × 10g. Open ended.

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6ft. × 12g. between columns. Delivery 10 weeks.
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All machines motorised 400-440/3/50.

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HERBERT No. 4 Capstan, steel tray model, 400/3/50. £195.
JONES & SHIPMAN Pillar Drill, No. 4 Morse Taper, 26in. table, power feeds, motorised a.c. £110.
PROGRESS Pillar Drill, No. 3 Morse Taper, 400/3/50. £75.
EDWARDS 48in. × 14 Gauge Power Guillotine, 400/3/50. £250.
EDWARDS 42in. Treadle Guillotine, 18 Gauge. £47 10s. 0d.

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Single Spindle
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BROWN & SHARPE 2G. (Choice of two.)
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B.S.A. GRIDLEY 6 sp. 1in.
GRIDLEY 6 sp. $\frac{9}{16}$in. (Choice of two.)
B.S.A. GRIDLEY 4 sp. $\frac{7}{8}$in. (Choice of three.)
CONOMATIC 6 sp. 1¼in.
GREENLEE 6 sp. 1⅝in.

CAPSTAN, COMB. TURRET LATHES

WARD No. 7 Covered bedtype, WTE series and wartime built. (Choice of two.)
GISHOLT No. 5 Chucker, Power Feeds, 39 to 500 r.p.m.
WARD 1A Hand Operated Collet Chuck. Speeds 75 to 4,130 r.p.m.
WARD 10B Comb. Power feed to turret, Ball chuck, Bar feed equipment. Rebuilt.
LIBBY IH5 Comb. Hole in spindle 5¼in. dia. Power and rapid feeds to saddle turret and cross slide.

GRINDERS

CHURCHILL 12in. by 50in. Hydr. Universal, internal spindle.
JONES & SHIPMAN 8in. by 16in. Universal, internal spindle.
CHURCHILL 20in. by 96in. Hyd. Cylindrical Serial Number 20468. For delivery August.
MYFORD 5in. by 9in. MG9 Cylindrical
CHURCHILL 42in. swing 120in. bore internal
HEALD No. 81 Internal Gagematic Automatic Chuck Grinder. Serial Number 18601.
HEALD Internal Model 81

MILLING MACHINES

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ARCHDALE 20in. Plain, Rapid Production.
CINCINNATI No. 3, Vert. Dial Type, table 62½in. by 15½in.; 18 to 450 r.p.m.
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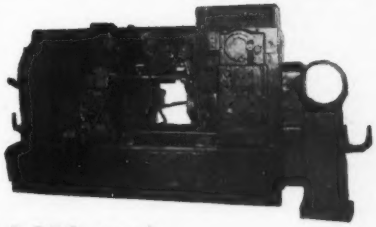

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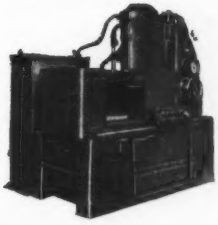
WICKMAN 5 Spindle 1⅜in. Cap. Bar Automatics. (Selection of several.)



£2,750
LUMSDEN 24in. dia. Retractable Rotary Table Surface Grinder Model 90RT. With Chuck.

£1,100
CARDIFF 8¼in. by 48in. S.S. & S.C. Gap Bed; 20 to 970 r.p.m.

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ALL MACHINES MOTORISED FOR 3 PHASE SUPPLY UNLESS OTHERWISE STATED

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POTTER & JOHNSON 4D.
BORERS (Horizontal)
KEARNS No. 2
BROACHING
AMERICAN Model H2, stroke 3pin.
CAPSTANS
HERBERT 2S.
MURAD ¾in.
HERBERT 4B.
DRILLS
DENBIGH 24in. B.G.
HERBERT " C " Power Feed.
CORONA No. 21 AR, No. 3 M.T.
JONES & SHIPMAN 816, ⅞in. cap.
CORONA IAX, No. 1 Morse Taper.
CORONA 15HF, ⅞in. cap.
LELAND GIFFORD 2-sp., No. 2 M.T.
HERBERT Type B. Single Spindle, ½in.
CORONA 6MX Cluster Type.
HERBERT Type H, ¼in. dqp.
CORONA 12AX, ⅝in. cap.
ENGRAVERS
LIENHARD 3 Dimensional (New).
LIENHARD No. 1H.
HUPFIELD Router.
T.T. & H. Type C, C.B. and M.A.
T.T.& H. Multi Etcher.
FILING AND SAWING MACHINES
JONES No. 13 Bandsaw.
Wickstead No. 1 Hacksaw.
RAPIDOR 6in. Hacksaw.
RAPIDOR Filing.
FOLDERS
Sheet Edging, 30in. × 22g.
GEAR CUTTERS
SAFAG Pinion.
MAXICUT 7in. × 2in. × 6 D.P.
PETERMAN No. 1 and 2.
GRINDERS (Surface)
CHURCHILL RBY 24in. ring.
CAPCO No. 2, 14in. × 6in.
CHURCHILL OSB 8in. × 30in.
LUMSDEN Vert. 210 XXM.
SNOW Table, 20in.
ABRASIVE No. 34 Vertical Spindle.
ABRASIVE No. 1½in. hand.
GRINDERS (Internal)
BRYANT 16/38 and 5.
GRINDERS (Cylindrical)
CHURCHILL 6 × 36in. B.Y.
CHURCHILL PBH 12 × 36in. Uni.
NEWALL 6 × 18. Model XL.
PRECIMAX MPB 10 × 48.
GRINDERS (Miscellaneous)
FIRTH BROWN ½-½in. Drill.
JONES & SHIPMAN, 10in. × 27in., T. & C.
J. & S. Drill, ½in. to ¾in.
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Further details from:—
C. & G. OLDFIELD, LTD.,
15, Abercorn Street,
PAISLEY.

C.V.A. Autos. No. 8, 3rd Slide Slotting Bar Feed, little used (3).
HERBERT 4 Senior Capstan, well equipped.
HERBERT 4 Capstan, 750 r.p.m., well equipped.
HERBERT 4 Capstan, 511 r.p.m., steel trade, well equipped.
WARD 2A Capstan.
MYFORD SUPER 7 Lathe, as new.
SNOW P., 24 × 8in. Hydraulic Surface Grinder.
NEWALL 10 × 24 Hydraulic Plain Cylindrical Grinder, built 1957 but only used for 6 months.
ARCHDALE Manufacturing type Horizontal Milling Machine, built 1951, automatic traverses.
CINCINNATI O8 Vertical Milling Machine.
CINCINNATI O8 Horizontal Milling Machine.
HERBERT No. 33 Horizontal Milling Machine, 36 × 9 working surface.
ASQUITH OD 2 8ft. Radial Drilling Machine, speeds to 830 r.p.m., No. 5 M.T.
CLEVELAND 130 Gear Hobbers (2).
ATLANTIC Jig Borer, equivalent to Newall No. 1 machine; only 2 years old, very little used.
NOBLE & LUND 20/22 Hydraulic Fluifeed, cold saw.

STAINES MACHINE TOOL CO., LTD.,
THE CAUSEWAY, STAINES.
Telephone: Staines 52647.

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Virtually New British Built
KEARNEY & TRECKER
MILWAUKEE Horizontal Milling Machines at prices much lower than cost.

MODEL 2CE Table Size 52in. × 12in. table travel 28in., spindle speeds (16) 25-1300 r.p.m.

MODEL 3CE Table Size 67in. × 15in., table travel 34in. spindle speeds (16) 25-1300 r.p.m.

These machines are available immediately from our London showrooms and are in immaculate condition, indistinguishable from new.

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HAVE MACHINE TOOLS AND EQUIPMENT FOR SALE INCLUDING THE FOLLOWING:-

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OOG BROWN & SHARPE S.S.

PITTLER 12mm. Swiss type.

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⅞in. **B.S.A. ACME GRIDLEY** RA6 spindle. Screwing spindle, Collets and Tooling. 3 available. 1944–1948.

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CINCINNATI, No. 2 Dial Type. Medium speed horizontal.

CINCINNATI 08 Vertical.

C.V.A., Model 79, Vertical Mill.

THIEL, Model 58 Tool Room Mill.

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NEWALL, Model No. 1.

WICKMAN HORSTMAN, Model No. 1 and No. 2.

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ESSEX Punch Shaper Microscope and equipment.

ROCKFORD 28in. Hydraulic Universal.

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WARD No. 7 Capstan.

WARD No. 7 Combination. Serial K. & L.

WARD OE. Capstan ¼in. Bar.

HERBERT No. 9 Combination.

HERBERT No. 4.

HERBERT No. 2S & 1S.

HERBERT No. 0.

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GISHOLT No. 4 A.G.H. Capstan.

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CORONA 12AX 2-spindle Drill.

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CHURCHILL, Models HBA, HBB, HBC and HBY.

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CAPSTAN LATHES

WARD No. 7 Chucking, covered bed.

TURRET LATHES

WARD No. 16, covered bed, 8¼in. spindle, 32in. 4-jaw chuck, rapid and power feeds to saddle, cross slide and turret, power rotating turret, spindle speeds 7-225 r.p.m., 50 h.p. motor.

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WARD No. 10B, covered bed. 4¼in. spindle power rotating turret, power and rapid feeds to turret only, collet head and bar feed.

DRILLING MACHINES

ASQUITH O.D.1 5ft. Radial, with loose box table.

AVEY 2-spindle drill, pedestal base, ½in. capacity.

HORIZONTAL MILLERS

SUNSTRAND No. 2 Electro Mill, auto. cycle, 12in. by 54in. table.

HERBERT No. 3ND. Plain.

EDGWICK No. 2, 11in. by 42in. table, No. 40 steep taper.

JONES & SHIPMAN duplex slot miller. Hydraulic feed.

VERTICAL MILLERS

WADKIN high speed for light alloy, 16in. by 40in. table.

GRINDING MACHINES

B.S.A.-Landis, 6in. by 18in. plain hydraulic cylindrical grinder.

BROWN & SHARPE No. 2 Surface Grinder, 18in. by 6in.

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HERBERT No. 2 Flash Tapper, ½in. capacity.

All machines motorised 400/3/50 unless otherwise stated.

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Bryant No. 24-36 Hydraulic Internal Grinder complete with Hydraulic Wheel Dressing device, Spindle, etc.

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WEBSTER & BENNETT 4ft. D Type Vertical Borer. Speeds 5 to 109 r.p.m.

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Double Ended Angle Cropping Machine. Cap. up to 6in. × ½in. angles.

DRILLING MACHINES

POLLARD 13in. Pillar Drill, No. 2 Morse Taper. R. & F. Table 11in. × 11in.

ARCHDALE 28in. H/Duty Pillar Drill, No. 4 Morse Taper. R. & F. Table Elc. Suds.

GRINDING MACHINES

New **NORTON** 10in., 12in., 14in., 16in. and 20in. D/E. Tool Grinders.

ABRASIVE No. 34 24in. × 8in. Vertical Spindle Surface Grinder.

HAMMERS

MASSEY 5 cwt. Slide Type Pneumatic Hammer. 400/3/50.

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VAN NORMAN No. 26 Horizontal and Vertical Milling Machine. Slotting head.

MILWAUKEE 3.H Vertical Milling Machine.

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TAYLOR & CHALLEN "370" 20 Ton O/F Press.

TAYLOR & CHALLEN "845" Dial Feed Notching Press.

BRADLEY & TURTON No 3 Flypress.

SWEENEY & BLOCKSIDGE Bench Press. Cap. 3 tons.

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KENDALL & GENT 3in. Screwing Machine. Leadscrew Type.

POLISHING MACHINES

3 and 5 h.p. Double Ended Polishing Spindles.

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ORMEROD 12in. Stroke Slotting Machine. 27in. Rotary Table.

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THE
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SMART & BROWN 1½in. cap. Internal Grinder.
BRYANT 16-38A Hydraulic Internal Grinder.
CHURCHILL Model HBB automatic sizing traverse feed type internal Grinding Machine with spindles for combined hole and face grinding, max. swing 19in.
PRATT & WHITNEY 36in.×12in. Vertical Spindle Surface Grinder.
JACKMAN No. 28, 53in. Disc Grinder.
HUNT No. 3 Twist Drill Grinder, 3in. cap.
HUNT No. 1 Twist Drill Grinder, ½in. cap.
BANDFACERS 43in. × 6in., and 36in. × 4in. (New.)

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REED PRENTICE No. 2 V.G. Vertical Miller; table 20in. × 9in.; capacity 16in. × 11in. × 15in.
ARCHDALE 12in. light type high speed Vertical Milling Machine, table 17in. × 10in., 12in traverse, speed 235-1,500 r.p.m.
B.C.A. Precision Vertical Milling, Boring and Drilling Machine, 8in. dia. table.
HERBERT 46V Vertical Milling Machine; capacity 36in. × 13½in. × 22½in.; table 58in. × 15in.; power rapid all ways.
CURD NUBE 2-spindle Vertical Profile Miller; table 17¼in. × 14¼in.
MILWAUKEE 2K Universal Miller; table 56in. × 12in.; capacity 28in. × 10in. × 17in.; 15-1,500 r.p.m.
CINCINNATI No. 2 dial type Universal Miller, table 49in. × 12in.; capacity 28in. × 10in. × 18in.; 500 r.p.m.
VICTORIA U.1 Universal Miller, table 40in. × 11in., capacity 25in. × 8in. × 16in., speeds 31 to 1,010.
VICTORIA U.1 Universal Miller, table 40in. × 11in.; capacity 25in. × 8in. × 16in., speeds 31 to 1,010; with vertical milling attachment.
VICTORIA U. 2 Universal Milling Machine, table 45in. × 11in. with vertical milling attachment, slotting attachment and rotary table.
PROGRESS Universal Milling Machine, table 40in. × 10in., capacity 24in. × 9in. × 18in.
PEDERSEN Horizontal Miller; table 49in. × 10in.; capacity 24in. × 7½in. × 16in.
ADCOCK & SHIPLEY 1AD Horizontal Milling Machine; table 19in. × 7in.; capacity 10in. × 6in. × 10in.; speeds 50-2,500 r.p.m.
HERBERT No. 1 Horizontal Milling Machine; table 26in. × 8¼in.; capacity 10in. × 3¼in. × 7in.; speed 100-530 r.p.m.
MILWAUKEE 4K Horizontal Milling Machine, table 82in. × 18in., capacity 42in. × 14in. × 20in., power rapid traverses, speeds 13 to 1,300 r.p.m.
HOLROYD 12in. × 54in. Thread Milling Machine; 7in. spindle bore.
HOLROYD Thread Milling Machine, 6in. dia. capacity for internal and external work.
HOLROYD No. 2A Thread Milling Machine; capacity 4in. × 30in.
BECKER Automatic Milling Machine; table 23in. × 12in.; with auto cycle to table and spindle.
KENT-OWENS 1-14 Production Miller; table 32in. × 9in.; hydraulic feed and rapid traverses.
KENT-OWENS 1-8 Hydraulic Production Miller; table 25in. × 9in.; 100-1,335 r.p.m.
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REDMAN 12ft. × 3ft. 6in. × 3ft. Planer, two toolboxes.

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ASQUITH O.D.I. 6ft. Radial Drill. No. 5 M.T. Spindle. Speeds (12) 31-830 r.p.m. Loose Box Table. Suds.
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Reconditioned **CINCINNATI** No. 4 Horizontal Miller. Dial type. Speeds (21) 18-1,300 r.p.m. 16 feeds. Table size 86½in. by 16in. Power feeds in all directions.
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BEAVER MILLERS.
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COLCHESTER, CHIPMASTER, STUDENT & TRIUMPH LATHES.
SMART & BROWN 'A', '1024' Lathes, Toggle Presses and Screwing Machines.
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Herbert Carbicut Lathe, 16 spindle speeds 445 to 3,025 r.p.m. 3 feed changes 70, 105, 140. 1½in. dia. spindle bore. 5 h.p. motor. 400-440/3/50.—BOX C910, MACHINERY, Clifton House, Euston Road, N.W.1.

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WEBSTER & BENNETT 36in. Vertical Boring and Turning Machine. Table 31in. dia. Pentagon turret.
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SCRIVENER No. 2 Centreless Grinding Machine. 6in. width of wheel.
HERBERT Model OV Swivel Head Vertical Milling Machine. Speeds 250 to 2,000 r.p.m. Table 18in. × 5in. W.S.
TAYLOR & CHALLEN Model G.D.P. 3½ Double Action Press. 10in. punch stroke, 22in. between columns.

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Semi-Automatic Thread Milling Machine by Hanson Whitney. Capacity 4in. dia. × 9in. long. Collet capacity 2in. External cap. 4in. dia. max. with 2in. cutter. Internal cap. ¾in. dia. min. with ½in. cutter. Some equipment available.—BOX C931, MACHINERY, Clifton House, Euston Road, N.W.1.

Huller UG3 Tapping Machine, 1955. 400/3/50.—BOX C902, MACHINERY, Clifton House, Euston Road, N.W.1.

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KELLY 28in. Stroke Heavy Duty Shaping Machine with swivelling table. 400/3/50.
RUSSELL Saw Sharpening Machine, max. capacity 42in. diameter. 400/3/50.
ORMEROD 12in. Slotting Machine. 400/3/50

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EYRE STREET, SPRING HILL,
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Tel. EDGbaston 1118 & 1119. 'Grams: Capstan, Birmingham.

Pedersen Plain, Miller, All-geared, 400/3/50, power feeds all ways, switchgear. Ex. Cond. Also Adcock & Shipley 1AD, auto-cycle production mill. Ex. Cond.—C. L. THOMAS LTD., Stirling Road, Solihull. Tel.: 3075-6.

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Delapena Induction Heating Units. With Generators. 2 and 6 kVA. For hardening, brazing, etc.—WILCOX & CO., Barr Street, Birmingham 19. NORthern 1234/5.

Richards No. 2 PRT Horizontal Boring and Facing Machine complete Live Spindle.

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Further details from:—
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BROADBENT 6ft. 0in. Double Standard Vertical Boring and Turning Mill, max. height admitted cross rail 46in., max. dia. admitted 77in., speeds to table (12) 1.6-40 r.p.m., feeds (6) 6-144 c.p.i.
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MITCHELL OF HALIFAX 8½in. centres Gap Bed S.S. & S.C. Lathe, to admit 6ft. 6in. between centres, swing in gap 29½in. × 9½in., dia. of hollow spindle 2½in., 9 speeds 26-500 r.p.m.
VICTORIA Model U.2 Universal Milling Machine, table size 45in. × 11¼in., power traverses; 12 speeds 31-1,010 r.p.m.
DENBIGH Model DVSR4 Variable Speed Horizontal Milling Machine, table size 46in. × 10in., automatic longt. feed 36½in., 9 speeds 25-720 r.p.m.
DENBIGH Model D.4. Horizontal Milling Machine, table size overall 46in. × 10in., auto. longt. feed 37½in., 9 speeds 19-720 r.p.m.
PACERA Model MF5/Mk.2 1in. cap. Round Column Drilling Machine, 18in. swing, spindle bored No. 3 M.T., 8 speeds 80-1,500 r.p.m.
PROGRESS Model 3A Pillar Drilling Machine 1¼in. cap., spindle bored No. 3 M.T., 5 speeds 110-1,780 r.p.m., feed 0.004in./rev.
PACERA Model A.10 Articulated Radial Type Drilling Machine, ¾in. cap., spindle bored No. 2 M.T., 10 speeds 80-4,000 r.p.m., depth of throat 24in., working surface of table 24in. square.
TAYLOR-HOBSON Model D Pantograph Engraving Machine, size of table 15in. × 8in.
MAIDEN Model 4C/ST Threading Machine mounted on cabinet base, cap. 4in. pipes, 2in. bolts.
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All machines fitted with electrical equipment for 400-440/3/50 cycles supply.

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KENDALL & GENT Model A.V.M. Open Side Plano *MILLING MACHINE*. Table size 78in. × 30in. Longitudinal traverse 72in. Max. distance spindle to table 34in. 27 spindle speeds 26 to 1,390 r.p.m. Motor drive 400/3/50.
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CINCINNATI Model 4-36 Hydromatic *MILLING MACHINE*. Table size 18in. × 67in. 8 spindle speeds 20 to 150 r.p.m. through pick-off gears. 36in. hydraulic table traverse. Vertical adjustment of head 7in. Max. adjustment of quill 6in. Motor drive 415/3/50. Price: £1,500

CARTER & WRIGHT Dual Feed No. 3 Keyseating and Slot *DRILLING MACHINE*. Tee slotted table 32in. × 12in. Max. length of keyway cut 24in. Max. width of keyway cut 1¼in. 8 spindle speeds 160 to 650 r.p.m. Motor drive 400/3/50.
Price: £675

HERBERT No. 9 Combination Turret Lathe. 20in. swing over bed × 54in. spindle to turret. Spindle bored 4¼in. dia. 16 spindle speeds 14 to 400 r.p.m. Power feed to saddle and turret. Motor drive 400/3/50. Price: £575

ALBA Model 6S Crank *SHAPING MACHINE*. Max. length of stroke 24in. 6 ram speeds. Variable feeds to table. Working surface of box table 23in. × 13in. top face, 13½in. × 14in. side face. Motor drive 400/3/50. Price: £325

HERBERT Model 2D *CAPSTAN LATHE*. Spindle speeds 50 to 2,550 r.p.m. With collet chuck and bar feed mechanism. Motor drive 400-440/3/50. Price: £580

WALKER TURNER 30in. Light Type Radial *DRILLING MACHINE*, with swivelling head. ¼in. capacity. 8 spindle speeds. Working surface of table 18in. × 26in. Max. distance spindle to column 30in. Motor drive 400/3/50. Price: £160

KEARNS Model No. 2 Horizontal *BORING, FACING AND MILLING MACHINE*. 3in. dia. traversing spindle. 20in. dia. facing head. Spindle speeds 66 to 290 r.p.m. Main table 7ft. × 3ft. Auxiliary table 4ft. × 4ft. Machine has extended cross traverse to table with outrigger supports. Motor drive 400/3/50. Price: £3,050

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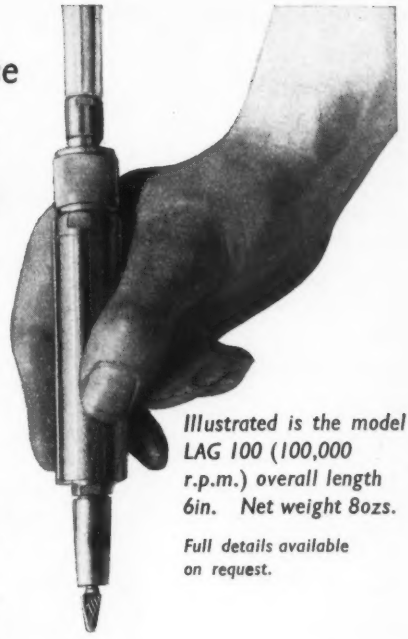

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INDEX TO ADVERTISERS

	PAGE
Abbey Heat Treatments Ltd.	148
A.B.M.T.M. Ltd.	25
Abwood Machine Tools Ltd.	7
Acbars Ltd.	105 & 161
Adams, Cyril & Co. Ltd.	16
Aircraft Unit Eng'g. Co.	152
Ajax Machine Tool Co. Ltd.	129
Alexander Bros.	151
Alleyne Foster Eng. Co. Ltd.	151
Allspeeds Ltd.	80
Almco Supersheen Division of G.B. Ltd.	45
Appleyard, S. & Co. Ltd.	132
Archdale, James & Co. Ltd.	42
Ashtead Engineering Co. Ltd.	150
Atkin, W. T. (Tottenham) Ltd.	154
Atlas Copco (Gt. Britain) Ltd.	26
Automation Limited	40
Avenue Engineering Co., The	150
Aylesbury Turned Parts (True Screws) Ltd.	152
Baker, Frank & Sons Ltd.	143
Barber & Colman Ltd.	*Inside Back Cover*
Beard & Fitch Ltd.	28
Bell, H. (Machine Tools) Ltd.	160, 169 & 176
Bellows-Valvair Ltd.	118
Benton Engineering Co. Ltd., The	150
B.H.P. Machine Tool Co.	44
Boneham & Turner Ltd.	116
Bosch Ltd.	24
Brasshouse, Peter Ltd.	141
Brayshaw Tools Ltd.	99
Bridges, G. F. Ltd.	145
British Laminated Brass Co. Ltd.	135
British Oxygen Co. Ltd.	63
British Ronceray Ltd.	133
Brockhouse, J. & Co. Ltd.	128
Brooke Tool Mnfg. Co. Ltd., The	59
Broom & Wade Ltd.	121
Brown, David Corporation (Sales) Ltd., The	79
Brown's Engineering Works	150
B.S.A. Tools Ltd.	97
Buck & Hickman Ltd.	4
Buck & Ryan Ltd.	135
Burdett, G. W. S. & Co. Ltd.	109
Burton, Griffiths & Co. Ltd.	97
Butcher, Henry & Co.	159
Butterworth British Automatic Machine Tool Co. Ltd.	115
Carborundum Co., Ltd., The	37
Carne, Rudolph & Co. Ltd.	52
Cashmore, John Ltd.	162
Catmur Machine Tool Corporation Ltd.	21
Centaur Tool Works	163, 169 & 173
Centec Machine Tools Ltd.	92
Chatwin, Thomas & Co.	110
Ching, Richard & Son Ltd.	156
Clarkson (Engineers) Ltd.	61
Clayton Eng'g. Co. Ltd.	144
Cohen, Geo. Sons & Co. Ltd.	174
Coventry Grinders Ltd.	155
Cox & Danks Ltd.	82
Crawford Collets Ltd.	6
Cross Manufacturing Co. (1938) Ltd.	136
Croydon Tool & Case Hardening Specialists Ltd.	149
Delancey Tool & Engineering Works Ltd.	151
De Roll, Louis Iron Works Ltd.	127
Desoutter Bros. Ltd.	30
Dimco (Gt. Britain) Ltd.	161
Donovan Electrical Co. Ltd., The	156
Douglas, A. Co. Ltd.	158 & 168
Dover Ltd.	116
Dowding & Doll Ltd.	23, 124 & 144
Dowling, David Ltd.	135
Drummond-Asquith Ltd.	53, 74 & 75
Drummond Bros. Ltd.	53
Dunbar & Cook Ltd.	126
Dunlop Rubber Co. Ltd.	54
Duplex Electric Tools Ltd.	143
Eagle Milling Co. Ltd.	147
Eclipse Foundry & Engineering Co. (Dudley) Ltd.	149
Economic Stampings Ltd.	153
Edmonton Tool & Eng'g. Co. Ltd.	155
Edwards, Albert (Machinery) Ltd.	157 & 161
Edwards Bros.	150
Edwards, F. J. Ltd.	64, 157, 159, 160, 172 & 174
Elgar Machine Tool Co. Ltd.	39, 47, 136 & 162
Elliott, B. (Machinery) Ltd.	51 & 161
English Numbering Machines Ltd.	139
Evans, Fredk. W. Ltd.	150
Flame Hardeners Ltd.	141
Fletcher Miller Ltd.	78
Flexibox Ltd.	101
Follsain Wycliffe Foundries Ltd.	119
Forrest, W. & Co. Ltd.	159 & 163
Forst Broach Co. (G.B.) Ltd.	56
Frye Machine Tool Co. Ltd.	159 & 168
Fuller, Horsey Sons & Cassell	106
Funditor Ltd.	38

(Continued on page 180)

INDEX TO ADVERTISERS—*(continued from page 179)*

	PAGE
G.A. Precision Products Ltd.	153
Gate Machinery Co. Ltd.	163
General Engineers Supply Co. (1937) Ltd., The	156
Goulder, J. & Sons Ltd.	15
Glass Fibre Fabrications Ltd.	96
Graepel, H. Ltd.	156
Granby, Paul & Co. Ltd.	86 & 87
Gray, R. O.	167
Greenwood & Batley Ltd.	117
Griffiths, Gilbert, Lloyd & Co. Ltd.	114
Grimston Electric Tools Ltd.	126
G.R.M. Heat Treatments Ltd.	149
Grosvenor Works (Holloway) Ltd.	154
Habit Diamond Tooling Ltd.	49
Haesler Sales	146
Hammond Eng'g. Co. Ltd., The	155
Harper, John & Co. Ltd.	13
Harvey, G. A. & Co. (London) Ltd.	48
Harvey-Hood Eng'g. Co. Ltd	148
Headland Eng'g. Developments Ltd.	132
Hedges Reinforced Plastics Ltd.	146
Heliot	172
Henderson & Keay Ltd.	77
Herbert, Alfred Ltd.	17 & 19
High Frequency Heat Treatment	149
High Speed Service Tool Co. Ltd.	149
Highbury Metal Spinning Co. (1955) Ltd.	153
Holly Engineering (Drayton) Ltd.	154
Hopkinsons Ltd.	139
Hughes Engineering Co. (Leicester) Ltd.	150
Humphreys, J. H. & Sons Ltd.	136
Hunt, Herbert & Sons Ltd.	137
Huntley & Sparks Ltd.	151
Hurlock, Wm. Jnr. Ltd.	176
Ide, C. F. Engineering Ltd.	146
Ideal Hardening Co. Ltd.	148
Imperial Chemical Industries Ltd.	12
Impregnated Diamond Products Ltd.	46
Industrial Trading Co. Ltd.	156
Jardine, John Ltd.	149
J.B. Machine Tool Co. Ltd.	158 & 161
Johansson, C. E. Ltd.	88
Jones, A. A. & Shipman Ltd.	102 & 113
Jones, E. H. (Machine Tools) Ltd.	158 & 160
Kayser Ellison & Co. Ltd.	93
K. & C. Machinery Ltd.	170
Keelavite Hydraulics Ltd.	5
Keir, Alan Ltd.	149
Kelly, R. & Sons Ltd.	159 & 168
Kemp Precision Tooling Ltd.	154
Kempsafe Oil Burners Ltd.	138
Kenworthy Jig & Press Tool Co. Ltd.	154
Kenilworth Mnfg. Co. Ltd., The	145
K.E.N.T. Machinery & Engineering Co.	164
Kinnings, Arnold & Sons Ltd.	104
Kirk, Harry Eng'g. Ltd.	164
Kitchen, A.-D. Walker Ltd.	106
Kneller (Instrument & Tools) Ltd.	81
Lancing Machine Tools Ltd.	111
Landen (Engineers) Ltd.	147
Lang, John & Sons Ltd.	25
Lattimer, E. R. Ltd.	152
Lawrence, A. & Co. (Machine Tools) Ltd.	157 & 161
Layton, M. C. Ltd.	158
Lee, Arthur & Sons Ltd.	55
Lees Hall & Sons Ltd.	150
Lench, Thos. Wm. Ltd.	122
Lenches (Birmingham) Ltd.	114
Leyton Eng'g. Co. Ltd.	150
Leytonstone Jig & Tool Co. Ltd.	22
Liberty Eng'g. Supplies Ltd.	164
Lines, J. H. Ltd.	144
MacDowall Equipment Co. Ltd.	154
MacEchern & Co. Ltd.	148
Machine Shop Equipment Ltd.	95
Marbaix, Gaston E. Ltd.	108
Marsden & Shiers Ltd.	153
Marsden, W. G. Engineering Ltd.	151
Martin Bros. (Machinery) Ltd.	168
Martonair Ltd.	103
Maun Industries Ltd.	143
Maysmith Eng'g. Co. Ltd.	155
Meddings, W. J. Ltd.	27 & 69
Mek-Elek Engineering Ltd.	134
Melbourne Eng' Co. Ltd.	122
Mercantile Credit Co. Ltd.	100
Midland Machine Tool Co., The	172
Millen, Edwin & Sons Ltd.	157 & 176
Mills, George (Engineers) Ltd.	149
Modern Machine Tools Ltd.	173
Monks & Crane Ltd.	134
Mortimer Engineering Co. Ltd.	144
Mortimer Machine Tool Co. Ltd.	43
Moser Cams & Tools Ltd.	134
Murray's (Pretoria) Eng'g Co. Ltd.	140
Naish Bros. & Co. Ltd.	153
Neill, James & Co. (Sheffield) Ltd.	*Inside Front Cover* & 68
Nettlefold & Moser Ltd	20
Newall Group Sales Ltd.	3
Newall Used Machine Division	160
Newman Industries Ltd.	158 & 163
Nickols Automatics Ltd.	128
Nielsen, F. C. & Son	156
Norton Grinding Wheel Co. Ltd.	*Back Cover*
Norton, T. & Co. Ltd.	118
Norton, W. E. (Machine Tools) Ltd.	165
Novogage Ltd.	149
O.K. Trading (B'ham Factors) Ltd.	156
Osborn, Samuel & Co. Ltd.	84
Parkes (Machine Tools) Ltd.	173 & 176
Parkin, F. M. (Sheffield) Ltd.	94
Peak Eng'g. Ltd.	8 & 9
Pidgen Bros. Ltd.	166
P.M.T. (Machine Tools) Ltd.	175
Polarcold Ltd.	153
Polistor Ltd.	176
Pollard, Fredk. & Co. Ltd.	72
Pratt, F. & Co. Ltd.	57
Pratt, Levick & Co. Ltd.	11
Precision Heating Ltd.	148
Precision Products (Romford) Ltd.	147
Pultra Ltd.	137
Raistrick, J. E. Ltd.	158
Rawlplug Co. Ltd., The	*Inside Back Cover*
Rayner, Peter Ltd.	146
Redcar Eng'g. Co. Ltd.	152
Reliant Design Co. Ltd.	147
Renold Chains Ltd.	83
Revolving Centres Ltd.	134
R.J.H. Tool & Equipment Co. Ltd., The	138
Rockwell Machine Tool Co. Ltd.	33, 34, 35, 36 & 142
Rodger, Setterington & Ptns.	147
Rodgers Bros. Ltd.	146
Rollo Industries Ltd.	130
Rolls Tools Ltd.	171
Rotax Ltd.	10
Roth, L.	164
Rowland, F. E. & Co. Ltd.	60
Rubert & Co. Ltd.	144
Ryder, Thomas & Son Ltd.	2
Rye, Claude Bearings	155 & 157
Sanderson Bros. & Newbould Ltd.	32
Sandvik Swedish Steels Ltd.	62
Schrader's Son, A.	81
Scottish Machine Tool Corp. Ltd.	50
Selson Machine Tool Co. Ltd., The	41
Seton Creaghe Engineering Ltd.	147, 149 & 152
Shand, J. H. Ltd.	120
Sheet Metal Machinery Co. Ltd.	140
Sheffield Twist Drill & Steel Co Ltd., The	89
Shell-Mex Ltd.	70 & 71
Shelmerdine & Mulley Ltd.	152
Simmonds Aerocessories Ltd.	107
Slingsby, Walter & Co. Ltd.	156
Smith & Grace Ltd.	136
Smith & Netherwood Ltd.	152
Song Machine Tools Ltd.	166, 169 & 174
Solex (Gauges) Ltd.	98
Southern Engineering & Machinery Co. Ltd.	158
Spectra Chemicals Ltd.	73
Spring Steel Productions Ltd.	132
Staines Machine Tool Co. Ltd.	170
Stalker Drill Works Ltd.	131
Stancroft Ltd.	158, 164 & 176
Stephens, R. & Son Ltd.	154
Stevens & Bullivant Ltd.	82
Stubs, Peter Ltd.	99
Sussex Rubber Co. Ltd.	142
Sykes Machine Tool Co. Ltd.	29
Tate Machine Tool Co. Ltd.	159, 166 & 170
Taylor & Jones Ltd.	110
Tecalemit Ltd.	76
Thoka Machinery Supplies Ltd.	123
Thompson, Joseph (Sheffield) Ltd.	112
Thompson, Michael S. Ltd	180
Times Machinery Co. Ltd.	104
Trevena & Glover Ltd.	153
Turner, G. H. & Co. Ltd.	140
Try, Gordon Ltd.	102
Try, Thos. Ltd.	102
Universal Ball Bearing Co.	155
Valley Products (Lye) Ltd	138
Vaughan Associates Ltd.	*Front Cover*
Veraloy Products Ltd.	58
Victa Engineering Co.	108
Visual Planning Systems Ltd.	138
Wadkin Ltd.	125
Ward, M. (Machine Tools) Ltd.	158 & 162
Ward, Thos. W. Ltd.	174
Webb, R.	151
Weeks & Wilson Ltd.	92
West Green Tool Co.	155
Westool Ltd.	90 & 91
White, Thos. & Sons Ltd.	18
Whiteley, Wm. & Sons Ltd.	14
Wickman Ltd.	85
Widdowson, Herbert & Sons Ltd.	65, 66, 67 & 170
Wigglesworth, Frank & Co. Ltd.	142
Wild-Barfield Electric Furnaces Ltd.	1
Williams, H. & Son Ltd.	179
Windley Bros. Ltd.	130
W.J.L. (Machinery) Ltd.	155
Worson Die Cushions Ltd.	145
Young, John S. & Co. Ltd.	124
Zephyr Cams Ltd.	151
Zwicky, G. (London) Ltd.	112

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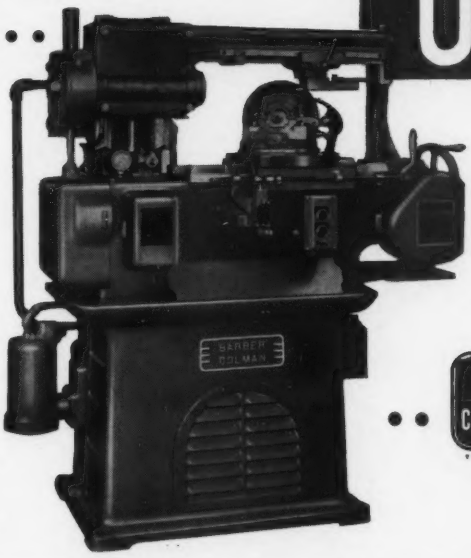

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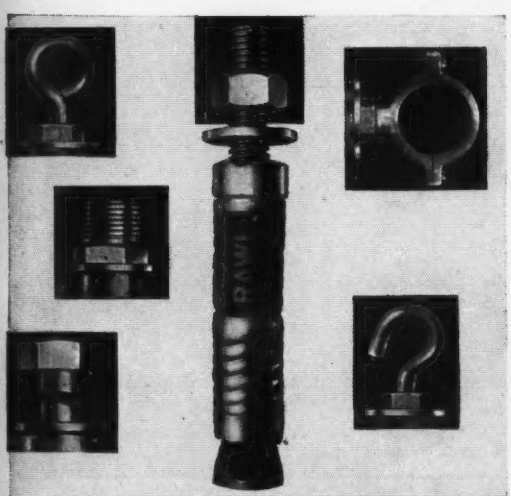

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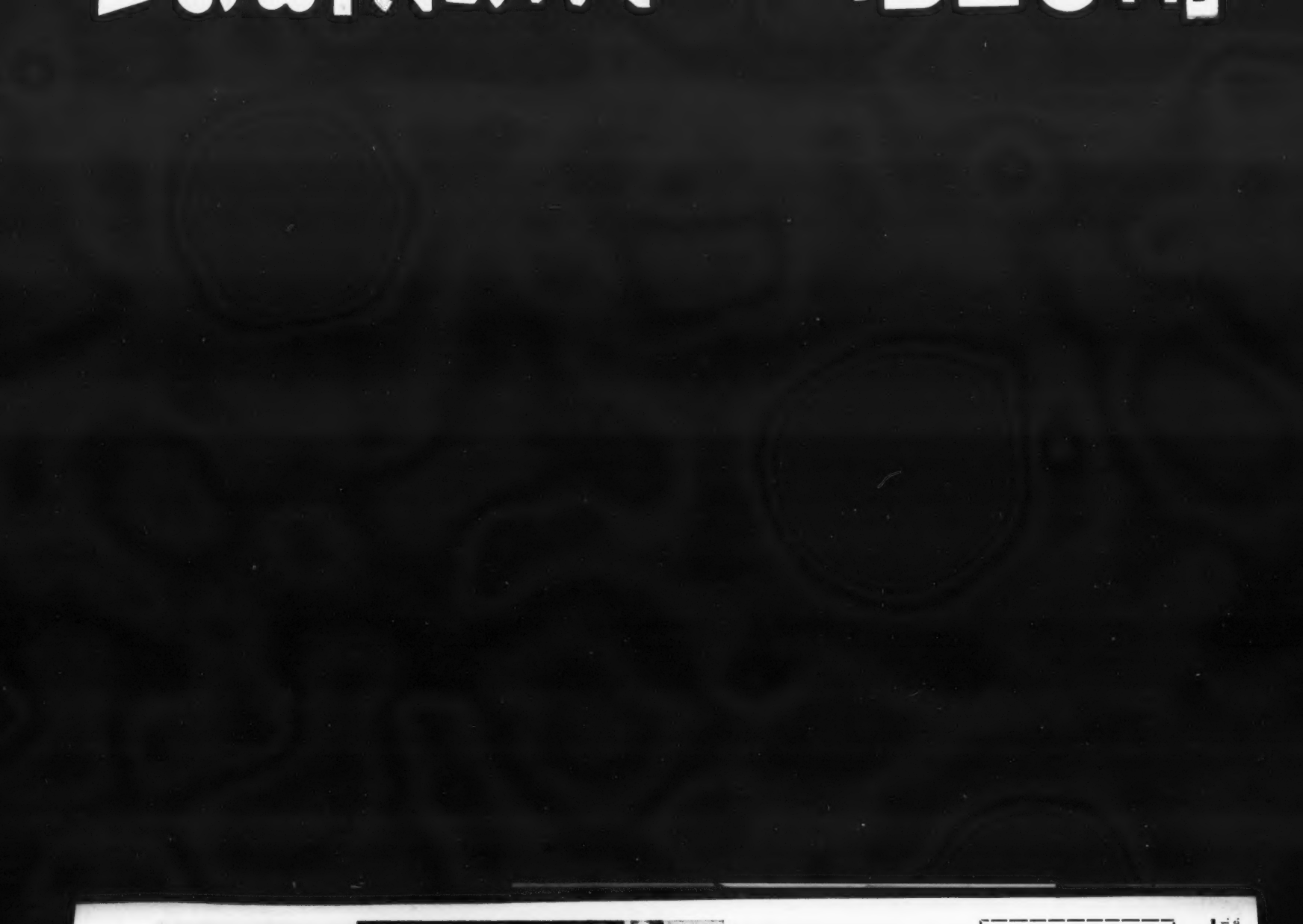
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